



Lecture 7

RF linacs

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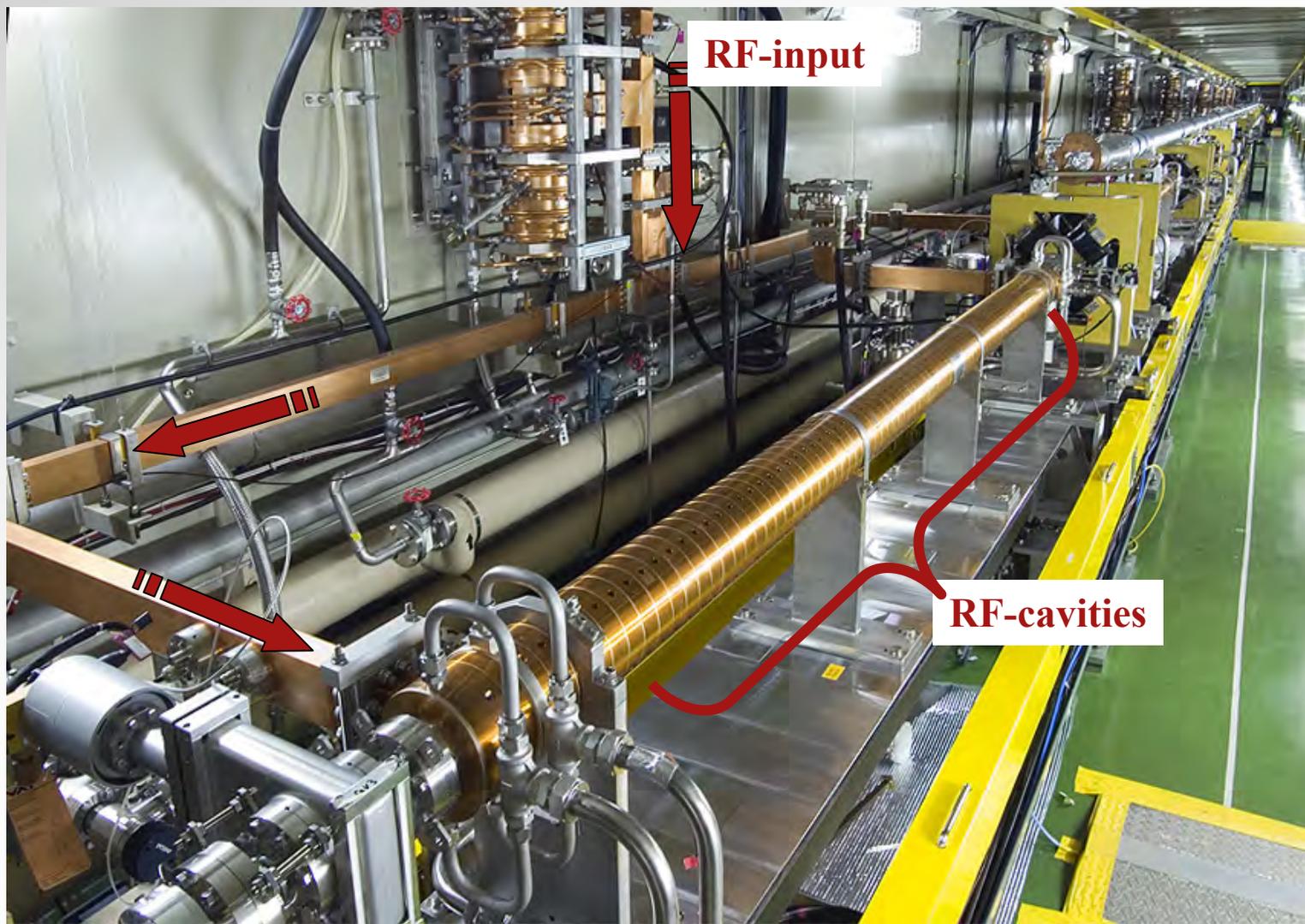
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S-band (~ 3 GHz) RF linac





Translate circuit model to a cavity model: Directly driven, re-entrant RF cavity

Outer region: Large, single turn Inductor

$$L = \frac{\mu_o \pi a^2}{2\pi(R + a)}$$



Central region: Large plate Capacitor

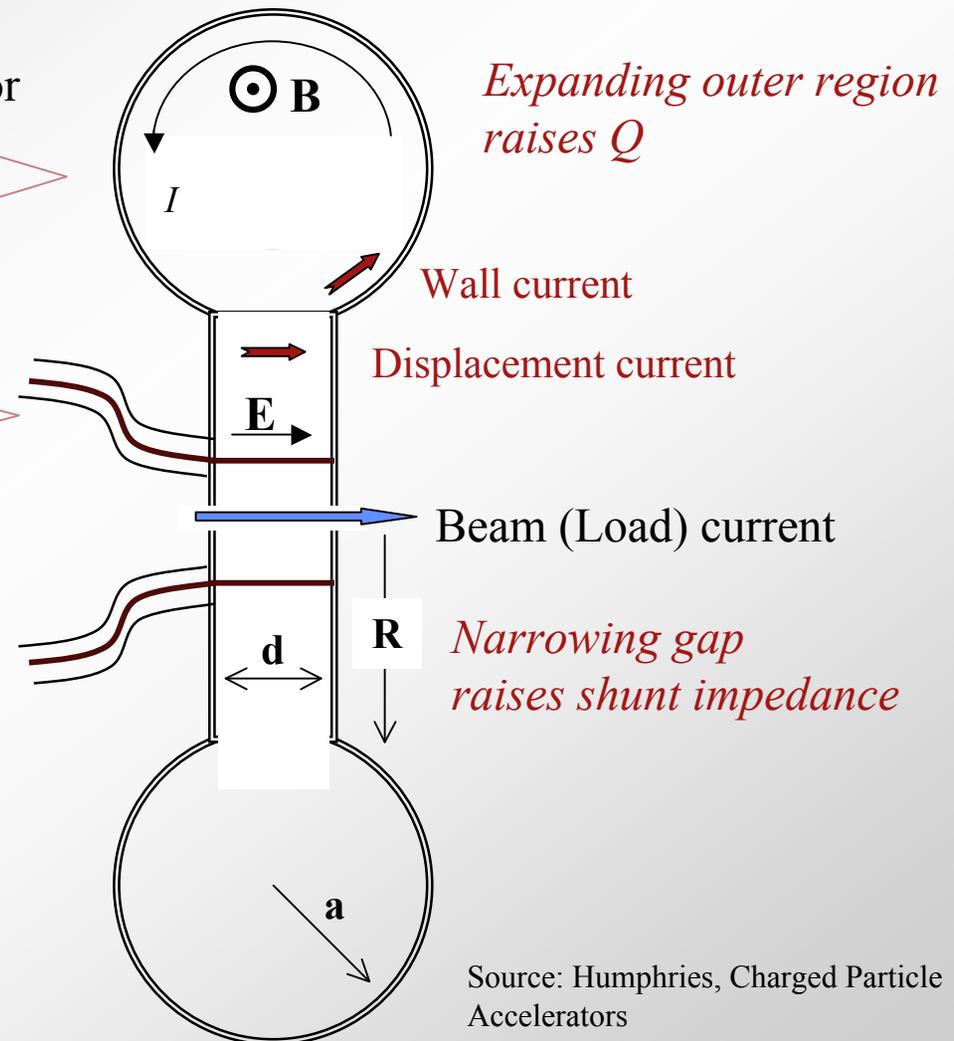
$$C = \epsilon_o \frac{\pi R^2}{d}$$



$$\omega_o = \frac{1}{\sqrt{LC}} = c \left[\frac{2((R + a)d)}{\pi R^2 a^2} \right]^{1/2}$$

Q – set by resistance in outer region

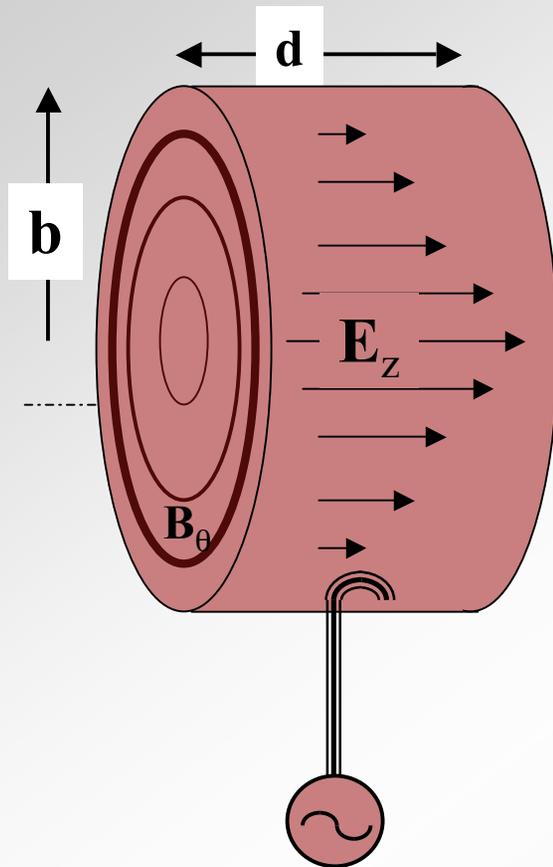
$$Q = \sqrt{\frac{L}{C}} / R$$



Source: Humphries, Charged Particle Accelerators



Properties of the RF pillbox cavity



$$\sigma_{walls} = \infty$$

- ❖ We want lowest mode: with only E_z & B_θ
- ❖ Maxwell's equations are:

$$\frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) = \frac{1}{c^2} \frac{\partial}{\partial t} E_z \quad \text{and} \quad \frac{\partial}{\partial r} E_z = \frac{\partial}{\partial t} B_\theta$$

- ❖ Take derivatives

$$\frac{\partial}{\partial t} \left[\frac{1}{r} \frac{\partial}{\partial r} (r B_\theta) \right] = \frac{\partial}{\partial t} \left[\frac{\partial B_\theta}{\partial r} + \frac{B_\theta}{r} \right] = \frac{1}{c^2} \frac{\partial^2 E_z}{\partial t^2}$$

$$\frac{\partial}{\partial r} \frac{\partial E_z}{\partial r} = \frac{\partial}{\partial r} \frac{\partial B_\theta}{\partial t}$$

\implies

$$\frac{\partial^2 E_z}{\partial r^2} + \frac{1}{r} \frac{\partial E_z}{\partial r} = \frac{1}{c^2} \frac{\partial^2 E_z}{\partial t^2}$$



For a mode with frequency ω

- ❖
$$E_z(r, t) = E_z(r) e^{i\omega t}$$
- ❖ Therefore,
$$E_z'' + \frac{E_z'}{r} + \left(\frac{\omega}{c}\right)^2 E_z = 0$$
 - (Bessel's equation, 0 order)

- ❖ Hence,

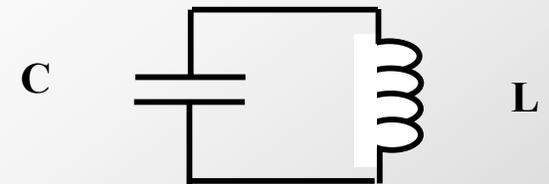
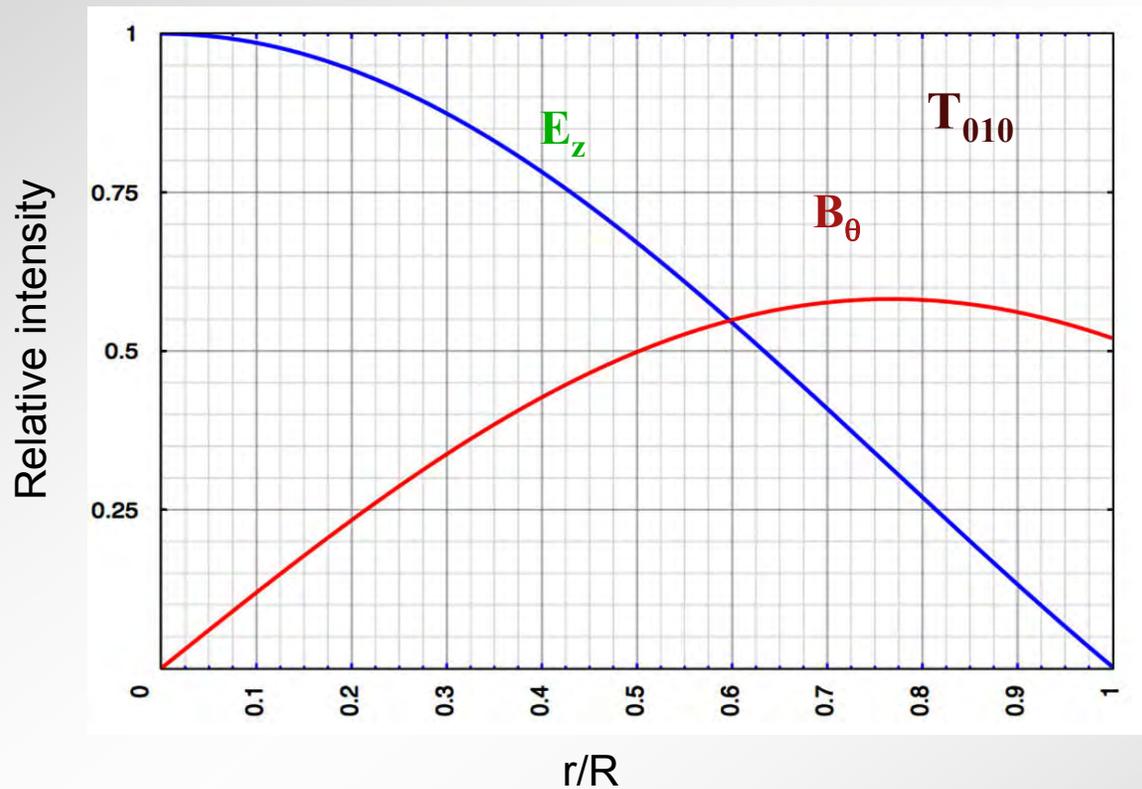
$$E_z(r) = E_o J_o\left(\frac{\omega}{c} r\right)$$

- ❖ For conducting walls, $E_z(R) = 0$, therefore

$$\frac{2\pi f}{c} b = 2.405$$

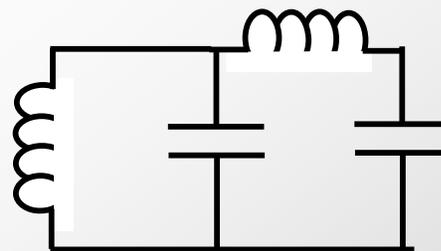
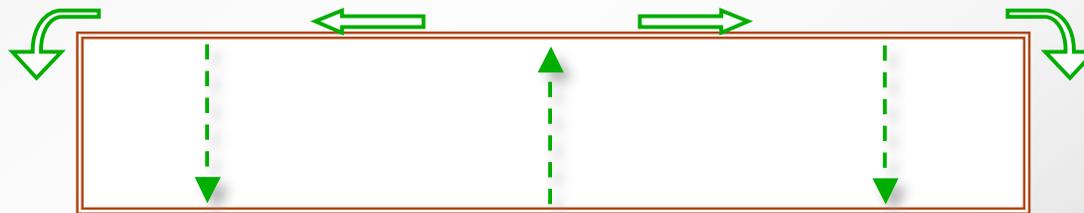
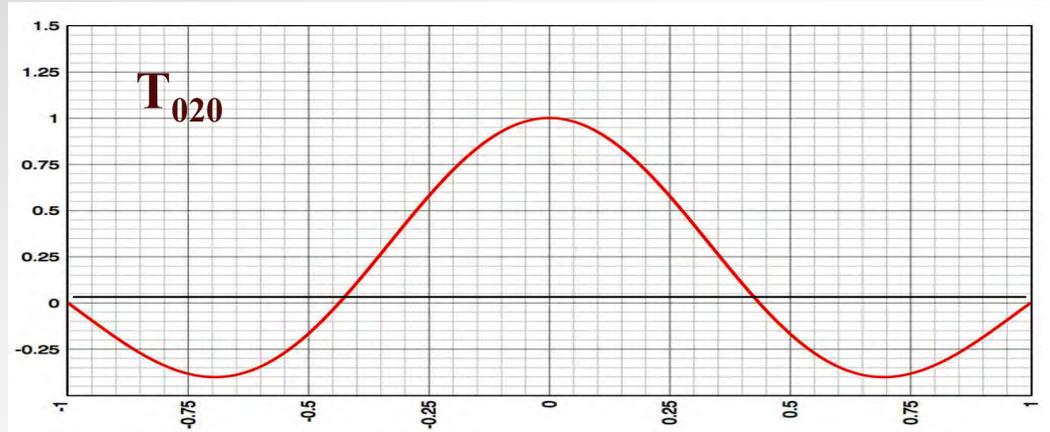


