



***S. Belomestnykh***

# **Superconducting RF for storage rings, ERLs, and linac-based FELs:**

- **Lecture 11** *Frequency tuners*





## *Why do SRF cavities need frequency tuners?*

- Tune cavity resonance to operating frequency after cool-down
- Actively compensate reactive part of beam loading
- Detune cavity on purpose for bypass operation
- Find resonance after RF trips
- Compensate slow frequency drift
- Compensate static Lorentz force detuning (CW operation)
- Compensate dynamic Lorentz force detuning (in pulsed machines)
- Compensate microphonics (in CW-machines)

## *Design issues*

- long lifetime
- tuner resolution
- compact
- low hysteresis / backlash
- limit range to avoid plastic deformation of the cavity
- limit cross-talk to neighboring cavities
- limit cryogenic heat load
- provide serviceability



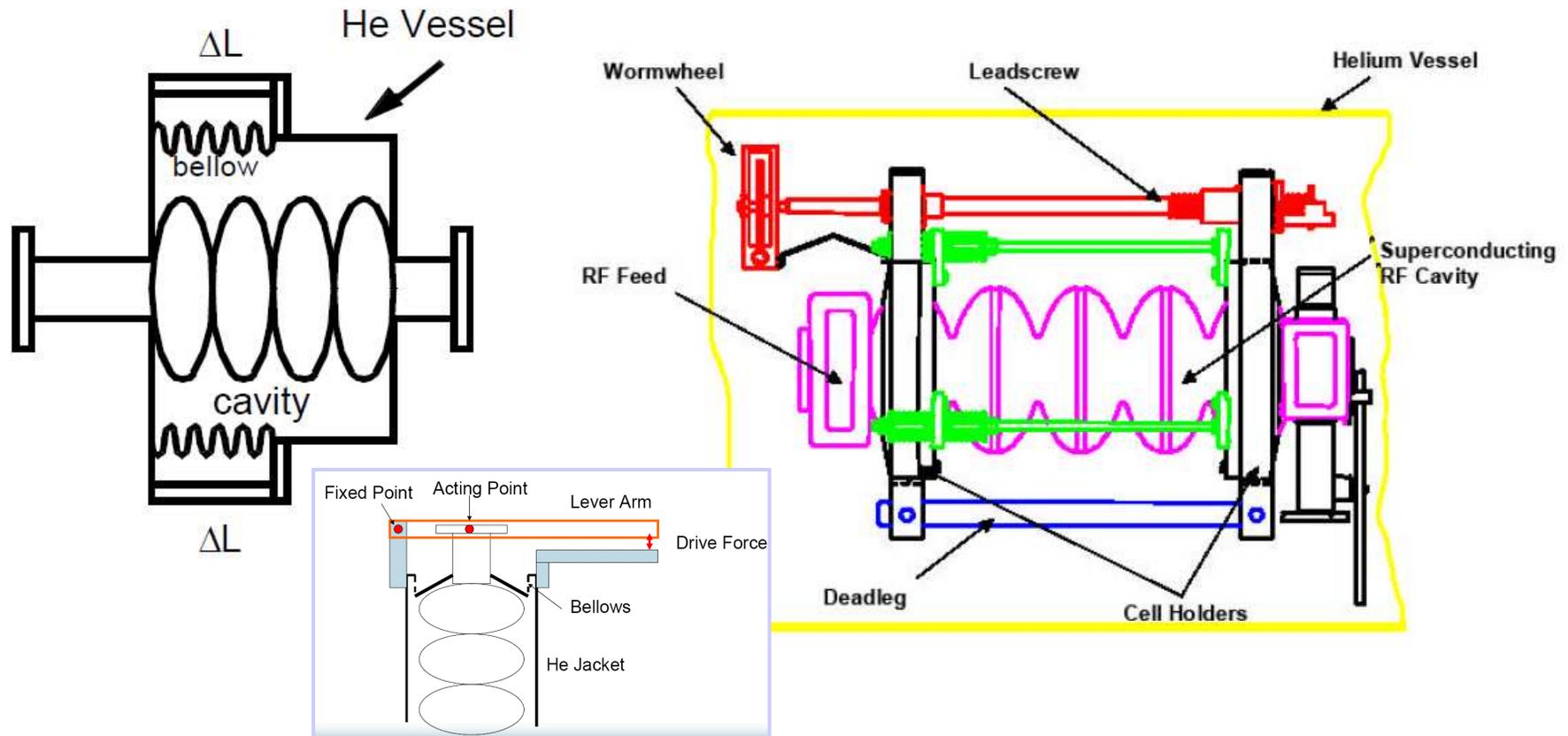
- **Mechanical length change or other deformation of the cavity**
  - based on a motor driven mechanism (slow/coarse) → compensate slow He pressure fluctuations and beam loading; two versions: 1) warm motor + lever + tuning plate = large size, but good serviceability; 2) cold motor = compact; wide tuning range of several 100 kHz, required resolution is ~1 Hz. Typical sensitivity is ~500 Hz/ $\mu\text{m}$ .
  - based on PZT or magnetostrictive element (fast) compensate microphonics and LF detuning in pulsed machines; still under development; narrow tuning range (several cavity bandwidths), but fast response (~1 kHz).
  - thermal tuners (LEP).
- **VXC (external reactance) or ferrite based tuner**
- **Other: Pneumatic, thermal, electronic damping**

**Note:** Tuners which control in addition to frequency also loaded  $Q$  and incident phase are possible (three stub tuner).

**We will review only mechanical tuners as this is the only type used in high- $\beta$  cavities. Many tuners incorporate piezo elements for fast tuning.**



# Mechanical tuners

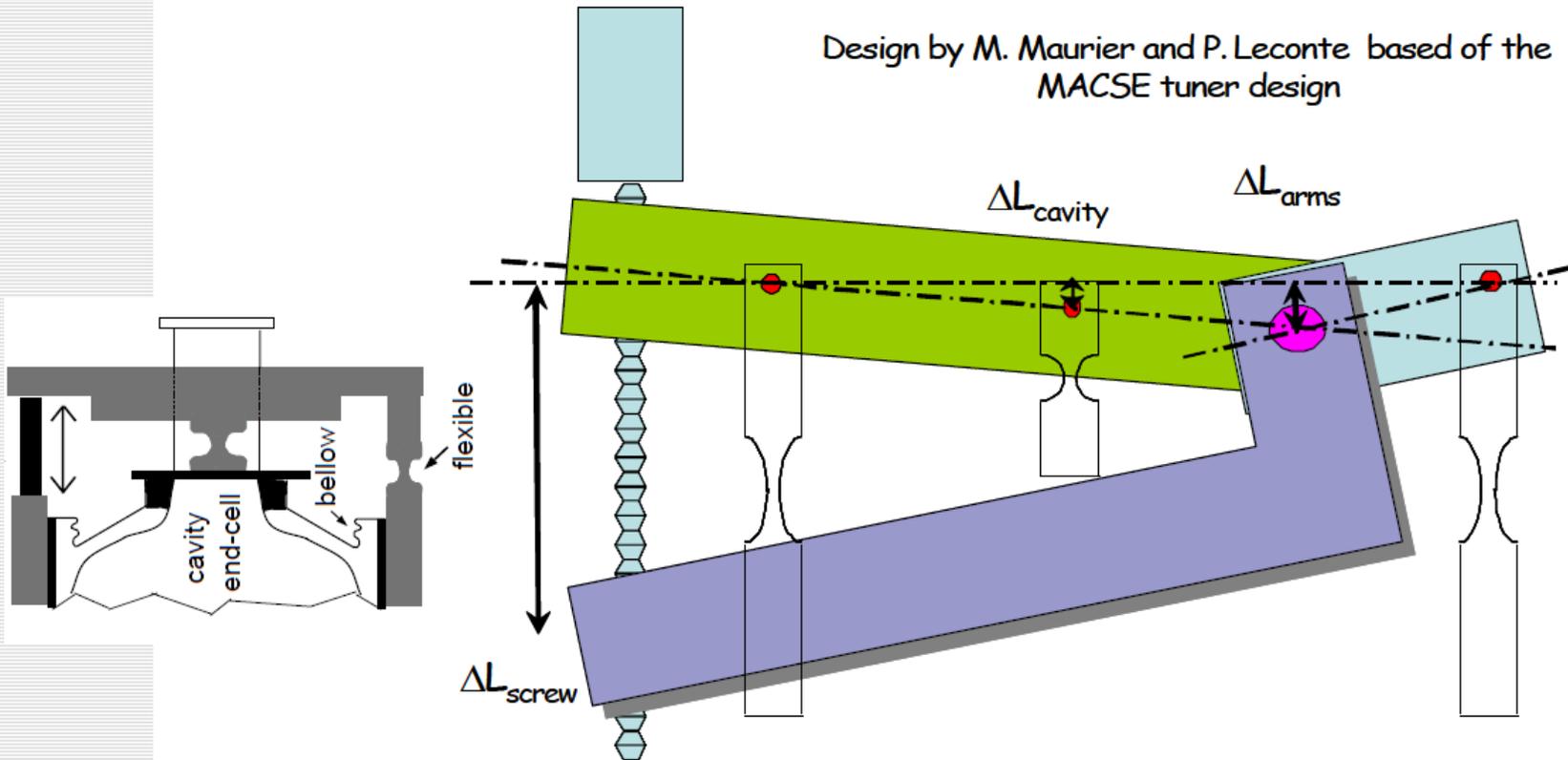


- Many tuners were developed over the years, but it seems that every mechanical engineer wants to develop his/her own design.
- We will consider how a tuner works using one example and then review several other designs.



# TTF (Saclay I) tuner

Design by M. Maurier and P. Leconte based of the  
MACSE tuner design

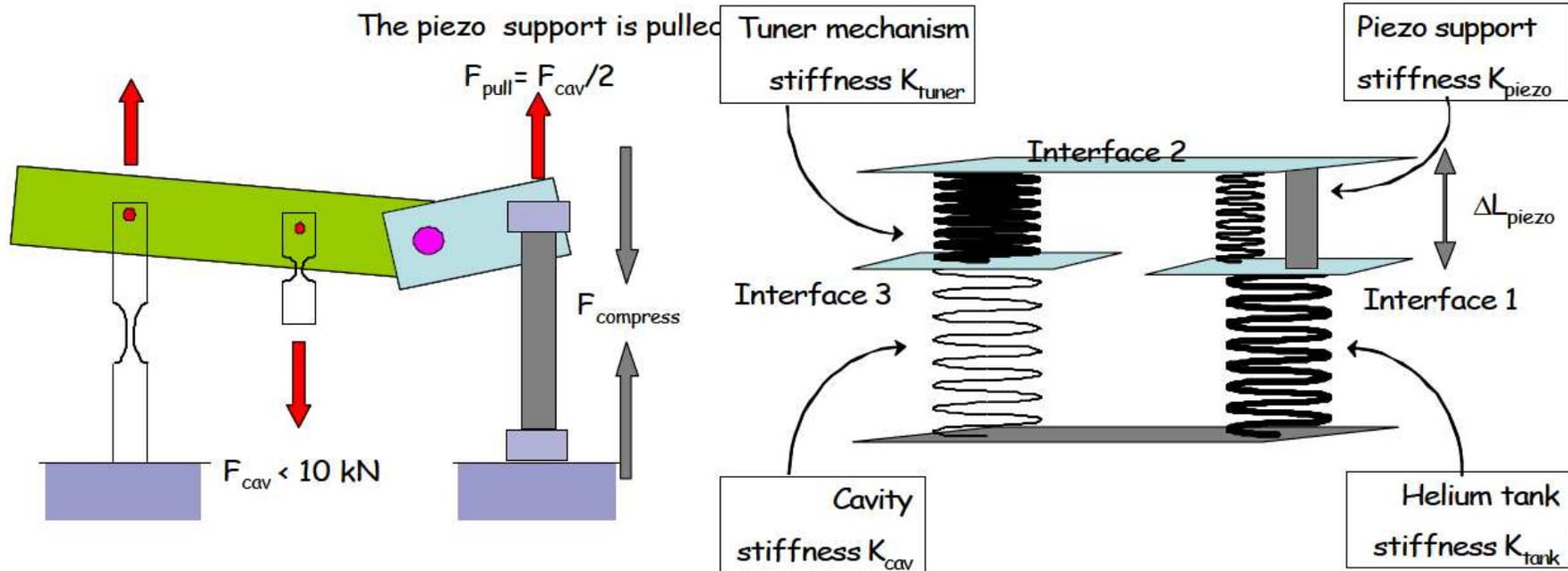


- Double lever system ratio ~1:17
- Stepping motor with harmonic drive gear box
- Screw-nut system : lubricant treatment (balzers Balinit C coating) for working at cold and in vacuum