E-fields & equivalent circuit: T_{010} mode



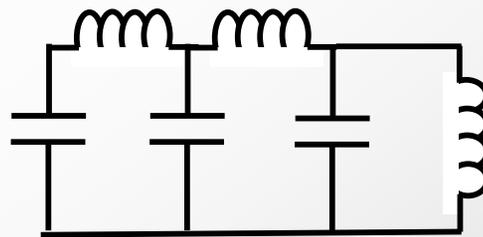
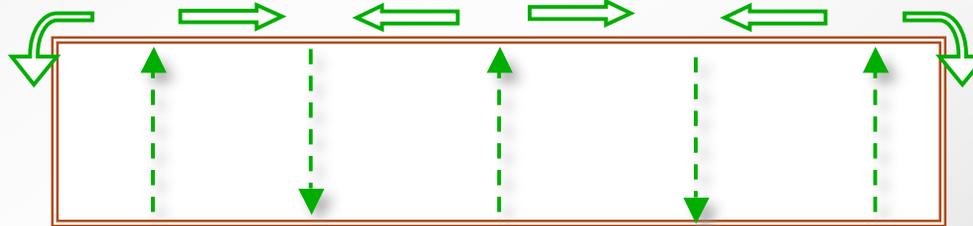
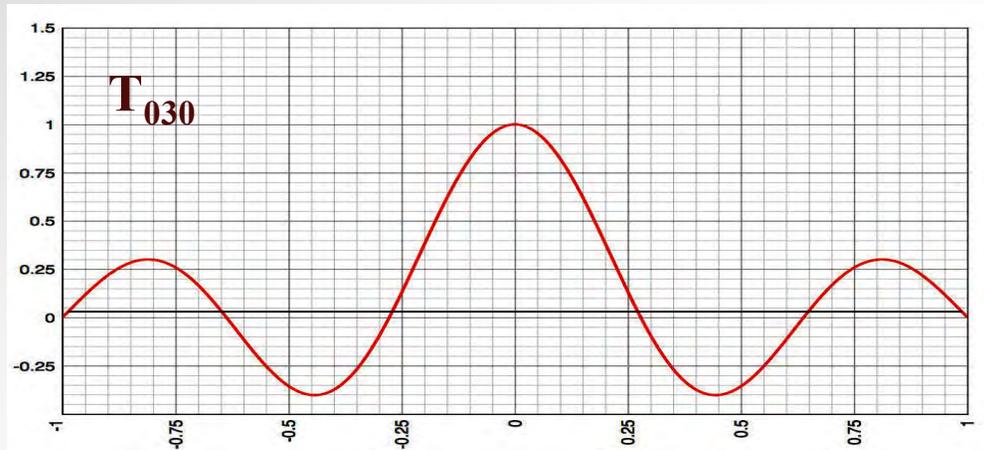


E-fields & equivalent circuits for T_{020} modes





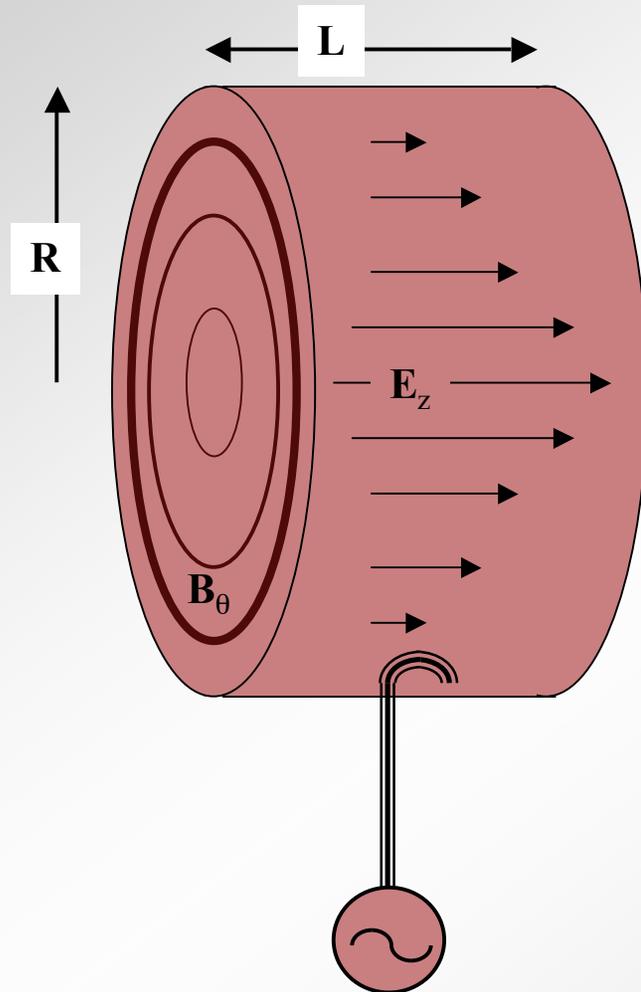
E-fields & equivalent circuits for T_{on0} modes



T_{on0} has
n coupled, resonant
circuits; each L & C
reduced by $1/n$



Simple consequences of pillbox model



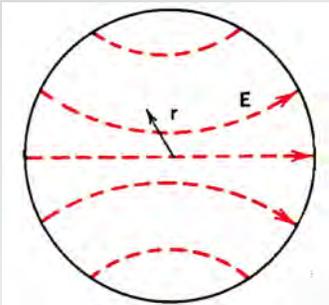
- ❖ Increasing R lowers frequency
==> Stored Energy, $\mathcal{E} \sim \omega^{-2}$
- ❖ $\mathcal{E} \sim E_z^2$
- ❖ Beam loading lowers E_z for the next bunch
- ❖ Lowering ω lowers the fractional beam loading
- ❖ Raising ω lowers $Q \sim \omega^{-1/2}$
- ❖ If time between beam pulses,
 $T_s \sim Q/\omega$
almost all \mathcal{E} is lost in the walls



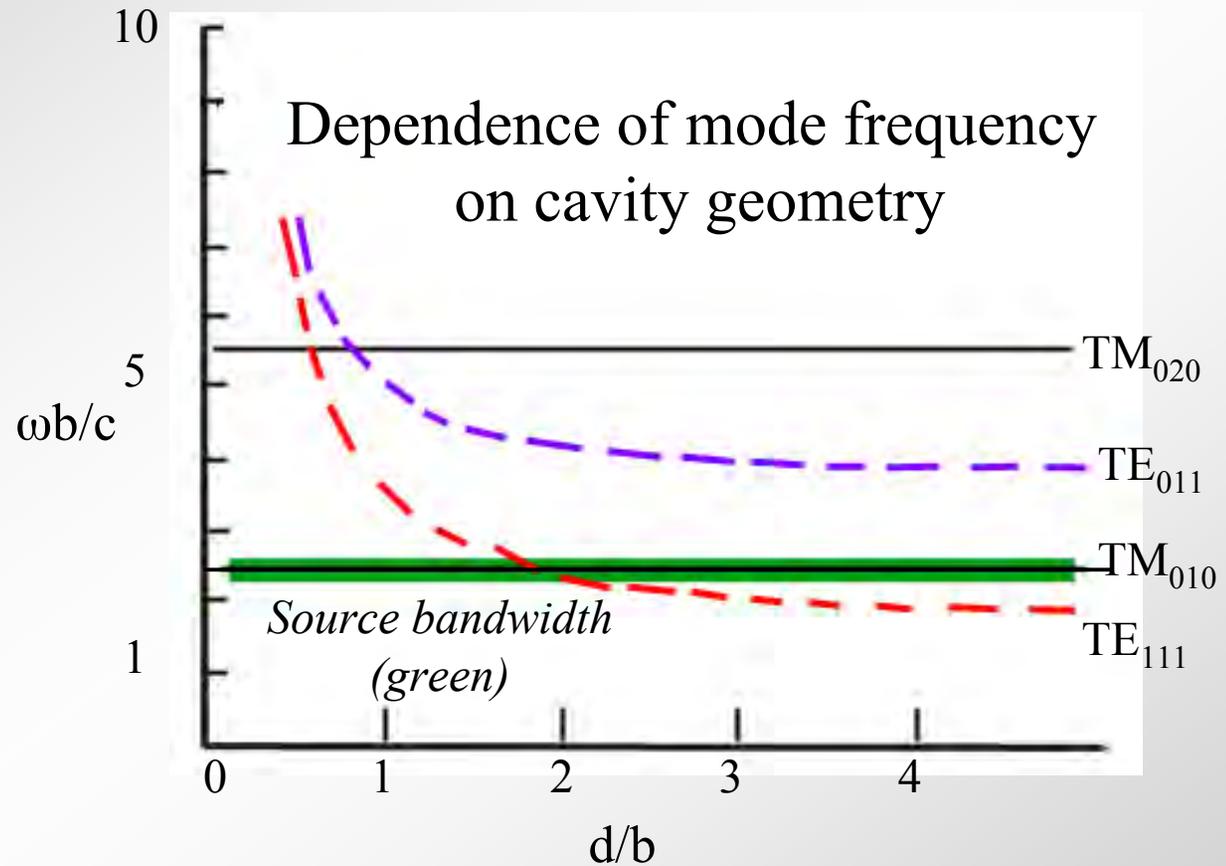
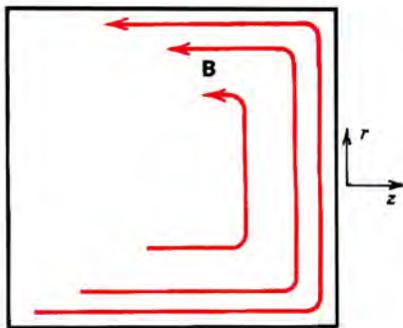
Keeping energy out of higher order modes

TE₁₁₁ mode

End view



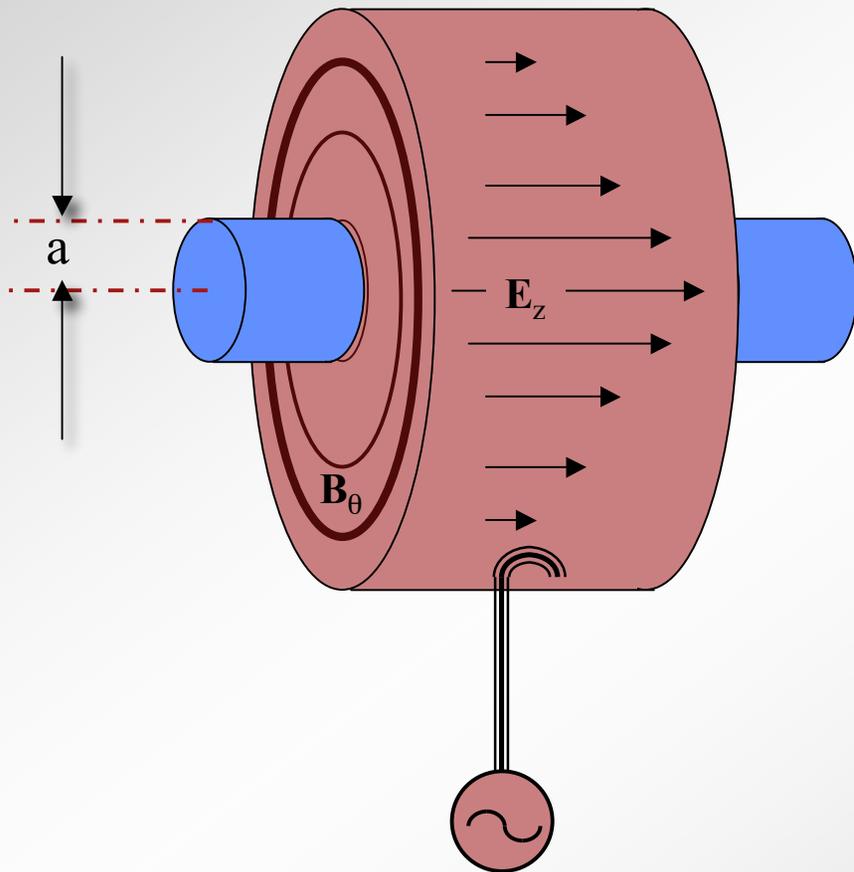
Side view



Choose cavity dimensions to stay far from crossovers



The beam tube makes the field modes (& cell design) more complicated



- ❖ Peak E no longer on axis
 - $E_{pk} \sim 2 - 3 \times E_{acc}$
 - $FOM = E_{pk}/E_{acc}$
- ❖ ω_0 more sensitive to cavity dimensions
 - Mechanical tuning & detuning
- ❖ Beam tubes add length & ϵ 's w/o acceleration
- ❖ Beam induced voltages $\sim a^{-3}$
 - Instabilities

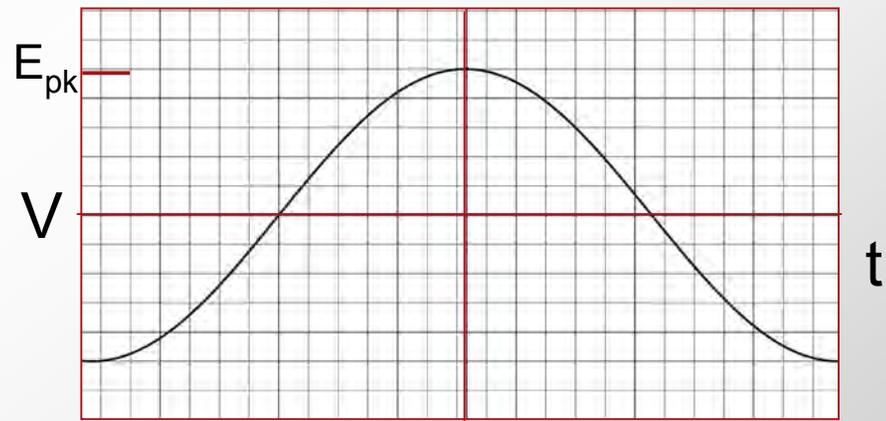
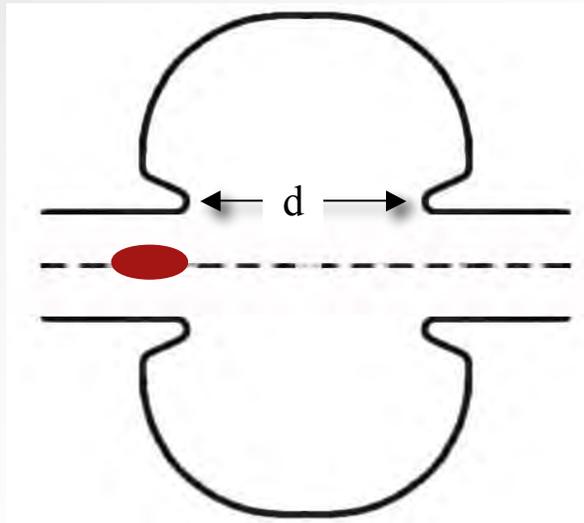
Cavity figures of merit



Figure of Merit: Accelerating voltage

- ❖ The voltage varies during time that bunch takes to cross gap
 - reduction of the peak voltage by Γ (transt time factor)

$$\Gamma = \frac{\sin(\vartheta/2)}{\vartheta/2} \quad \text{where } \vartheta = \omega d / \beta c$$