P. Bosland



# TTF tuner with piezo



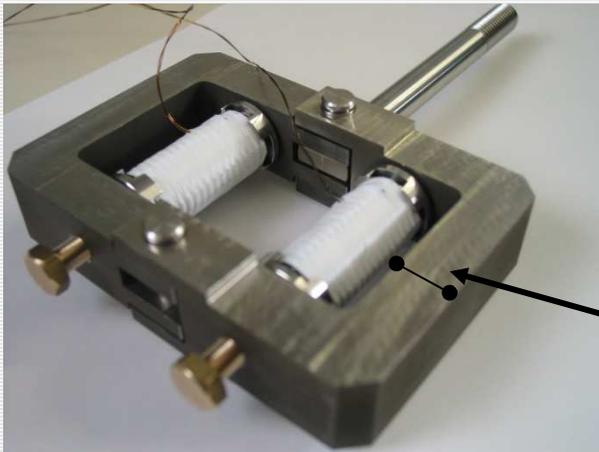
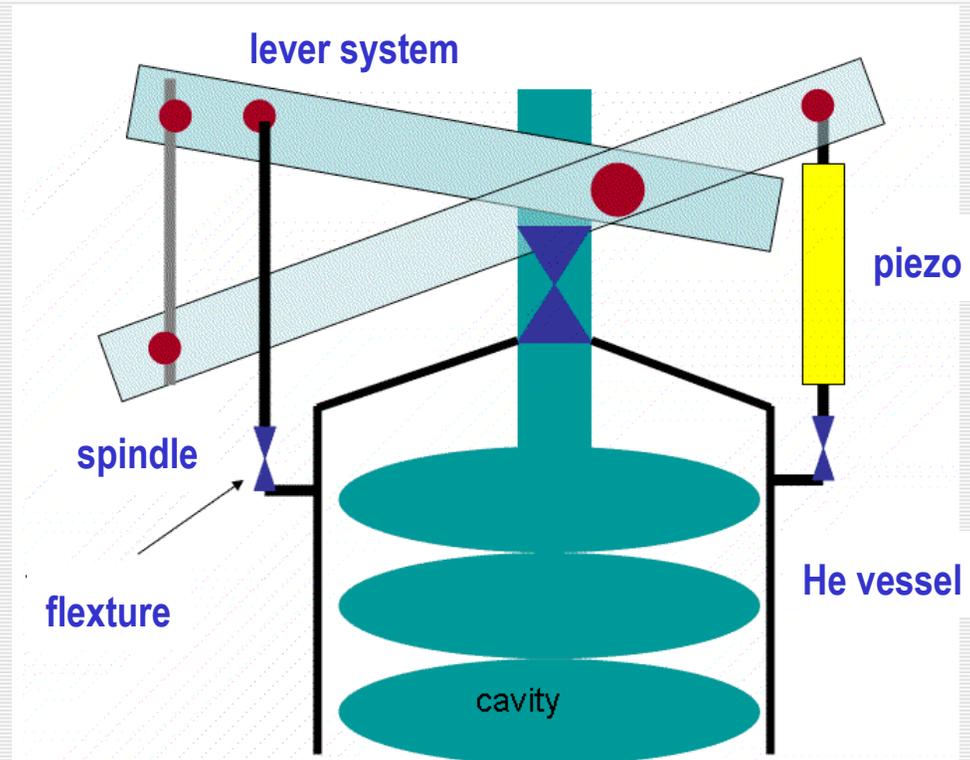
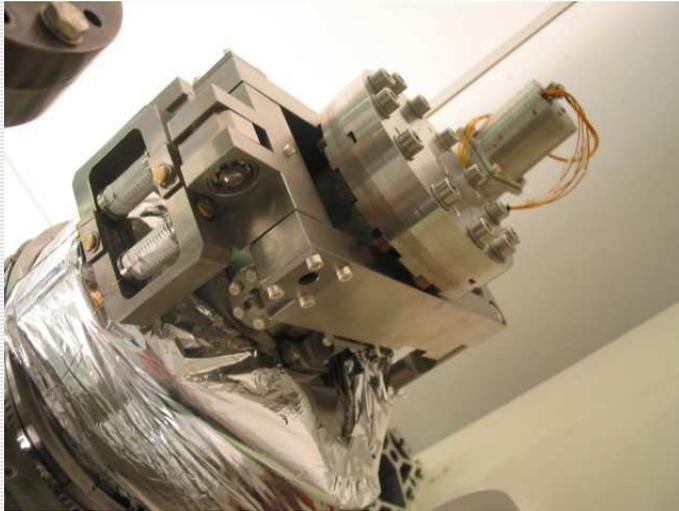
- The Piezo actuator is kept under compression by the support  $F_{\text{compress}}$
- The effective pre-load strength on the stack is  $F_{\text{preload}} = F_{\text{compress}} - F_{\text{cav}}/2$

- $\Delta L_{\text{cav}} = \Delta L_{\text{piezo}}/2$  if
  - tuner is infinit rigid ( 100 kN/mm vs 3 kN/mm for the cavity)
- the piezo displacement speed is slow compared to the system response
- the tuner is not at the neutral point

P. Bosland



# TTF tuner with piezo (2)

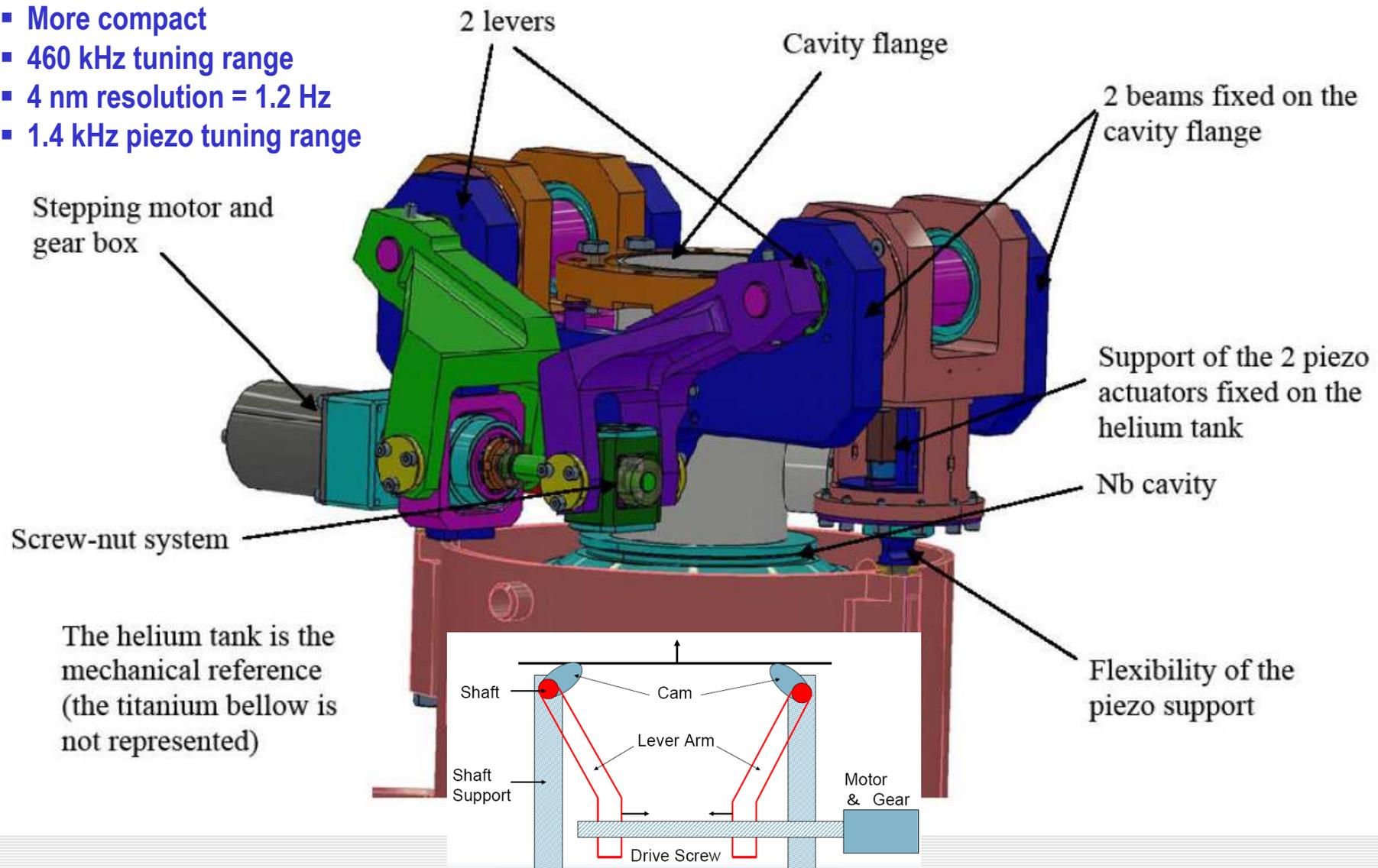


Modified piezo holder frame:  
higher wall thickness



# Saclay II tuner

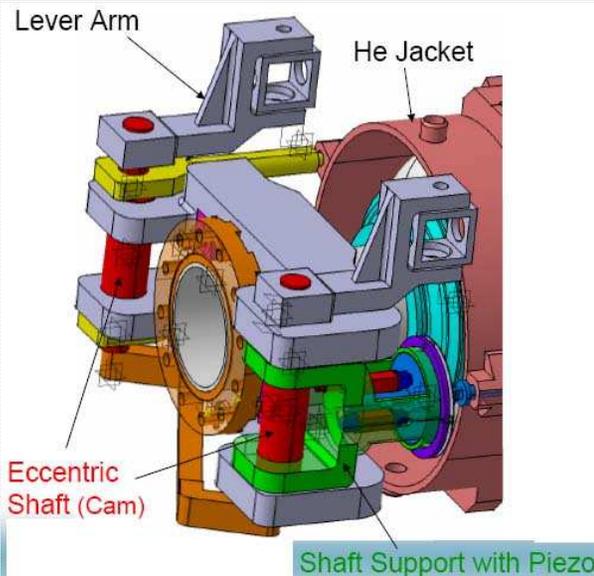
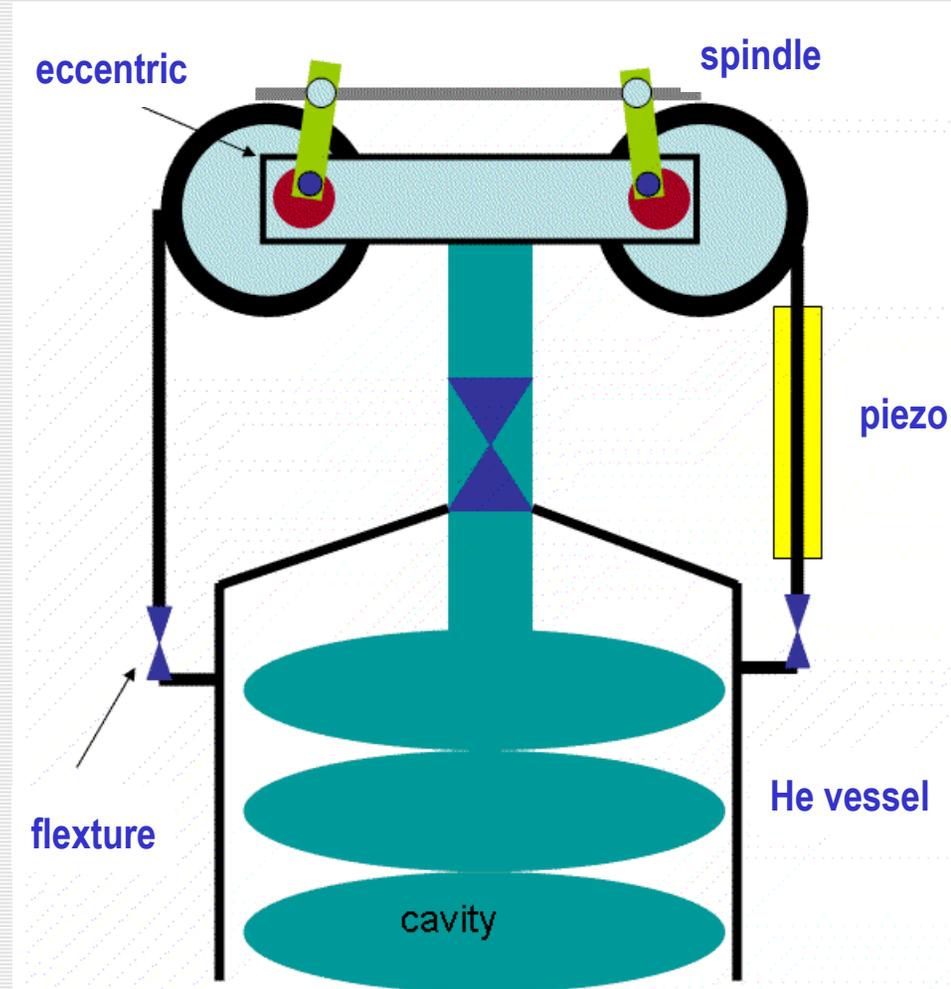
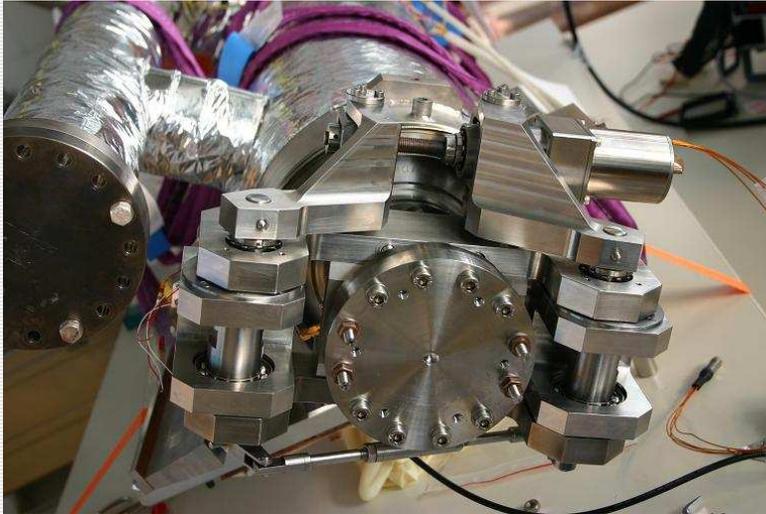
- More compact
- 460 kHz tuning range
- 4 nm resolution = 1.2 Hz
- 1.4 kHz piezo tuning range



The helium tank is the mechanical reference (the titanium bellow is not represented)