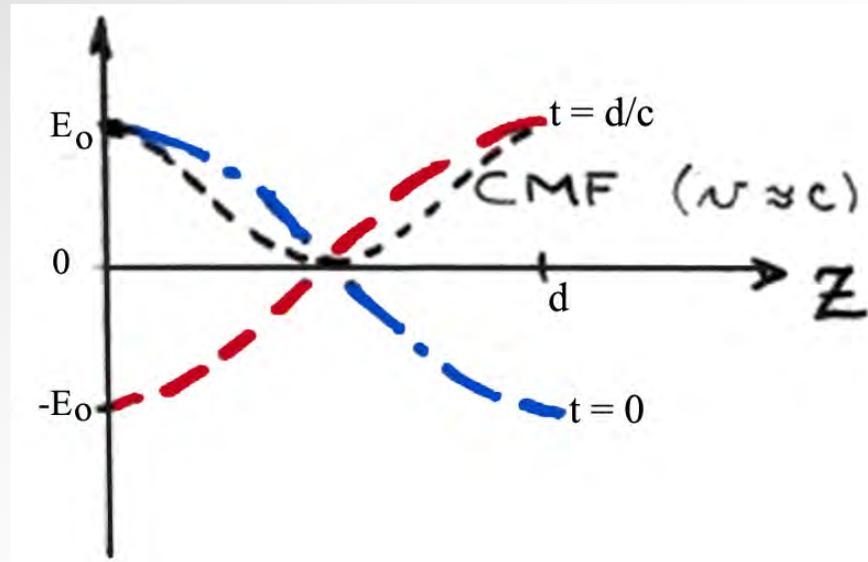


For maximum acceleration

$$T_{\text{cav}} = \frac{d}{c} = \frac{T_{\text{rf}}}{2} \implies \Gamma = 2/\pi$$



Compute the voltage gain correctly



The voltage gain seen by the beam can be computed in the co-moving frame, or we can use the transit-time factor, Γ & compute V at fixed time

$$V_o^2 = \Gamma \int_{z_1}^{z_2} E(z) dz$$



Figure of merit from circuits - Q

$$Q = \frac{\omega_o \circ \text{Energy stored}}{\text{Time average power loss}} = \frac{2\pi \circ \text{Energy stored}}{\text{Energy lost per cycle}}$$

$$\mathcal{E} = \frac{\mu_o}{2} \int_v |H|^2 dv = \frac{1}{2} L I_o I_o^*$$

$$\langle \mathcal{P} \rangle = \frac{R_{surf}}{2} \int_s |H|^2 ds = \frac{1}{2} I_o I_o^* R_{surf}$$

$$R_{surf} = \frac{1}{\text{Conductivity} \circ \text{Skin depth}} \sim \omega^{1/2}$$

$$\therefore Q = \frac{\sqrt{L/C}}{R_{surf}} = \left(\frac{\Delta\omega}{\omega_o} \right)^{-1}$$



Measuring the energy stored in the cavity allows us to measure Q

- ❖ We have computed the field in the fundamental mode

$$\begin{aligned} U &= \int_0^d dz \int_0^b dr 2\pi r \left(\frac{\epsilon E_o^2}{2} \right) J_1^2(2.405r/b) \\ &= b^2 d \left(\epsilon E_o^2 / 2 \right) J_1^2(2.405) \end{aligned}$$

- ❖ To measure Q we excite the cavity and measure the E field as a function of time
- ❖ Energy lost per half cycle = $U\pi Q$
- ❖ Note: energy can be stored in the higher order modes that deflect the beam



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Figure of merit for accelerating cavity: Power to produce the accelerating field

Resistive input (shunt) impedance at ω_0 relates power dissipated in walls to accelerating voltage

$$R_{in} = \frac{\langle V^2(t) \rangle}{\mathcal{P}} = \frac{V_o^2}{2\mathcal{P}} = Q\sqrt{L/C}$$

Linac literature commonly defines “shunt impedance” without the “2”

$$\mathcal{R}_{in} = \frac{V_o^2}{\mathcal{P}} \sim \frac{1}{R_{surf}}$$

Typical values 25 - 50 M Ω



Computing shunt impedance

$$R_{in} = \frac{V_o^2}{\mathcal{P}}$$

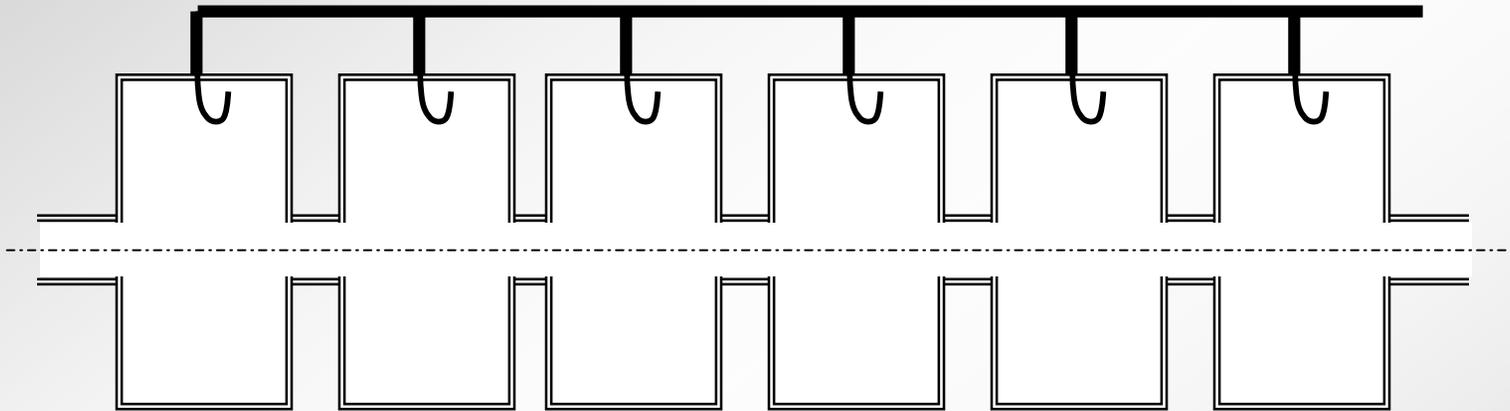
$$\langle \mathcal{P} \rangle = \frac{R_{surf}}{2} \int_s |H|^2 ds$$

$$R_{surf} = \frac{\mu\omega}{2\sigma_{dc}} = \pi Z_o \frac{\delta_{skin}}{\lambda_{rf}} \quad \text{where } Z_o = \sqrt{\frac{\mu_o}{\epsilon_o}} = 377\Omega$$

The on-axis field E and surface H are generally computed with a computer code such as SUPERFISH for a complicated cavity shape



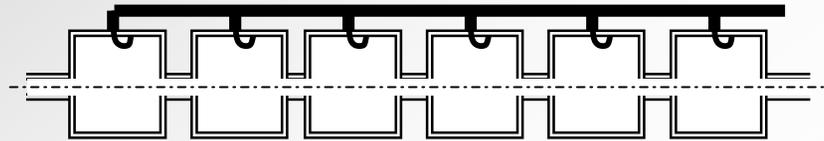
Make the linac out of many pillbox cavities



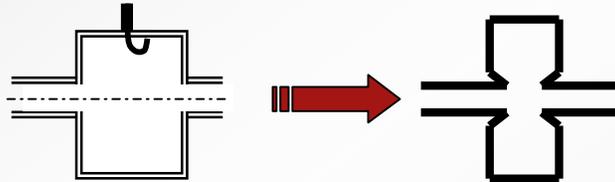
Power the cavities so that $E_z(z,t) = E_z(z)e^{i\omega t}$



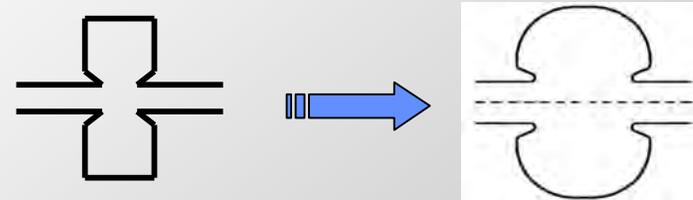
How can we improve on an array of pillboxes?



- ❖ Return to the picture of the re-entrant cavity

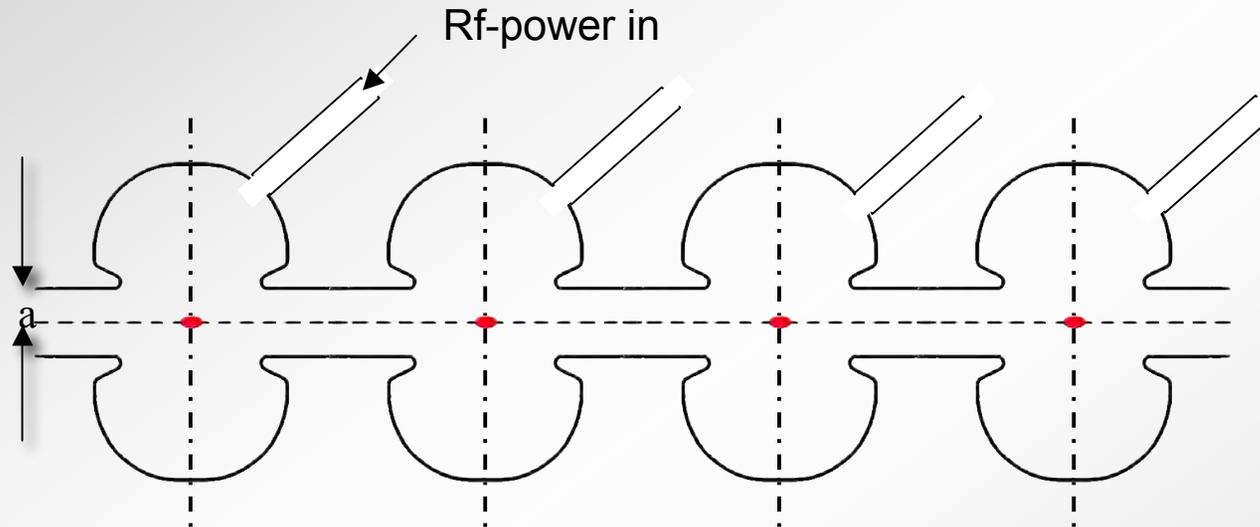


- ❖ Nose cones concentrate E_z near beam for fixed stored energy
- ❖ Optimize nose cone to maximize V^2 ; I.e., maximize R_{sh}/Q
- ❖ Make H-field region nearly spherical; raises Q & minimizes P for given stored energy





Thus, linacs can be considered to be an array of distorted pillbox cavities...



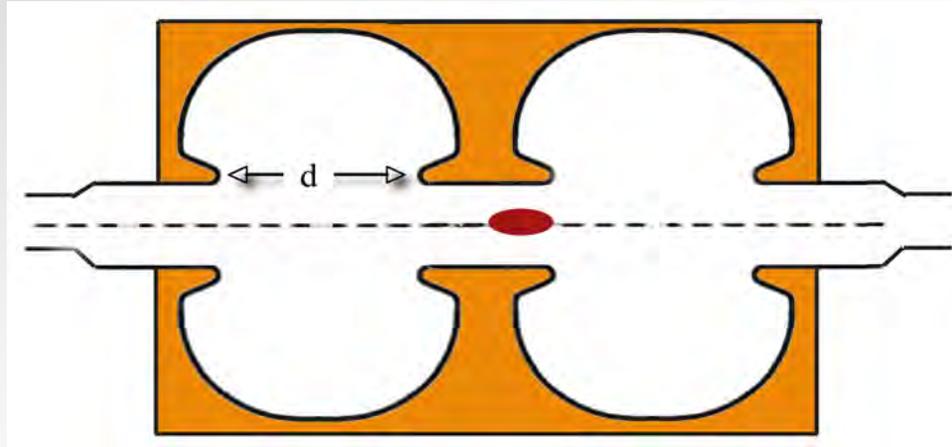
In warm linacs “nose cones” optimize the voltage per cell with respect to resistive dissipation

$$Q = \sqrt{L/C} / \mathcal{R}_{\text{surface}}$$

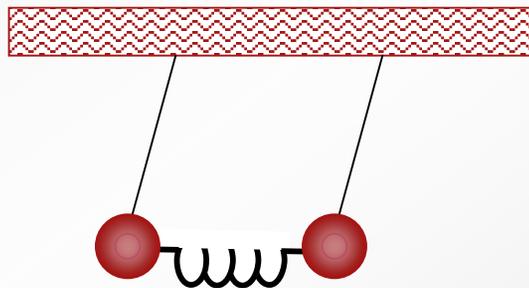
Usually cells are feed in groups not individually.... and



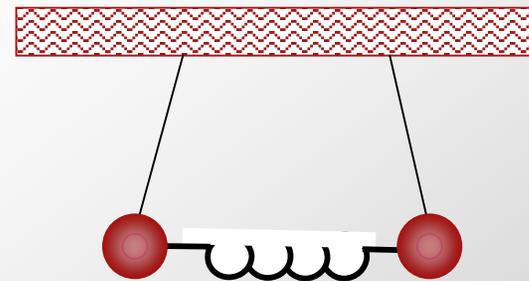
Linacs cells are linked to minimize cost



==> coupled oscillators ==> multiple modes



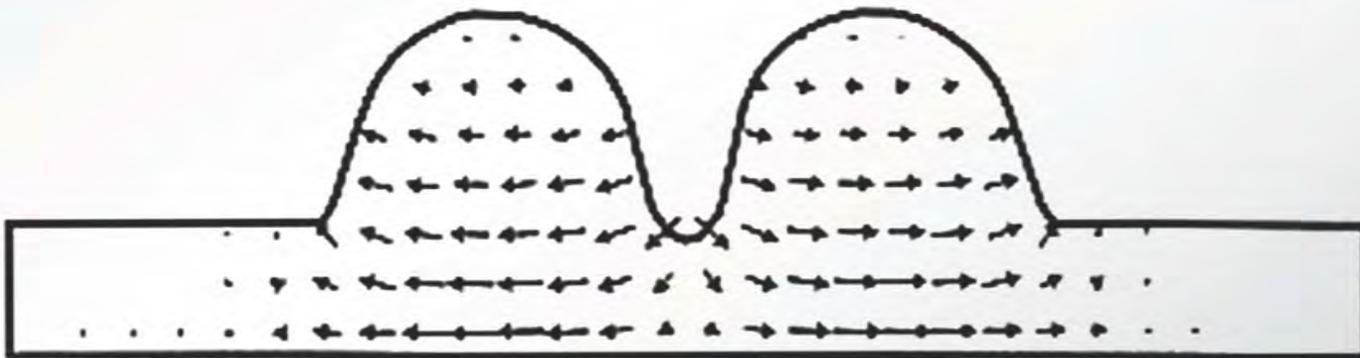
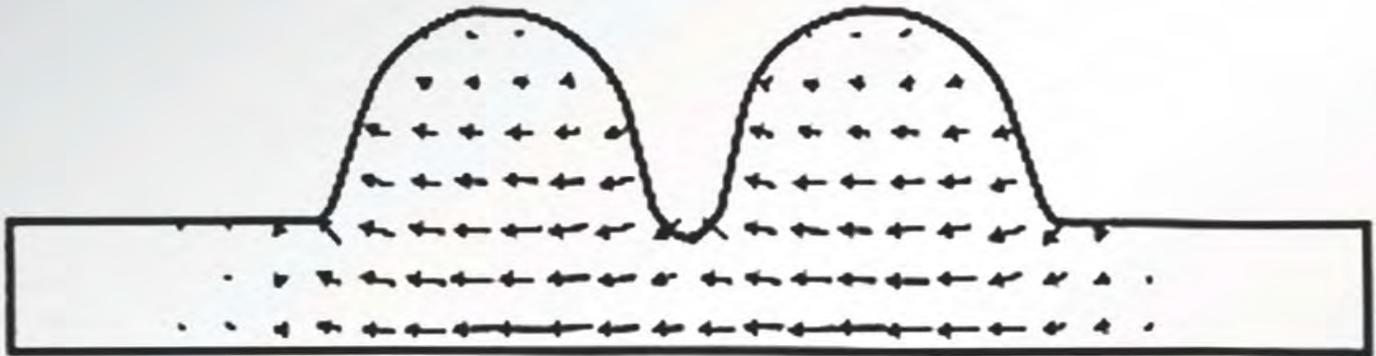
Zero mode