# Saclay II tuner (2)





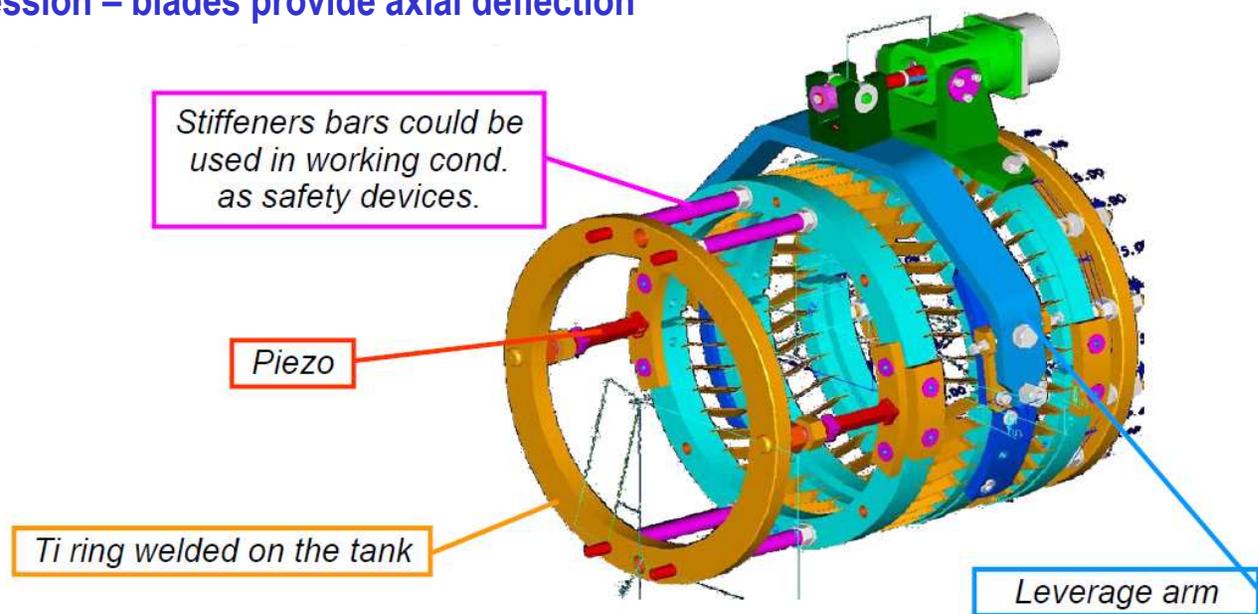
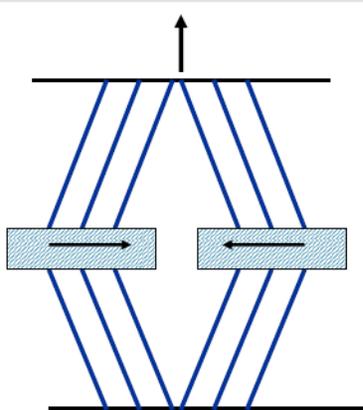
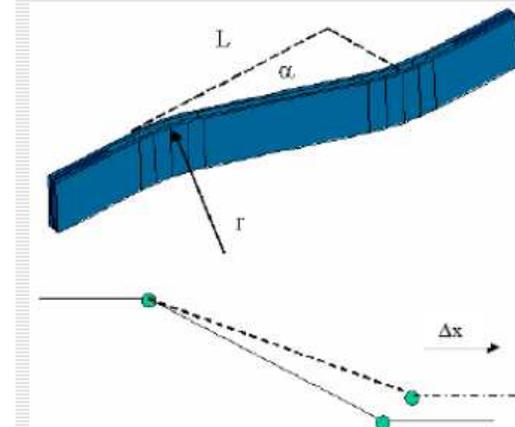
# Blade tuner

## Tuner specs:

- 1 mm fine tuning (on cavity)  $\rightarrow \Delta F$  on all piezo (sum)  $\approx 3.5$  kN
- 1 kHz fast tuning  $\rightarrow \approx 3$   $\mu\text{m}$  cavity displacement  $\rightarrow \approx 4$   $\mu\text{m}$  piezo displacement
- 4  $\mu\text{m}$  piezo displacement  $\rightarrow \approx \Delta F$  on all piezo  $\approx 11.0$  N
- $\sim 1$  Hz resolution

## Mechanism – all components are cold, in vacuum:

- Titanium frame
- Attaches to helium vessel shell
- Pre-tune using bolts pushing on shell rings
- Dicronite coating on bearings and drive screw
- Cavity tuned in tension or compression – blades provide axial deflection





# Blade tuner variations

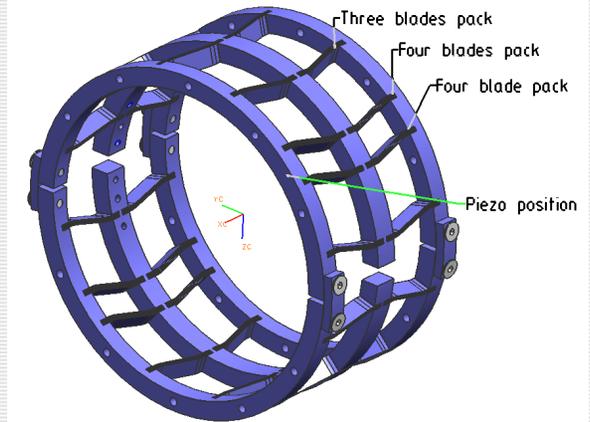
## 1st DESY prototype (Kaiser, Peters)



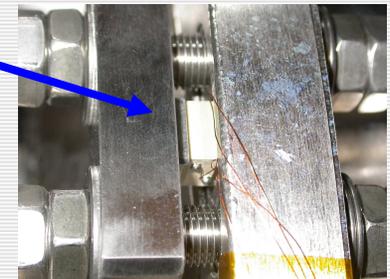
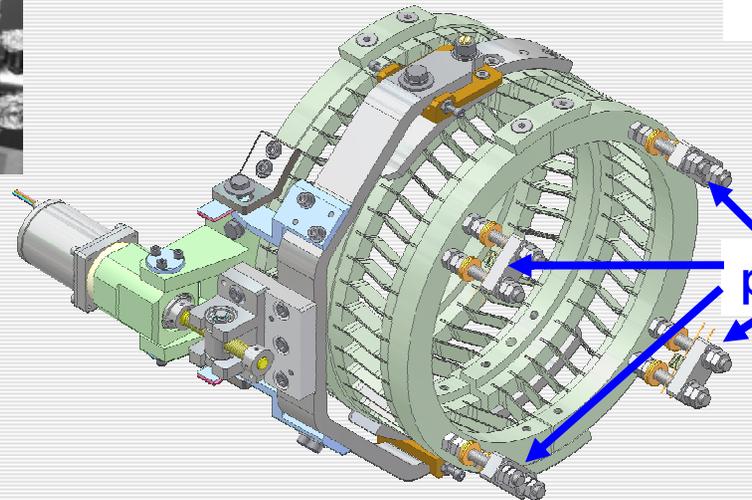
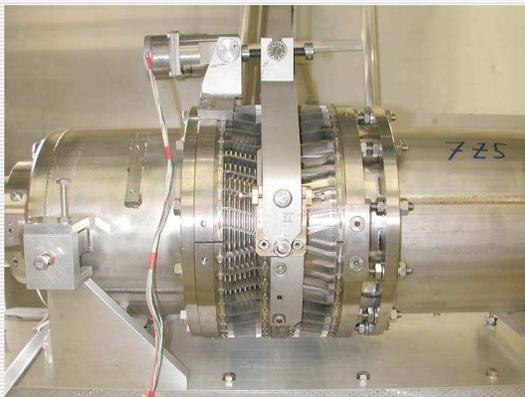
*Blade tuner occupies no beam line space: it is mounted on top of the He vessel. Can be used where beam line real estate is at premium.*