π mode

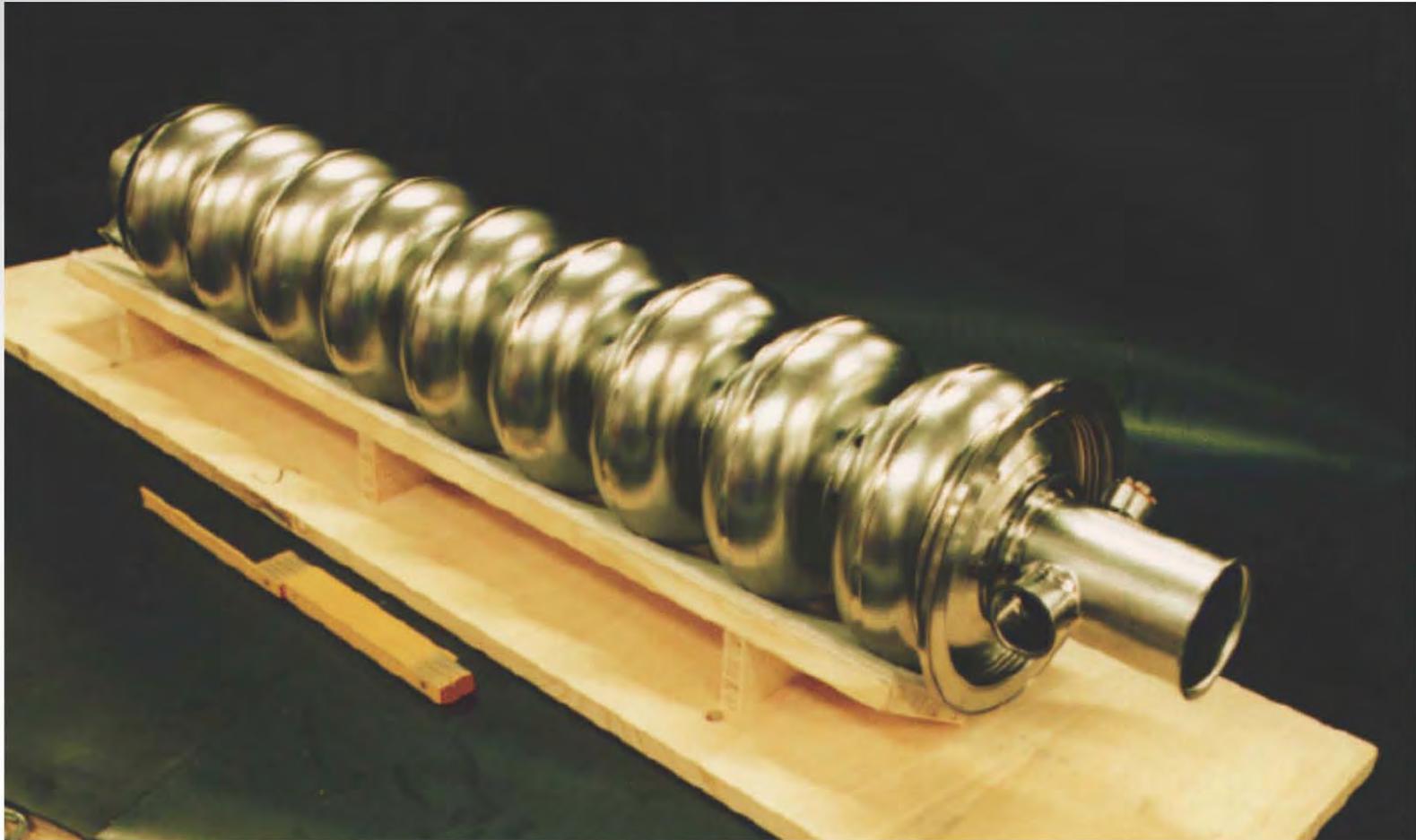


Modes of a two-cell cavity



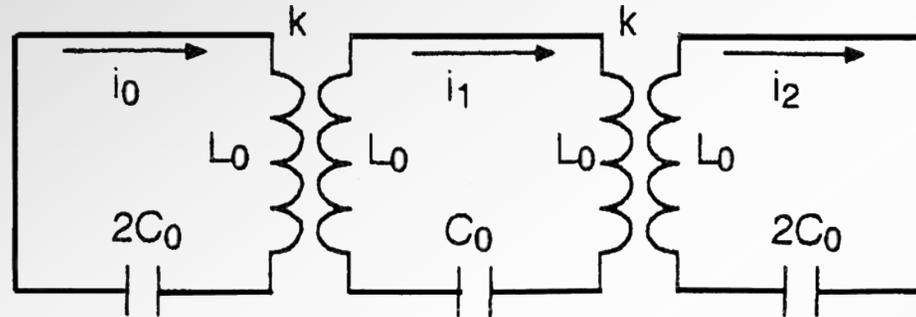


9-cavity TESLA cell





Example of 3 coupled cavities



$$x_0 \left(1 - \frac{\omega_0^2}{\Omega^2} \right) + x_1 k = 0 \quad \text{oscillator } n = 0$$

$$x_1 \left(1 - \frac{\omega_0^2}{\Omega^2} \right) + (x_0 + x_2) \frac{k}{2} = 0 \quad \text{oscillator } n = 1$$

$$x_2 \left(1 - \frac{\omega_0^2}{\Omega^2} \right) + x_1 k = 0 \quad \text{oscillator } n = 2$$

$$x_j = i_j \sqrt{2L_0} \quad \text{and} \quad \Omega = \text{normal mode frequency}$$



Write the coupled circuit equations in matrix form

$$\mathbf{L}\mathbf{x}_q = \frac{1}{\Omega_q^2} \mathbf{x}_q \quad \text{where} \quad \mathbf{L} = \begin{pmatrix} 1/\omega_o^2 & k/\omega_o^2 & 0 \\ k/2\omega_o^2 & 1/\omega_o^2 & k/2\omega_o^2 \\ 0 & k/\omega_o^2 & 1/\omega_o^2 \end{pmatrix} \quad \text{and} \quad \mathbf{x}_q = \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix}$$

- ❖ Compute eigenvalues & eigenvectors to find the three normal modes

$$\text{Mode } q=0: \text{ zero mode} \quad \Omega_0 = \frac{\omega_o}{\sqrt{1+k}} \quad \mathbf{x}_0 = \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

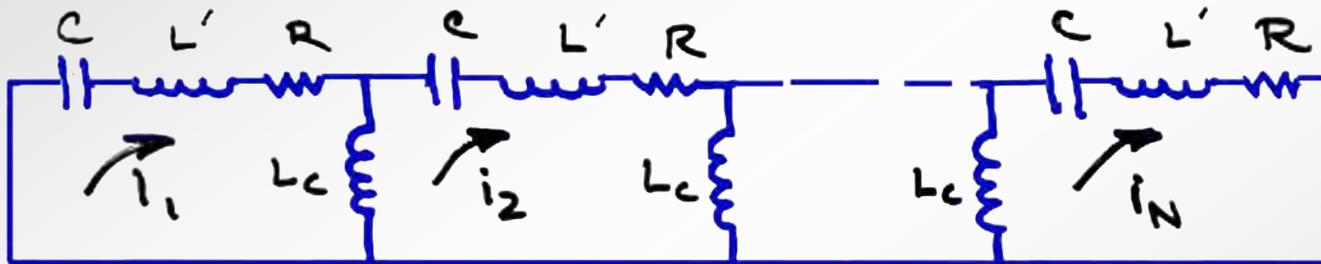
$$\text{Mode } q=1: \pi/2 \text{ mode} \quad \Omega_1 = \omega_o \quad \mathbf{x}_1 = \begin{pmatrix} 1 \\ 0 \\ -1 \end{pmatrix}$$

$$\text{Mode } q=2: \pi \text{ mode} \quad \Omega_2 = \frac{\omega_o}{\sqrt{1-k}} \quad \mathbf{x}_2 = \begin{pmatrix} 1 \\ -1 \\ 1 \end{pmatrix}$$



For a structure with N coupled cavities

- ❖ \implies Set of N coupled oscillators
 - N normal modes, N frequencies
- ❖ From the equivalent circuit with magnetic coupling



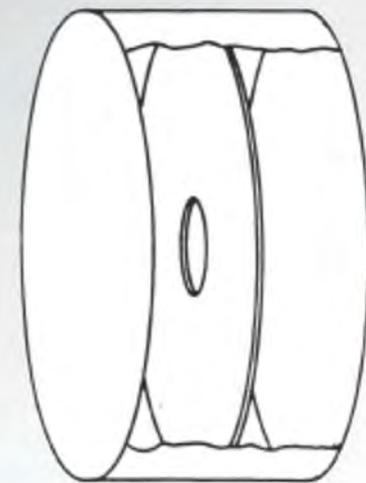
$$\omega_m = \frac{\omega_o}{\left(1 - B \cos \frac{m\pi}{N}\right)^{1/2}} \approx \omega_o \left(1 + B \cos \frac{m\pi}{N}\right)$$

where $B =$ bandwidth (frequency difference between lowest & high frequency mode)

- ❖ Typically accelerators run in the π -mode

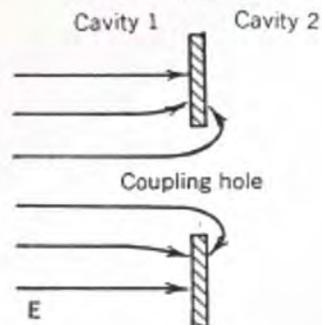


Magnetically coupled pillbox cavities



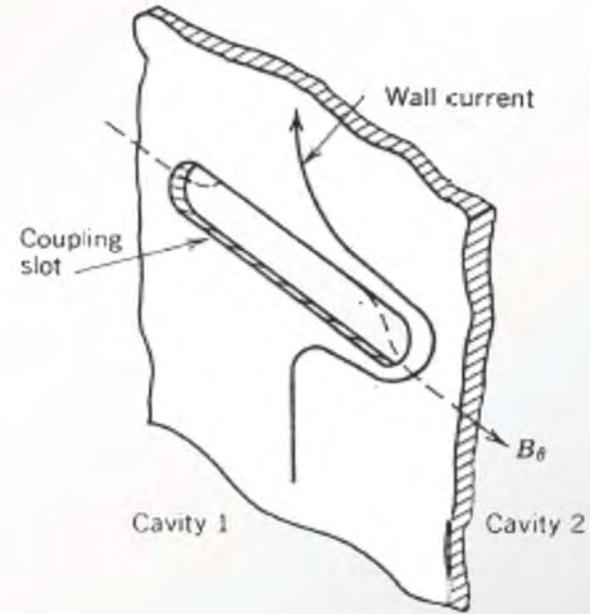
Cavity 1 Cavity 2

(a)



Cavity 1 Cavity 2

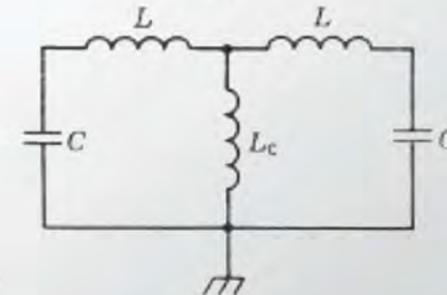
(c)



Cavity 1

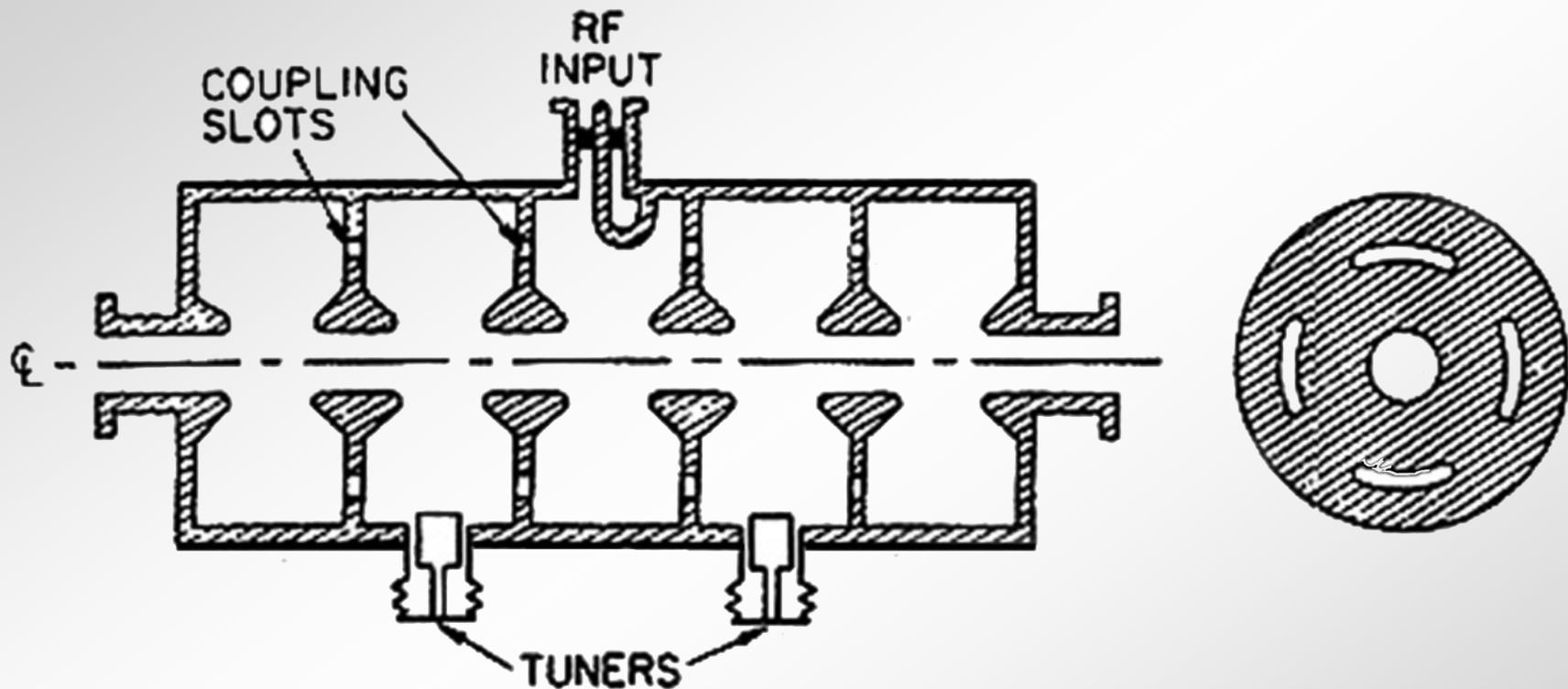
Cavity 2

(d)