## ILC version (Pagani)



## Cornell ERL injector

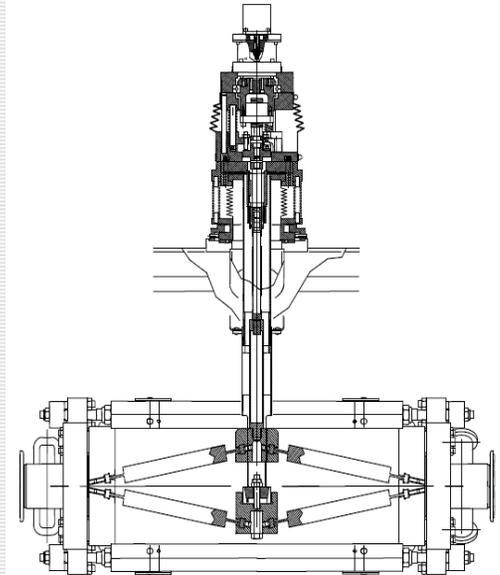
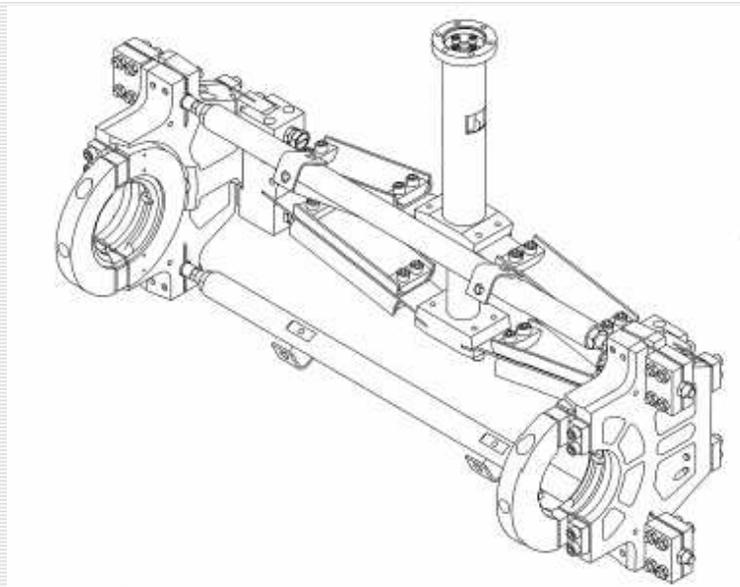


- Modification of the INFN blade tuner
- Added piezos for microphonics compensation



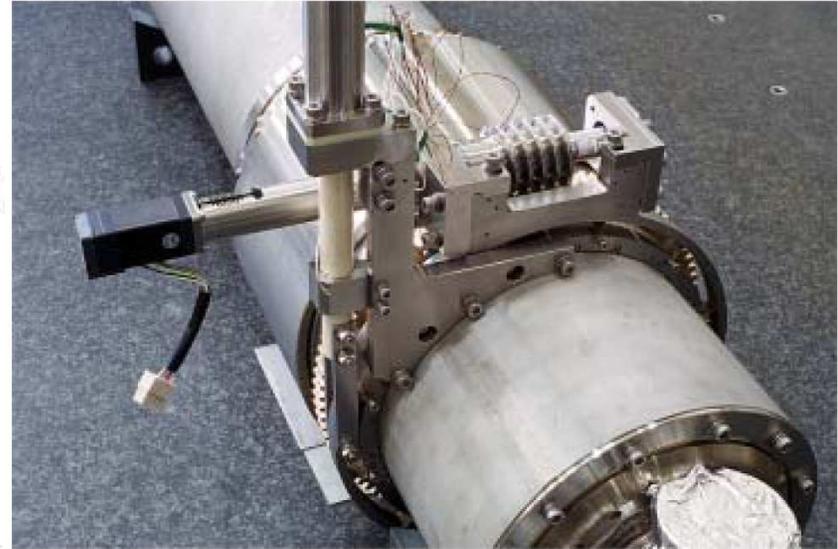
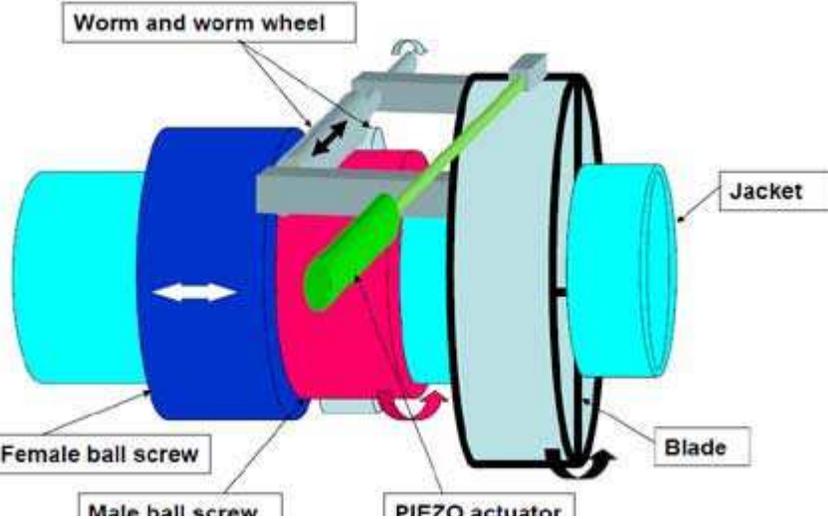
# CEBAF Upgrade tuner

- Scissor jack mechanism
  - Ti-6Al-4V Cold flexures & fulcrum bars
  - Cavity tuner in tension only
  - Attaches on hubs of cavity
- Warm transmission
  - Stepper motor, harmonic drive, ball screw and piezo mounted on top of CM
  - Openings required in shielding and vacuum tank
- No bellows between cavities
  - Need to accommodate thermal contraction of cavity string
  - Pre-load and offset each tuner while warm





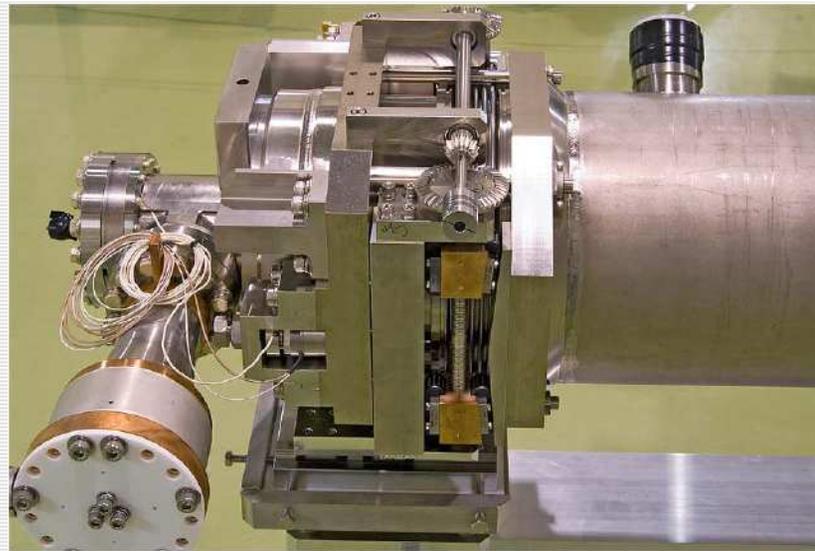
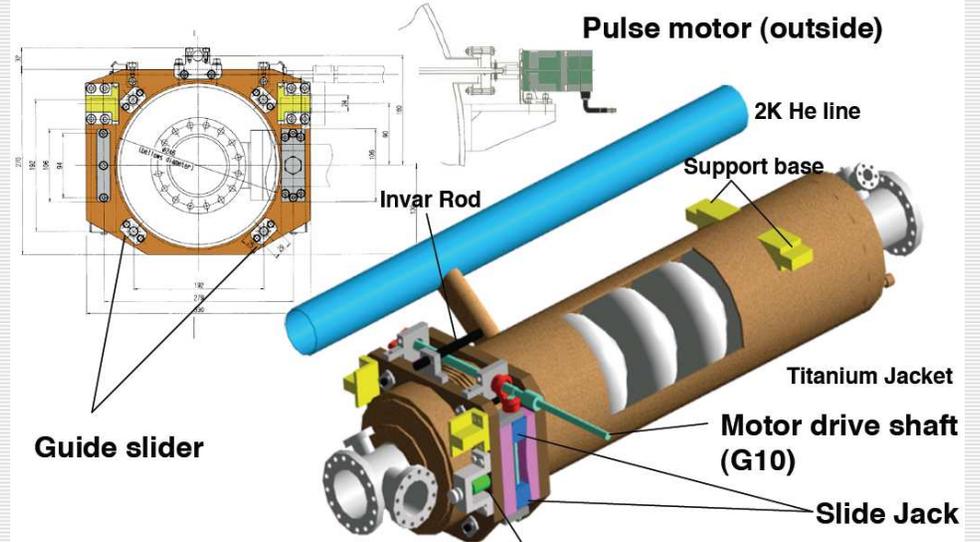
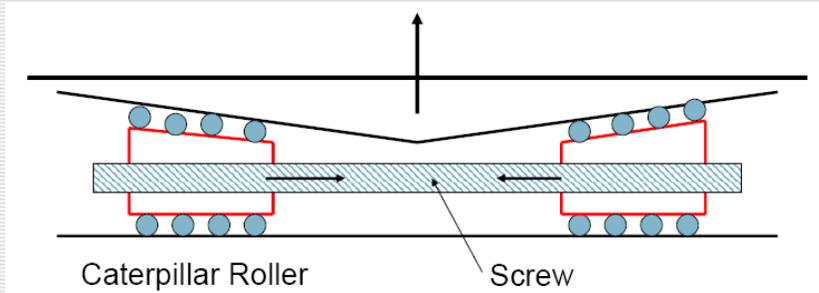
# Coaxial ball screw tuner (KEK)



- Design objectives
  - Provide large tuning range while maintaining stiffness
  - 10  $\mu\text{m}$  fast tuning stroke for 3 kHz Lorentz force detuning at 45 MV/m
- Warm transmission
  - Stepper motor, harmonic drive, ball screw and piezo mounted on top of CM
  - Openings required in shielding and vacuum tank
- No bellows between cavities
  - Need to accommodate thermal contraction of cavity string
  - Pre-load and offset each tuner while warm



# Slide jack tuner (KEK)



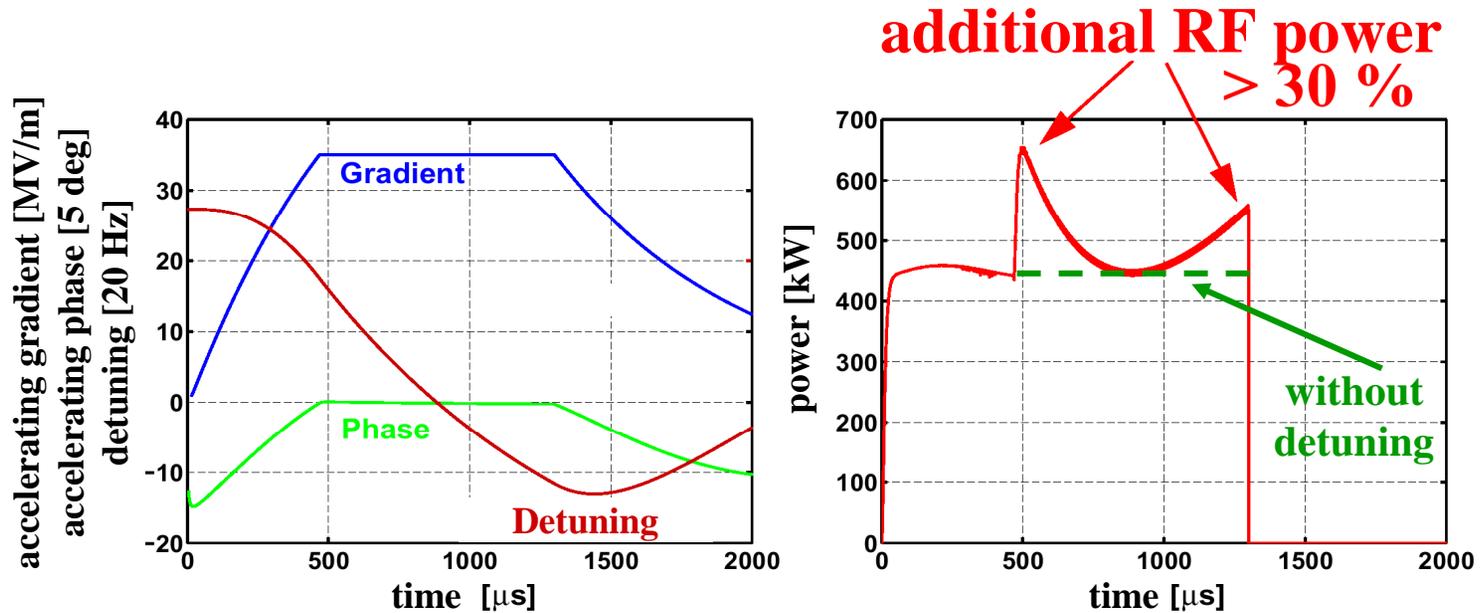


# Comparison of tuners

Design	Saclay I	Saclay II	Blade Tuner	JLab upgrade	KEK slide jack	KEK coaxial ball screw
Motor tuning range	750 kHz	460 kHz	550 kHz	500 kHz	1100 kHz	>4000 kHz
Slow resolution	0.75 Hz	1.2 Hz	< 1 Hz	< 1 Hz	< 100 Hz	< 120 Hz
Motor hysteresis	satisfying	backlash	problems at low amplitudes	satisfying		
Transmission location	5 K, vacuum	5 K, vacuum	5 K, vacuum	RT, air	RT, air	80 K, vacuum
Number of piezo elements	1 - 2	2	2 - 4	2	1	1
Piezo tuning range	840 Hz	1420 Hz	1400 Hz	1000 Hz	1900 Hz	2500 Hz
Group delay	360 $\mu$ s	150 $\mu$ s	650 $\mu$ s			
Stiffness	lower	higher	lowest			
Lowest resonance	40 Hz	40 Hz	35 Hz			
Piezo location	5 K, vacuum	5 K, vacuum	5 K, vacuum	RT, air	RT, air	80 K, vacuum