5-cell π -mode cell with magnetic coupling

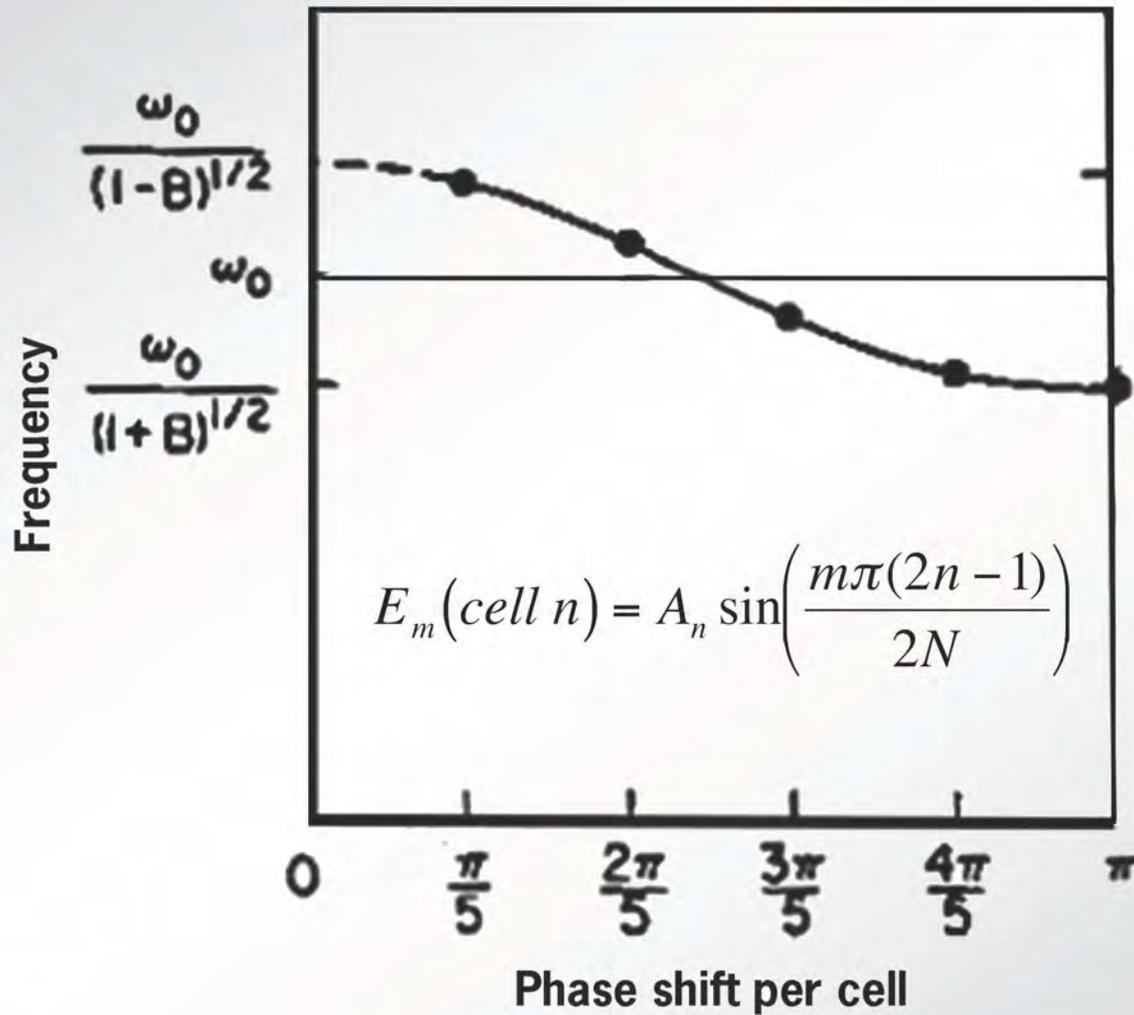


The tuners change the frequencies by perturbing wall currents \implies changes the inductance \implies changes the energy stored in the magnetic field

$$\frac{\Delta\omega_o}{\omega_o} = \frac{\Delta U}{U}$$

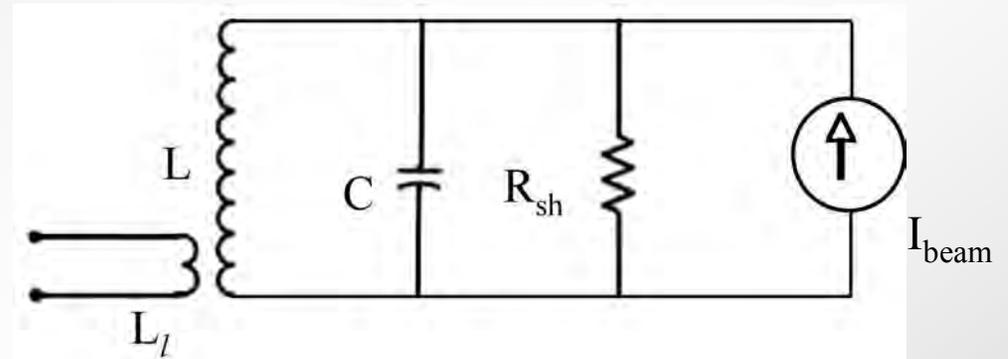
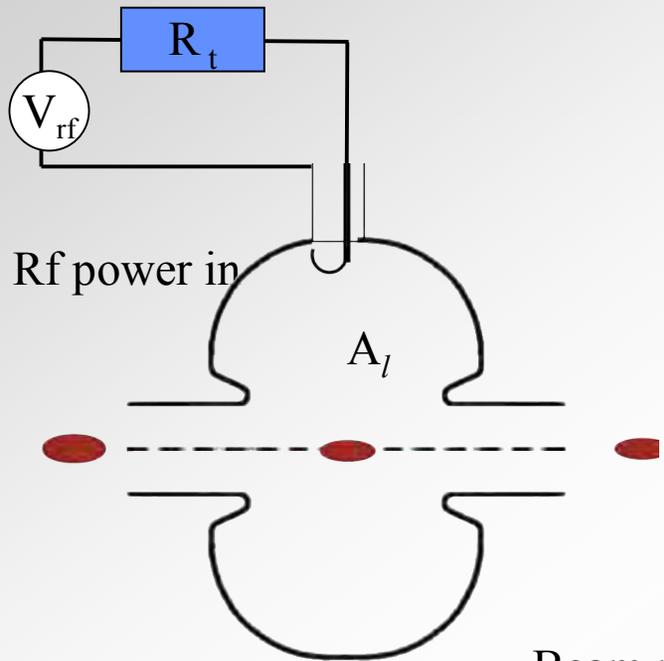


Dispersion diagram for 5-cell structure



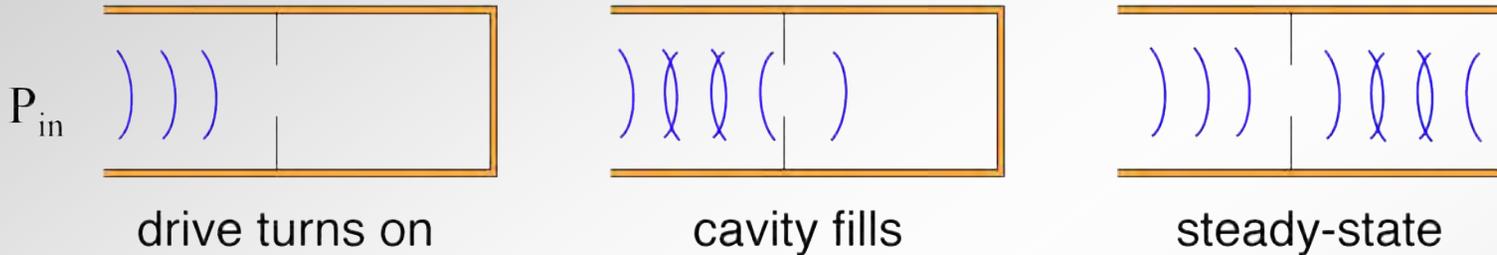


Power exchange with resonant cavities





Effects of wall-losses & external coupling on stored energy, U



- ❖ Define “wall quality factor”, Q_w , & “external” quality factor, Q_e
- ❖ Power into the walls is $P_w = \omega U / Q_w$.
- ❖ If P_{in} is turned off, then the power flowing out $P_e = \omega U / Q_e$
- ❖ Net rate of energy loss = $\omega U / Q_w + \omega U / Q_e = \omega U / Q_{loaded}$



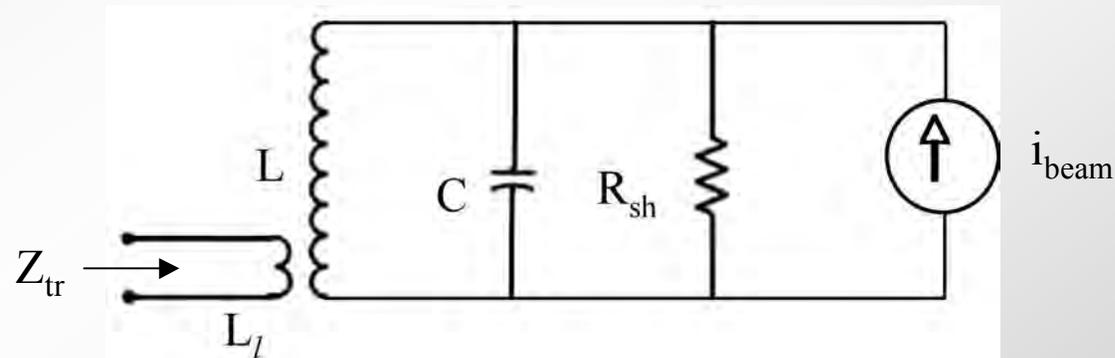
Till time & coupling

- ❖ Loaded fill time

$$T_{\text{fill}} = 2Q_L/\omega$$

- ❖ Critically coupled cavity: $P_{\text{in}} = P_{\text{w}} \implies 1/Q_e = 1/Q_w$

- ❖ In general, the coupling parameter $\beta = Q_w / Q_e$





Effects of the rf source & beam at resonance

- ❖ Voltage produced by the generator is

$$V_{gr} = \frac{2\sqrt{\beta}}{1 + \beta} \cdot \sqrt{R_{shunt} P_{gen}}$$

- ❖ The voltage produced by the beam is

$$V_{b,r} = \frac{i_{beam}}{Z_{tr}(1 + \beta)} \approx \frac{I_{dc} R_{shunt}}{(1 + \beta)}$$



Effects of the rf source & beam at resonance

- ❖ The accelerating voltage is the sum of these effects

$$V_{accel} = \sqrt{R_{shunt} P_{gen}} \left[\frac{2\sqrt{\beta}}{1+\beta} \left(1 - \frac{K}{\sqrt{\beta}} \right) \right] = \sqrt{R_{shunt} P_{wall}}$$

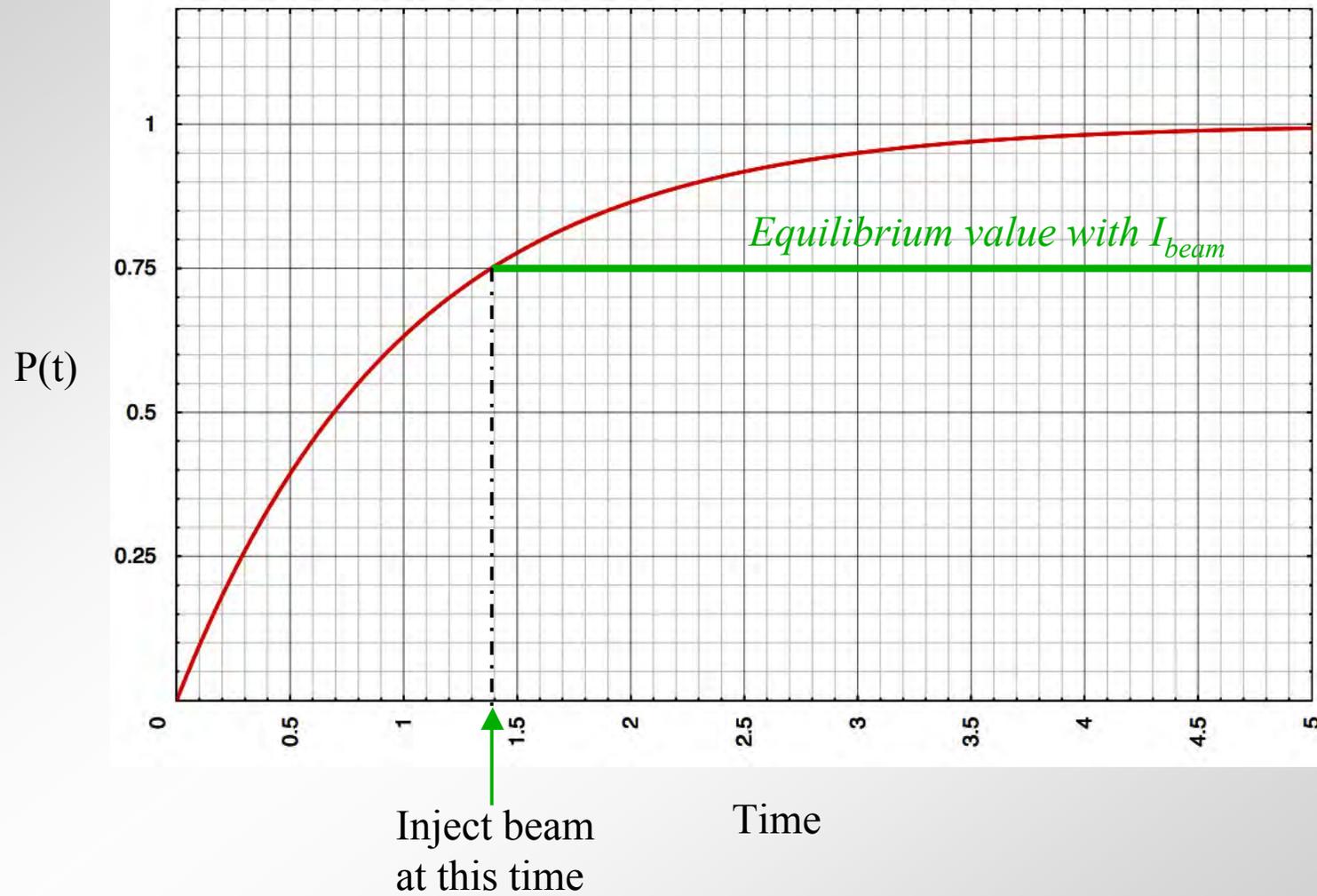
where $K = \frac{I_{dc}}{2} \sqrt{\frac{R_{shunt}}{P_{gen}}}$ is the "loading factor"

- ❖ $\implies V_{acc}$ decreases linearly with increasing beam current





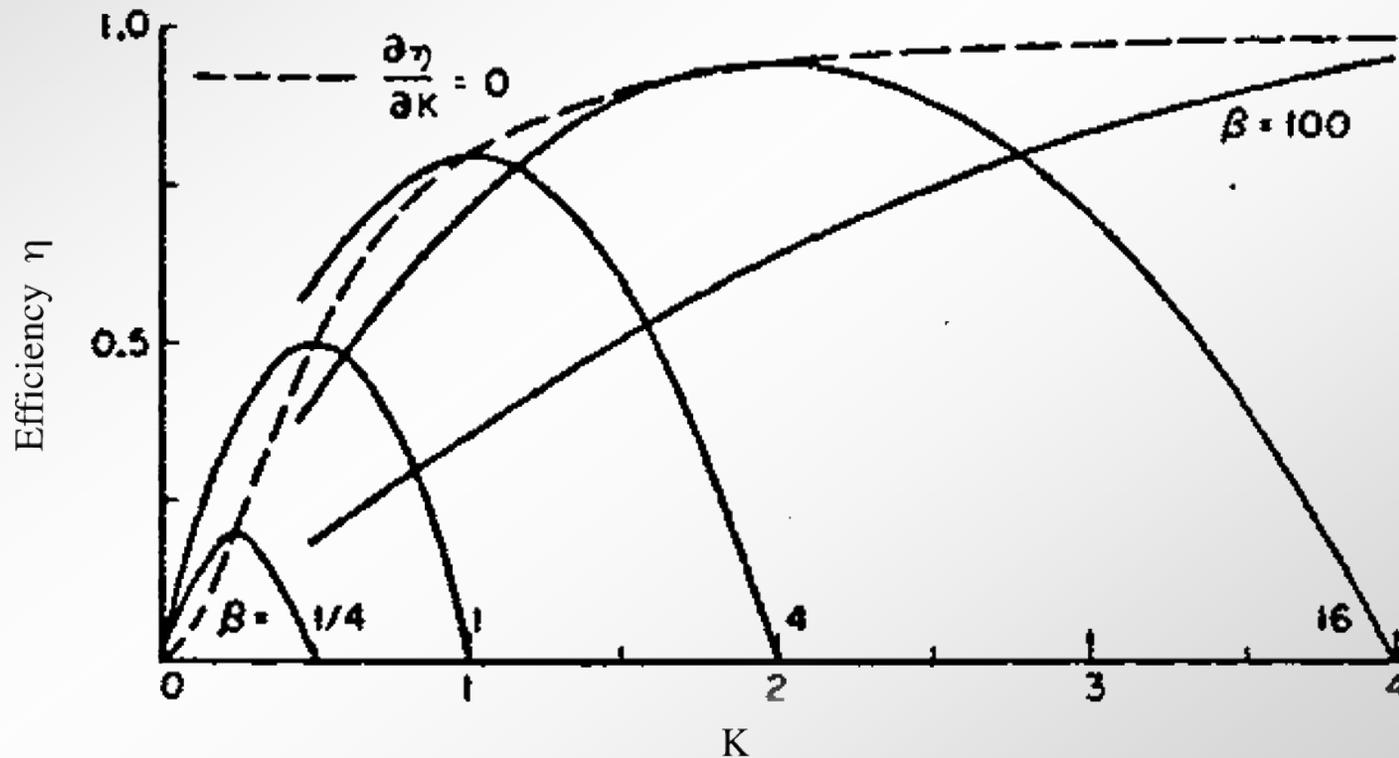
Power flow in standing wave linac





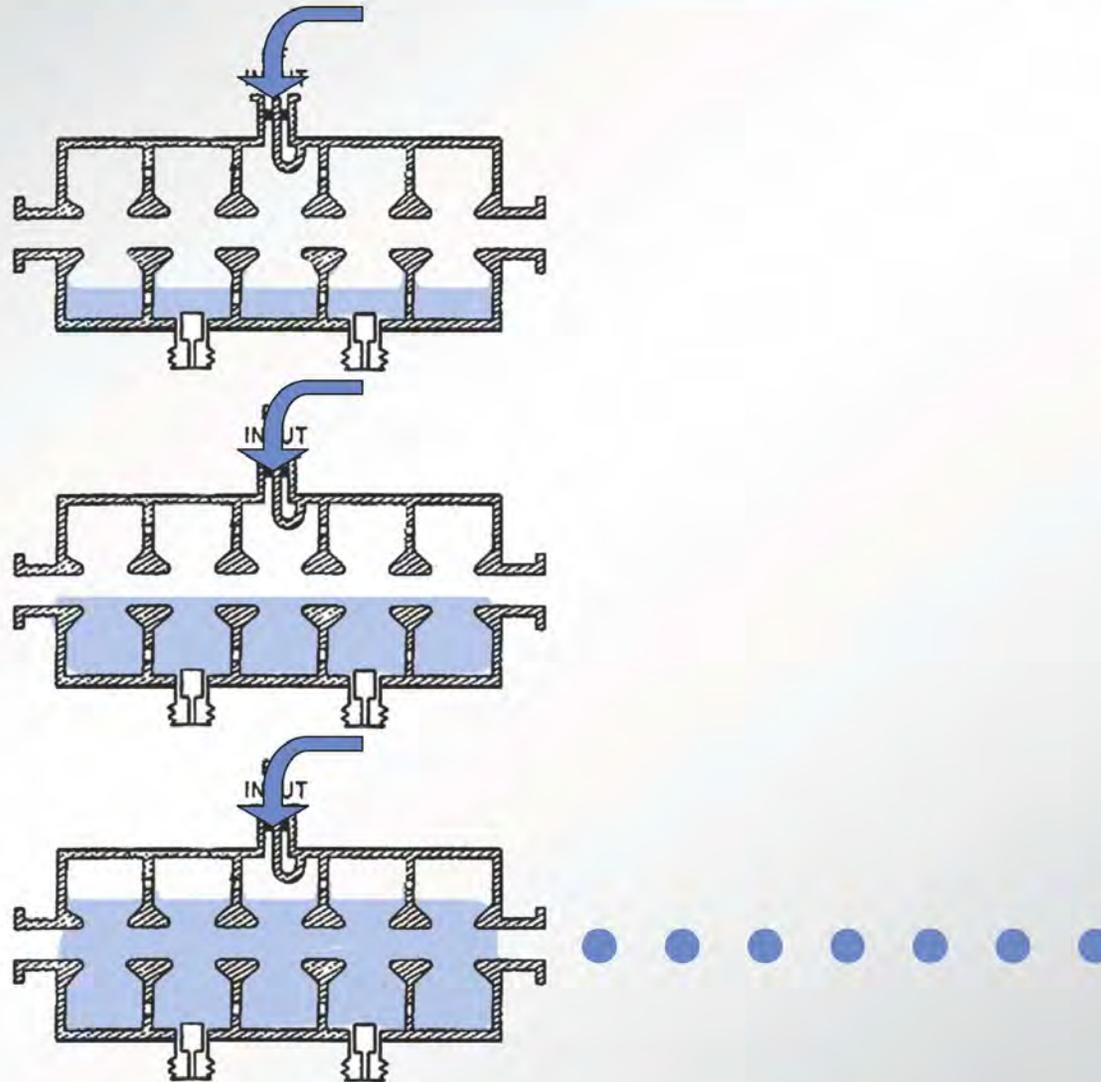
Efficiency of the standing wave linac

$$\eta = \frac{I_{dc} V_{acc}}{P_{gen}} = \frac{2\sqrt{\beta}}{1+\beta} \left[2K \left(1 - \frac{K}{\sqrt{\beta}} \right) \right]$$





Schematic of energy flow in a standing wave structure



What makes SC RF attractive?



Comparison of SC and NC RF

Superconducting RF

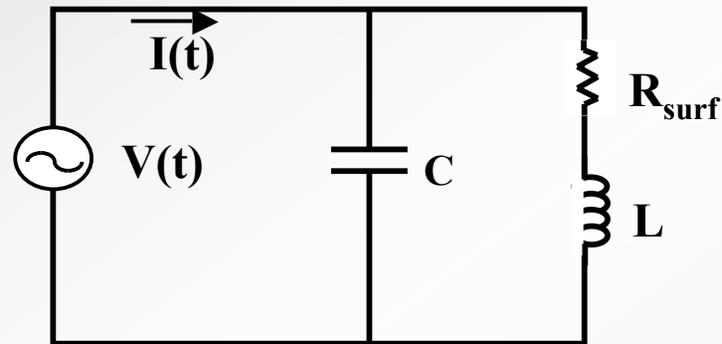
- ❖ High gradient
==> 1 GHz, meticulous care
- ❖ Mid-frequencies
==> Large stored energy, \mathcal{E}_s
- ❖ Large \mathcal{E}_s
==> very small $\Delta E/E$
- ❖ Large Q
==> high efficiency

Normal Conductivity RF

- ❖ High gradient
==> high frequency (5 - 17 GHz)
- ❖ High frequency
==> low stored energy
- ❖ Low \mathcal{E}_s
==> $\sim 10x$ larger $\Delta E/E$
- ❖ Low Q
==> reduced efficiency



Recall the circuit analog



As $R_{surf} \implies 0$, the $Q \implies \infty$.

In practice,

$$Q_{nc} \sim 10^4$$

$$Q_{sc} \sim 10^{11}$$



Figure of merit for accelerating cavity: Power to produce the accelerating field

Resistive input (shunt) impedance at ω_0 relates power dissipated in walls to accelerating voltage

$$R_{in} = \frac{\langle V^2(t) \rangle}{\mathcal{P}} = \frac{V_o^2}{2\mathcal{P}} = Q\sqrt{L/C}$$

Linac literature more commonly defines “shunt impedance” without the “2”

$$\mathcal{R}_{in} = \frac{V_o^2}{\mathcal{P}} \sim \frac{1}{R_{surf}}$$

For SC-rf \mathcal{P} is reduced by orders of magnitude

BUT, it is deposited @ 2K

Traveling wave linacs



Electromagnetic waves

From Maxwell equations, we can derive

$$\nabla^2 E_i = \frac{\partial^2 E_i}{\partial x^2} + \frac{\partial^2 E_i}{\partial y^2} + \frac{\partial^2 E_i}{\partial z^2} = \frac{1}{c^2} \frac{\partial^2 E_i}{\partial t^2} \quad i = x, y, z$$

for electromagnetic waves in free space (no charge or current distributions present).

The plane wave is a particular solution of the EM wave equation

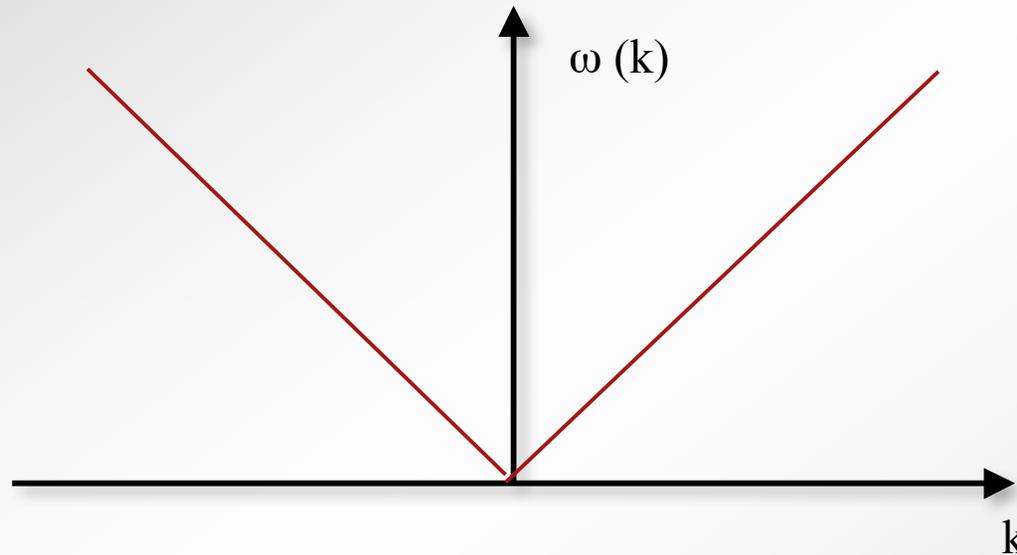
$$\bar{E} = \bar{E}_o e^{i(\omega t - ks)} = \bar{E}_o \left[\underbrace{\cos(\omega t - ks) + i \sin(\omega t - ks)}_{\text{Phase of the wave} = \phi} \right]$$

when

$$\omega = c k$$



Dispersion (Brillouin) diagram: monochromatic plane wave



The phase of this plane wave is constant for

$$\frac{d\phi}{dt} = \omega - k \frac{ds}{dt} \equiv \omega - kv_{ph} = 0$$

or

$$v_{ph} = \frac{\omega}{k} = c$$



Plane wave representation of EM waves

- ❖ In more generality, we can represent an arbitrary wave as a sum of plane waves:

$$\bar{E} = \sum_{n=-\infty}^{\infty} \bar{E}_{no} e^{i(n\omega_0 t - ks)}$$

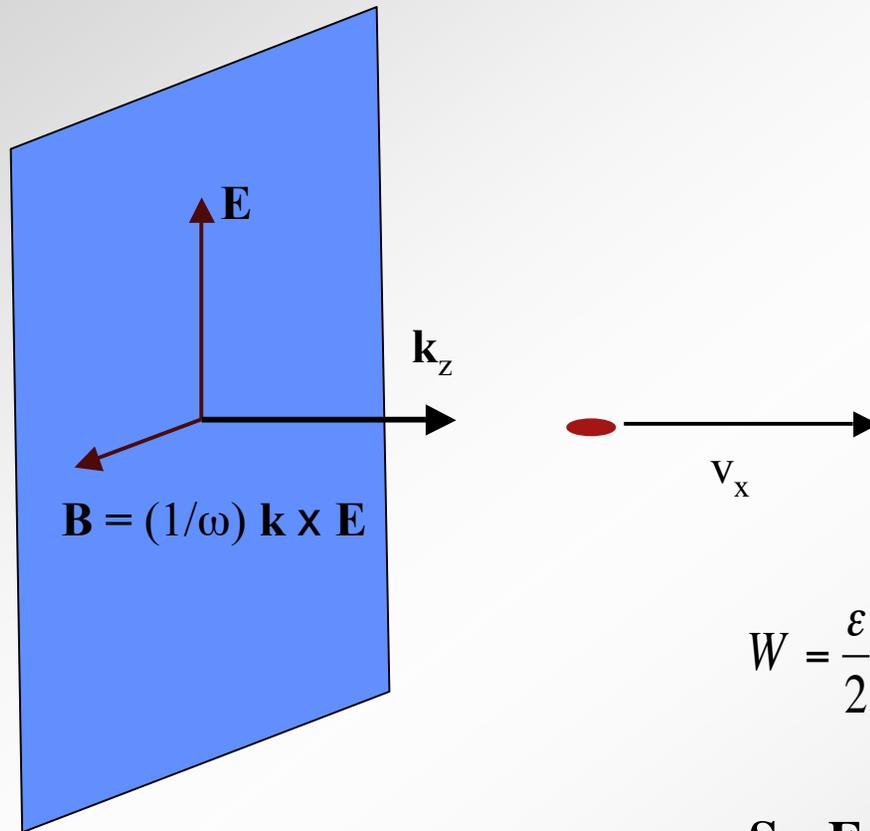
Periodic Case

$$\bar{E} = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} dt f(\omega) e^{i(\omega t - ks)}$$

Non-periodic Case



Exercise: Can the plane wave accelerate the particle in the x-direction?



$$W = \frac{\epsilon}{2} \left(E^2 + \frac{1}{\epsilon\mu} B^2 \right) = \frac{\epsilon}{2} \left(E^2 + c^2 B^2 \right) = \epsilon E^2$$

$$\mathbf{S} = \mathbf{E} \times \mathbf{H} = \frac{1}{\mu} \mathbf{E} \times \mathbf{B} = \frac{1}{\mu c} E^2 = \sqrt{\frac{\epsilon}{\mu}} E^2$$



Can accelerating structures be smooth waveguides?

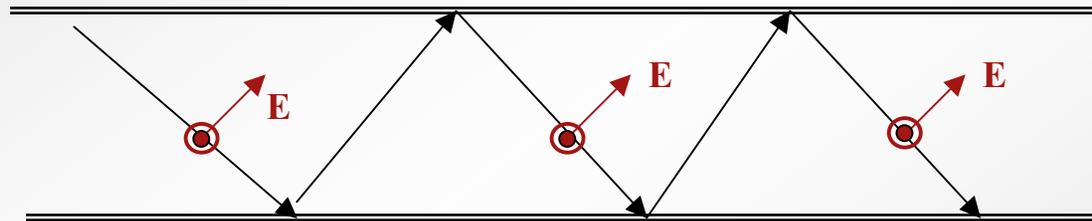
- ❖ Assume the answer is “yes”
- ❖ Then $\mathbf{E} = \mathbf{E}(r, \theta) e^{i(\omega t - kz)}$ with $\omega/k = v_{ph} < c$
- ❖ Transform to the frame co-moving at $v_{ph} < c$
- ❖ Then,
 - The structure is unchanged (by hypothesis)
 - \mathbf{E} is static (v_{ph} is zero in this frame)
 - ==> By Maxwell's equations, $\mathbf{H} = 0$
 - ==> $\nabla \circ \mathbf{E} = 0$ and $\mathbf{E} = -\nabla \phi$
 - But ϕ is constant at the walls (metallic boundary conditions)
 - ==> $\mathbf{E} = 0$

The assumption is false, smooth structures have $v_{ph} > c$



We need a longitudinal E-field to accelerate particles in vacuum

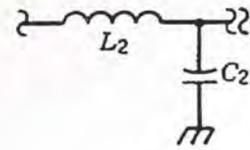
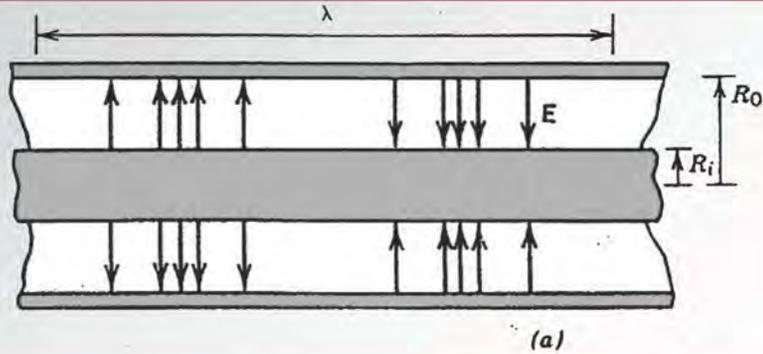
- ❖ Example: the standing wave structure in a pillbox cavity
- ❖ What about traveling waves?
 - Waves guided by perfectly conducting walls can have E_{long}



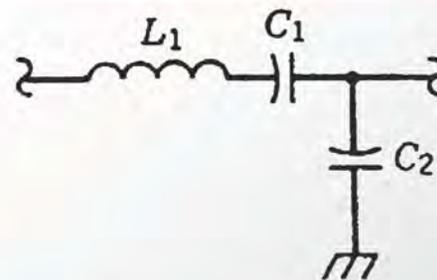
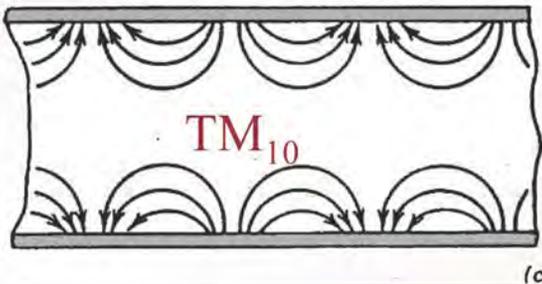
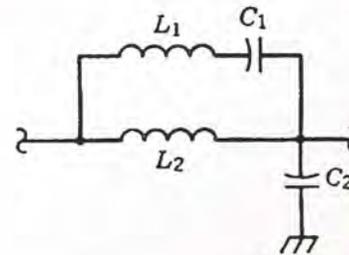
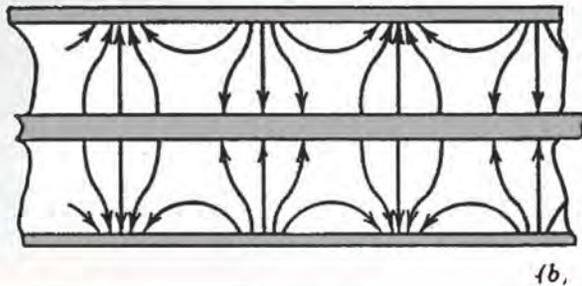
- ❖ But first, think back to phase stability
 - To get continual acceleration the wave & the particle must stay in phase
 - Therefore, we can accelerate a charge with a wave with a synchronous phase velocity, $v_{\text{ph}} \approx v_{\text{particle}} < c$