## Example: TTF cavity at 35 MV/m (simulation)

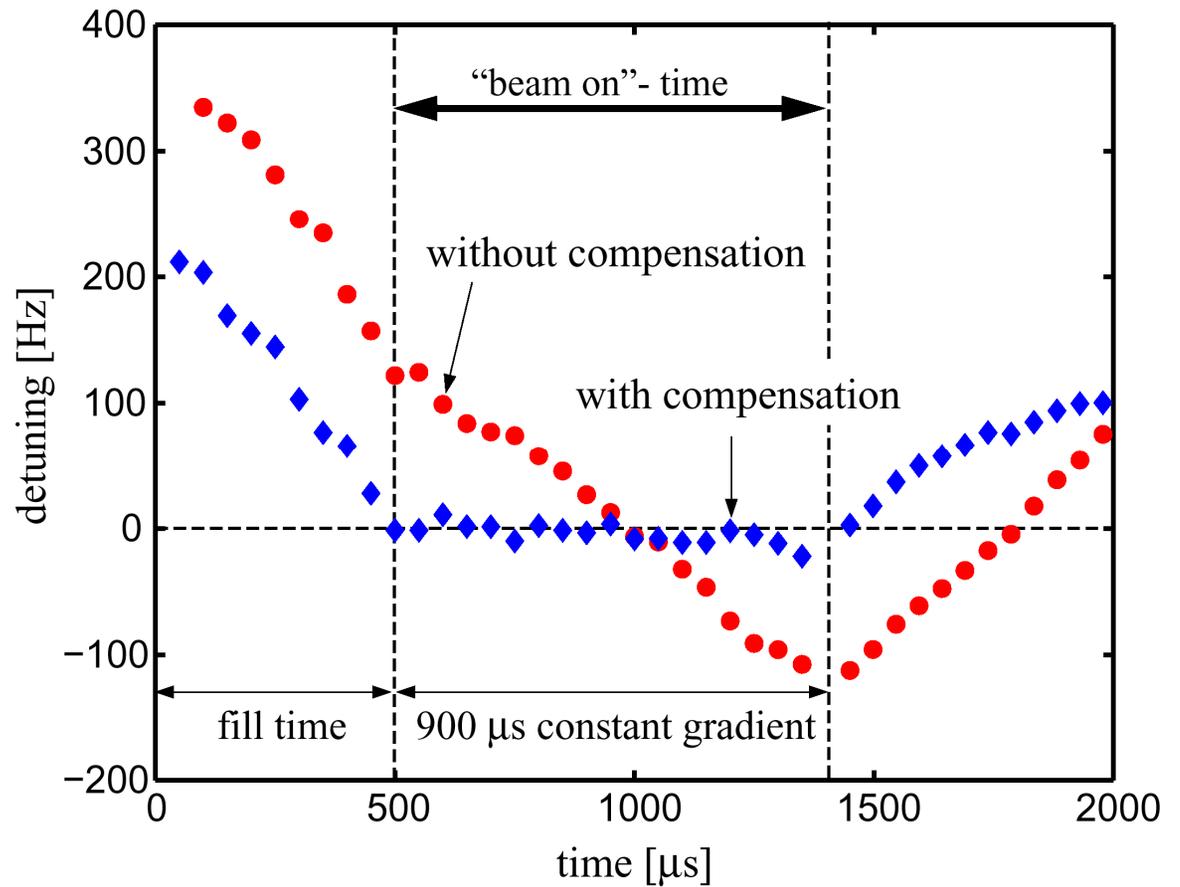
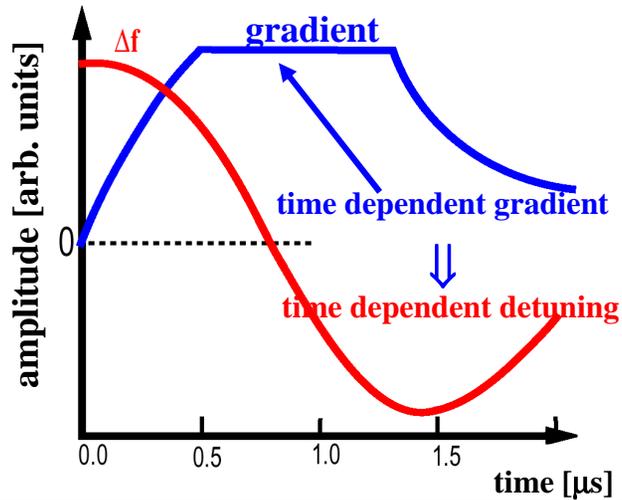


$$\frac{\Delta P}{P_{(\Delta f = 0)}} = \frac{1}{4} \left[ \frac{\Delta f}{f_{1/2}} \right]^2 \propto E^4$$



# Lorentz-force detuning compensation

*TESLA 9-cell cavity at 23.5 MV/m with 10 Hz repetition rate:*





## *Coarse tuners (stepping motor)*

- Typically cold, must be reliable and maintainable → access ports
- Direct cavity drive reduces stiffness requirements on helium vessel
- Tuner / Helium vessel stiffness should be approximately factor of 10 higher than cavity stiffness
- Flexures exhibit reduced backlash
- Typically tune in tension or compression to avoid “dead band”
- Cold transmission: Materials considerations (lubrication, vacuum); Access for repair or replacement; Electrical feedthroughs
- Warm transmission: Cooldown/tuning compliance; Port for transmission; Bellows

## *Piezo tuners*

- Operate in compression
- Warm range is 5 to 10 time larger than cold range
- Capacitive device: Low vs. High voltage (stiffer)
- Shorter piezos: reduce hysteresis; stiffer, but reduced tuning range



# What have we learned?

- Frequency tuner designs have advanced significantly during during the last decade to meet the needs of the high gradient and/or pulsed superconducting accelerators.
- A variety of technologies are available for cavity tuner designs. However combined stepper motor and piezo tuning is the method of choice for high- $\beta$  cavities.
- Important design considerations: frequency resolution; compactness; hysteresis/backlash; cold vs warm transmission; reliability; ease of maintenance; cost.

★ Next lecture: cavity fabrication, preparation and testing.