Propagating modes & equivalent circuits



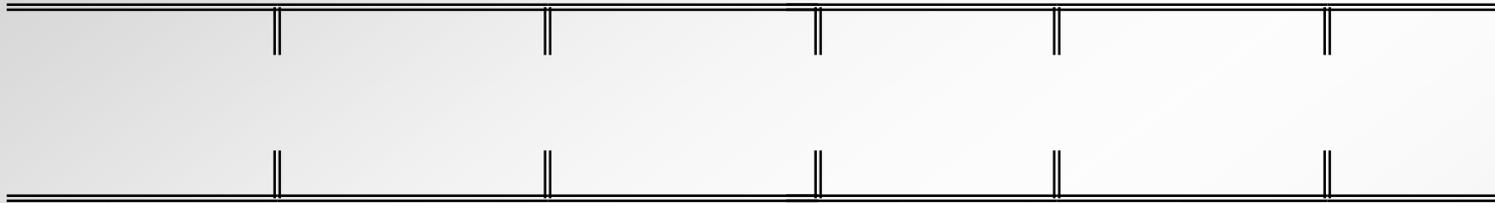
All frequencies can propagate



Propagation is cut-off at low frequencies



To slow the wave, add irises



In a transmission line the irises

- a) Increase capacitance, C
- b) Leave inductance \sim constant
- c) \implies lower impedance, Z
- d) \implies lower v_{ph}

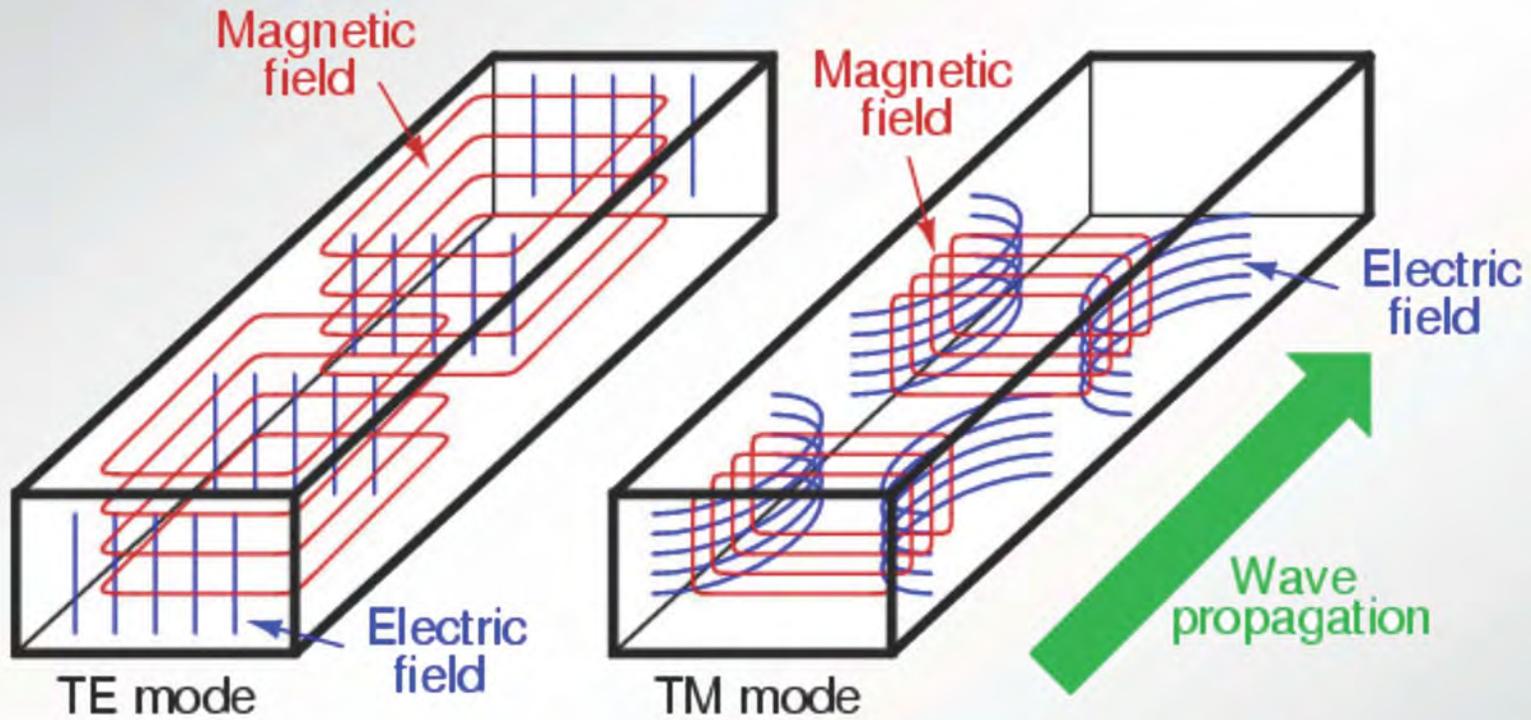
$$\frac{\omega}{k} = \frac{1}{\sqrt{LC}}$$

$$Z = \frac{L}{C}$$

Similar for TM₀₁ mode in the waveguide



Fields in waveguides



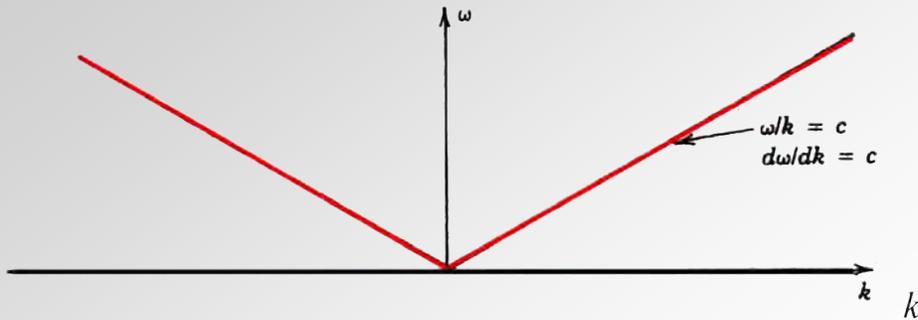
Magnetic flux lines appear as continuous loops
Electric flux lines appear with beginning and end points

Figure source: www.opamp-electronics.com/tutorials/waveguide

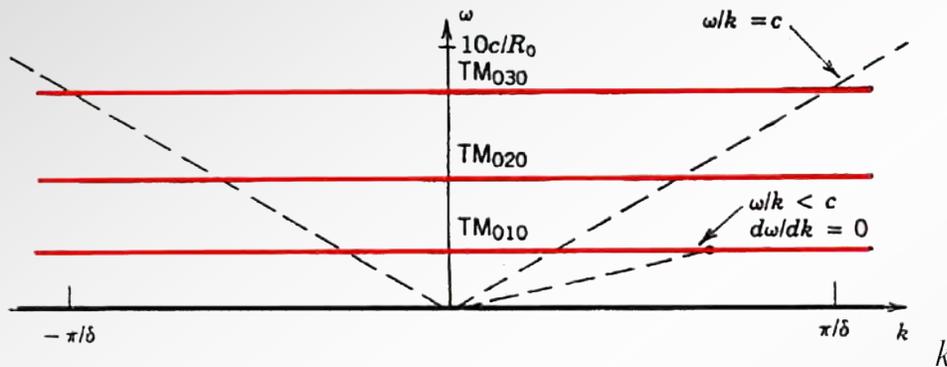
Lessons In Electric Circuits copyright (C) 2000-2002 Tony R. Kuphaldt



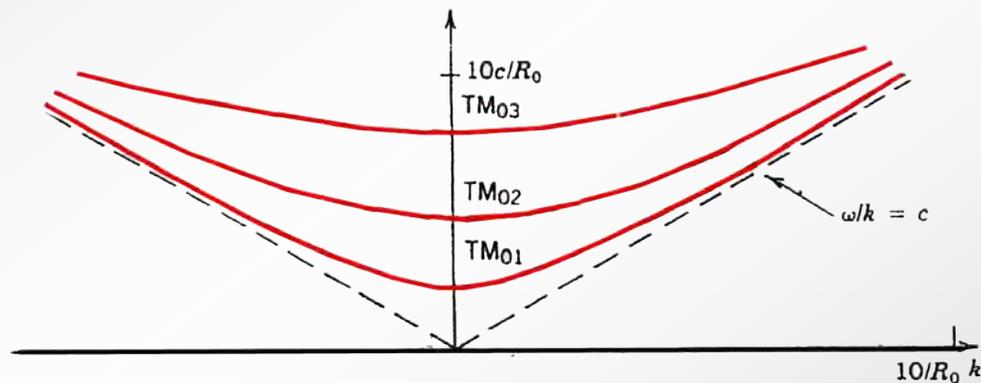
Dispersion diagrams



Transmission line
TEM mode



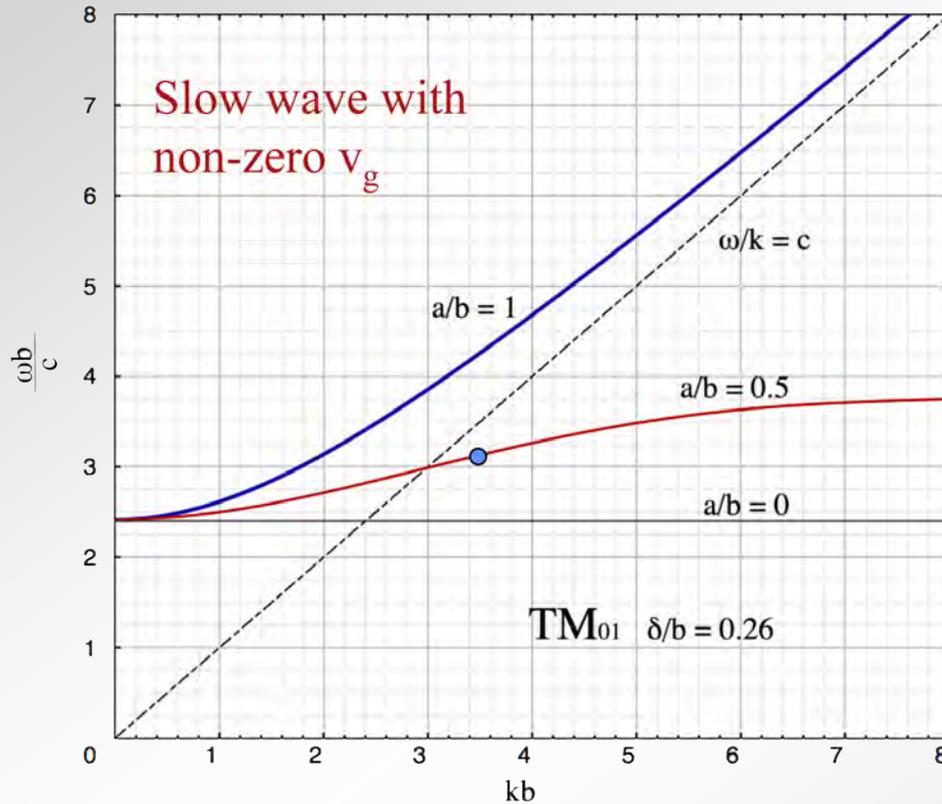
Weakly coupled pillboxes
 TM_{0n0} modes



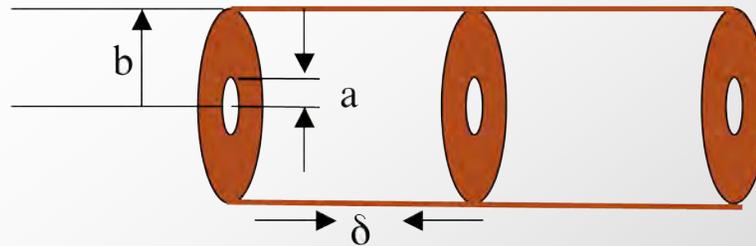
Smooth waveguide,
 TM_{0n} modes



Dispersion relation for SLAC structure



Small changes in a
lead to large
reduction
in v_g





Notation

$\beta_g = v_g/c =$ Relative group velocity

$E_a =$ Accelerating field (MV/m)

$E_s =$ Peak surface field (MV/m)

$P_d =$ Power dissipated per length (MW/m)

$P_t =$ Power transmitted (MW/m)

$w =$ Stored energy per length (J/m)



Structure parameters for TW linacs

$$r_{shunt} = \frac{E_a^2}{\left| \frac{dP_t}{dz} \right|} \quad (\text{M}\Omega/\text{m})$$

$$Q = \frac{w\omega}{\left| \frac{dP_t}{dz} \right|}$$

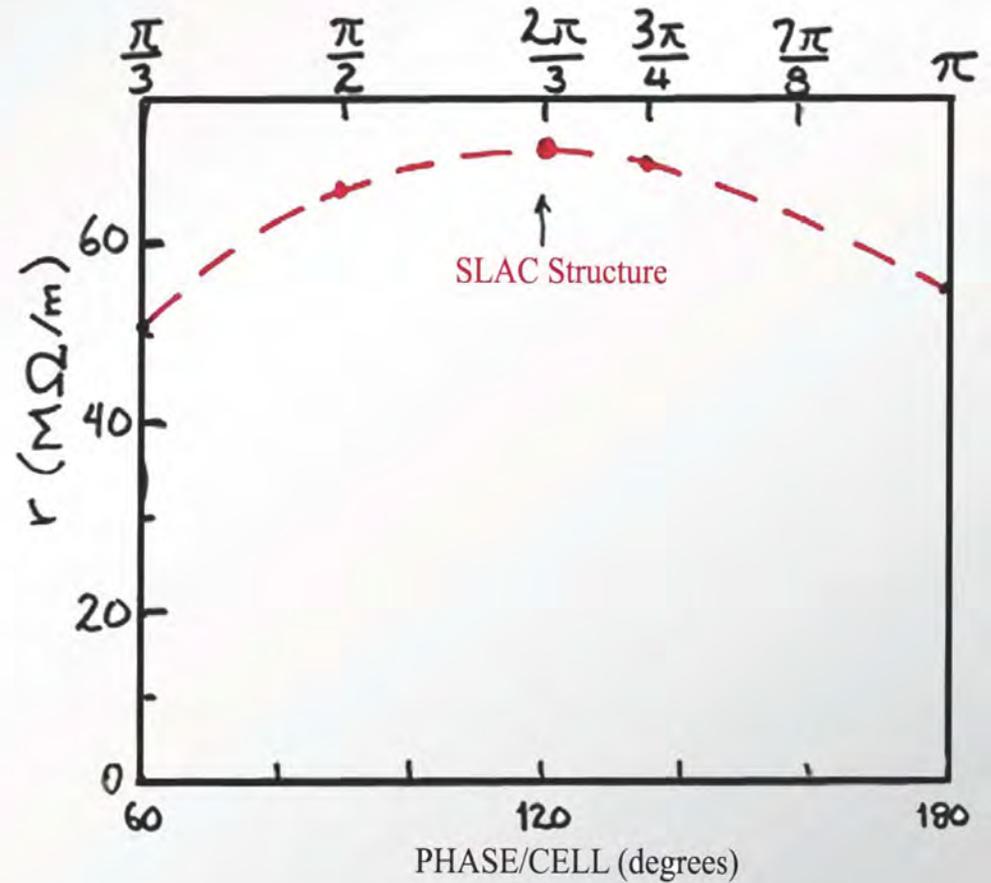
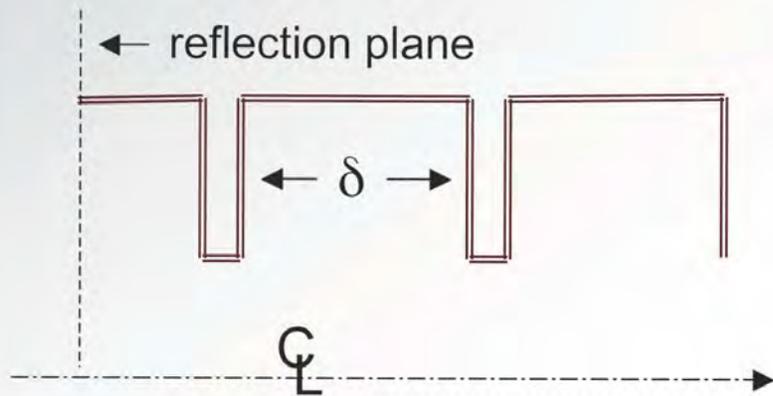
$$\frac{r_{shunt}}{Q} = \frac{E_a^2}{w\omega}$$

$$s = \frac{E_a^w}{w} = \text{Elastance} \quad (\text{M}\Omega/\text{m}/\mu\text{s})$$

W_{acc} = energy/length for acceleration



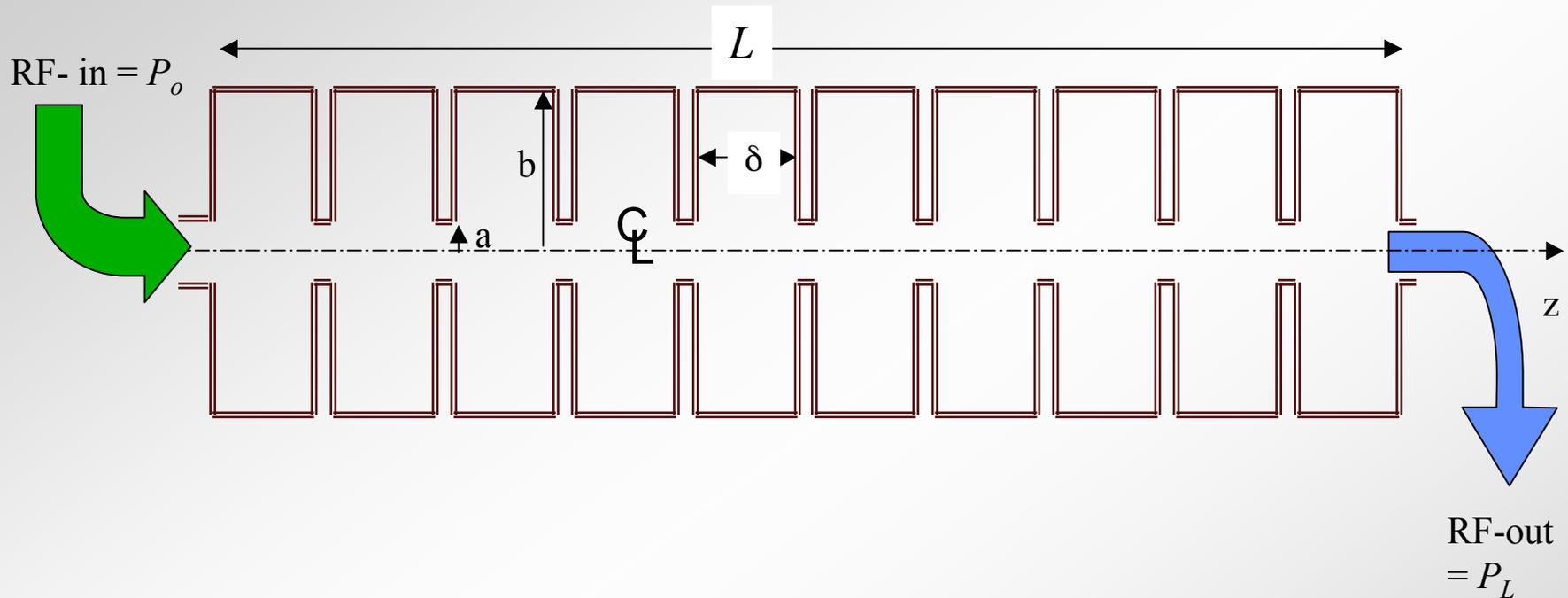
Variation of shunt impedance with cell length



Calculations by D. Farkas (SLAC)



The constant geometry structure

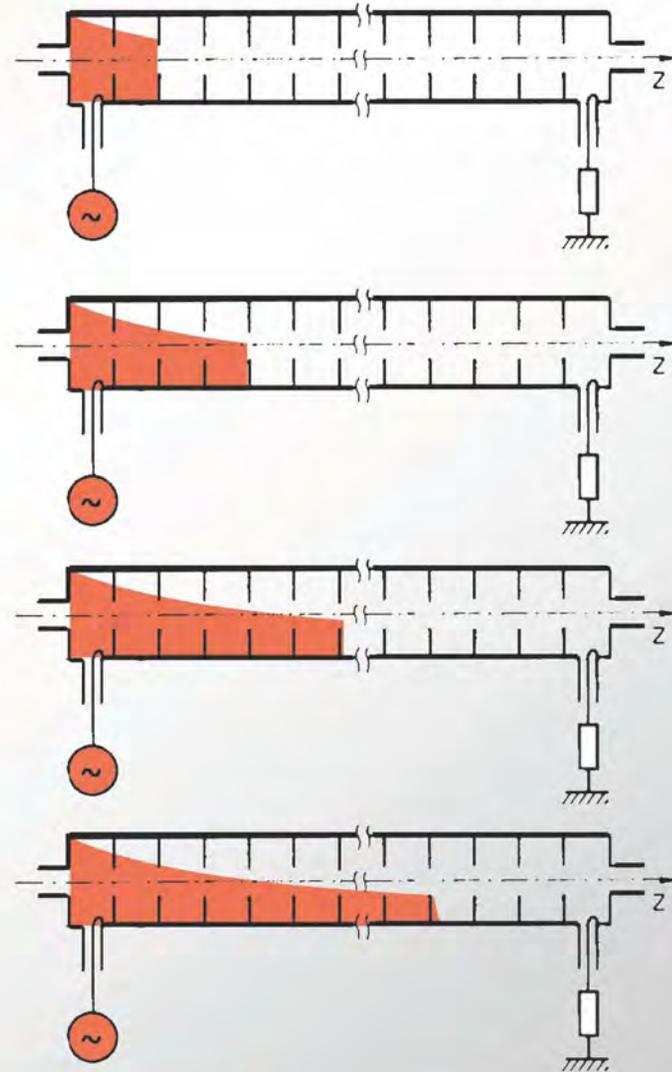
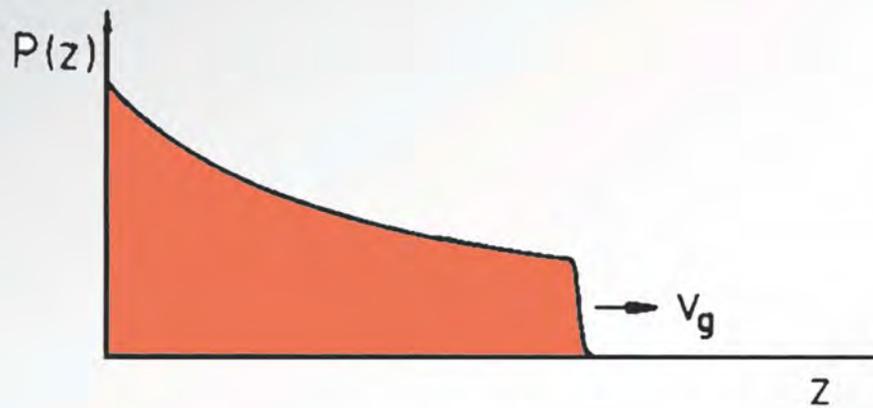


In a structure with a constant geometry,
the inductance & capacitance per unit length are constant

\implies **constant impedance structure**



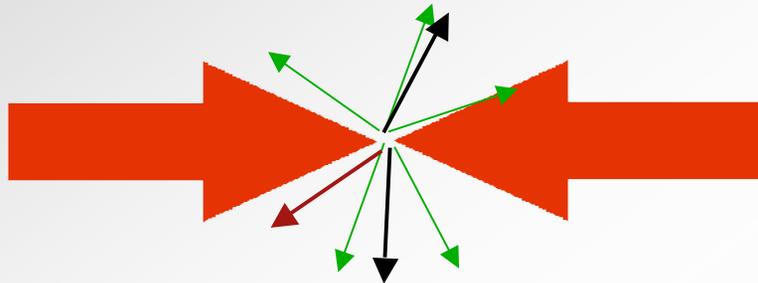
Filling the traveling wave linac





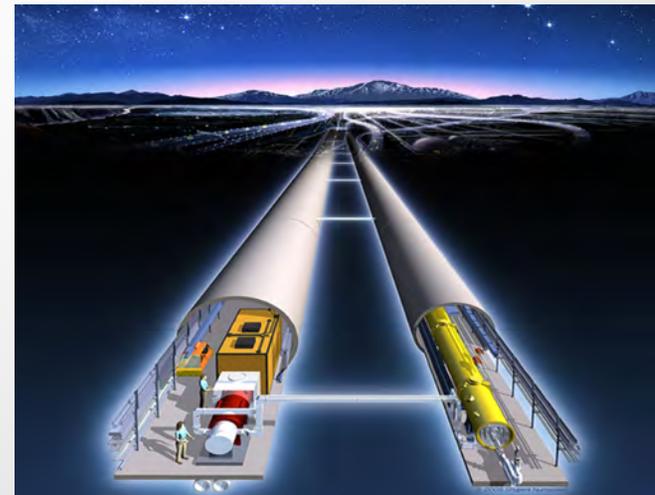
Why do we need beams?

Collide beams



FOMs: Collision rate, energy stability, Accelerating field

Examples: LHC, ILC, RHIC





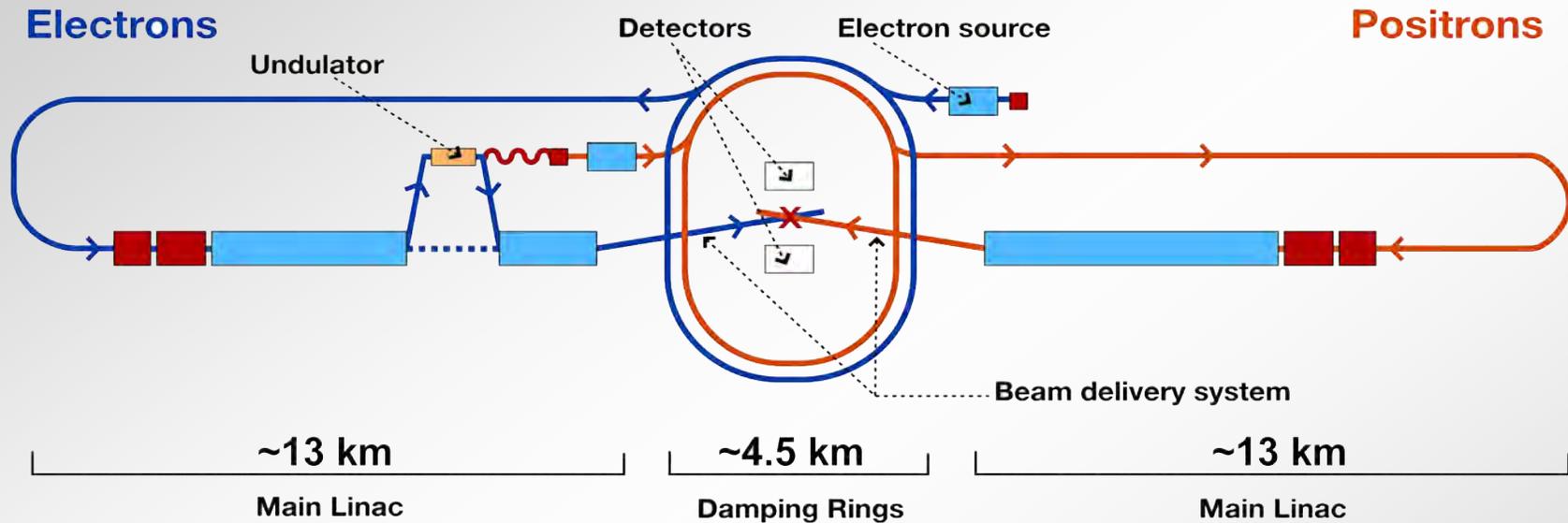
In LHC storage rings...

- ❖ Limited space & Large rf trapping of particles
 - V/cavity must be high
- ❖ Bunch length must be large (≤ 1 event/cm in luminous region)
 - RF frequency must be low
- ❖ Energy lost in walls must be small
 - R_{surf} must be small

SC cavities were the only practical choice



For ILC, SC rf provides high power, low ϵ beams at high efficiency

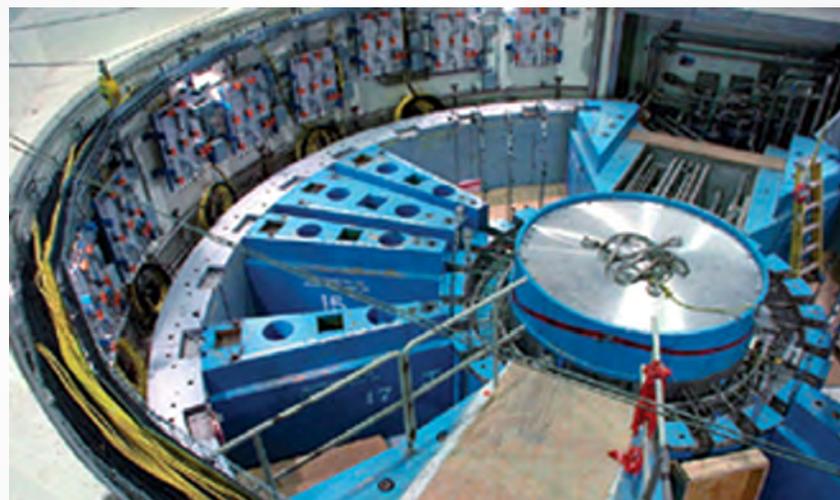
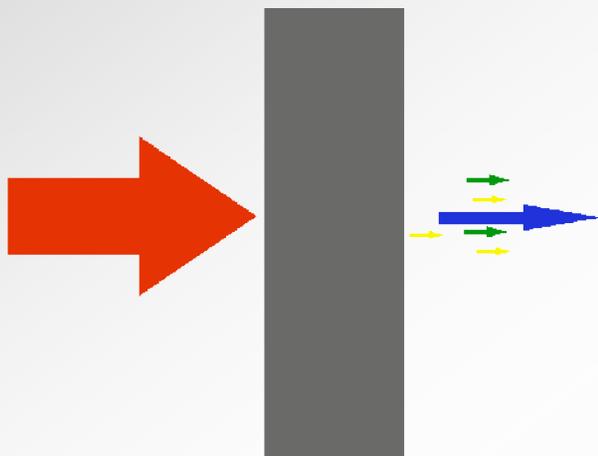


- **To deliver required luminosity (500 fb^{-1} in 4 years) \implies**
 - powerful polarized electron & positron beams (11 MW /beam)
 - tiny beams at collision point \implies minimizing beam-structure interaction
- **To limit power consumption \implies high “wall plug” to beam power efficiency**
 - Even with SC rf, the site power is still 230 MW !



Why do we need beams?

Intense secondary beams



1 MW target at SNS

FOM: Secondaries/primary
Examples: spallation neutrons,
neutrino beams



The Spallation Neutron Source

❖ 1 MW @ 1 GeV (compare with ILC 11 MW at 500 GeV
(upgradeable to 4 MW))

==> miniscule beam loss into accelerator

==> large aperture in cavities ==> large cavities

==> low frequency

==> high energy stability

==> large stored energy

==> high efficiency at E_z

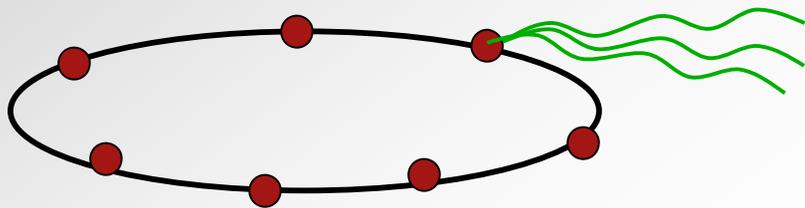
==> **SC RF**





Matter to energy: Synchrotron radiation science

Synchrotron light source
(pulsed incoherent X-ray emission)



FOM: Brilliance v. λ

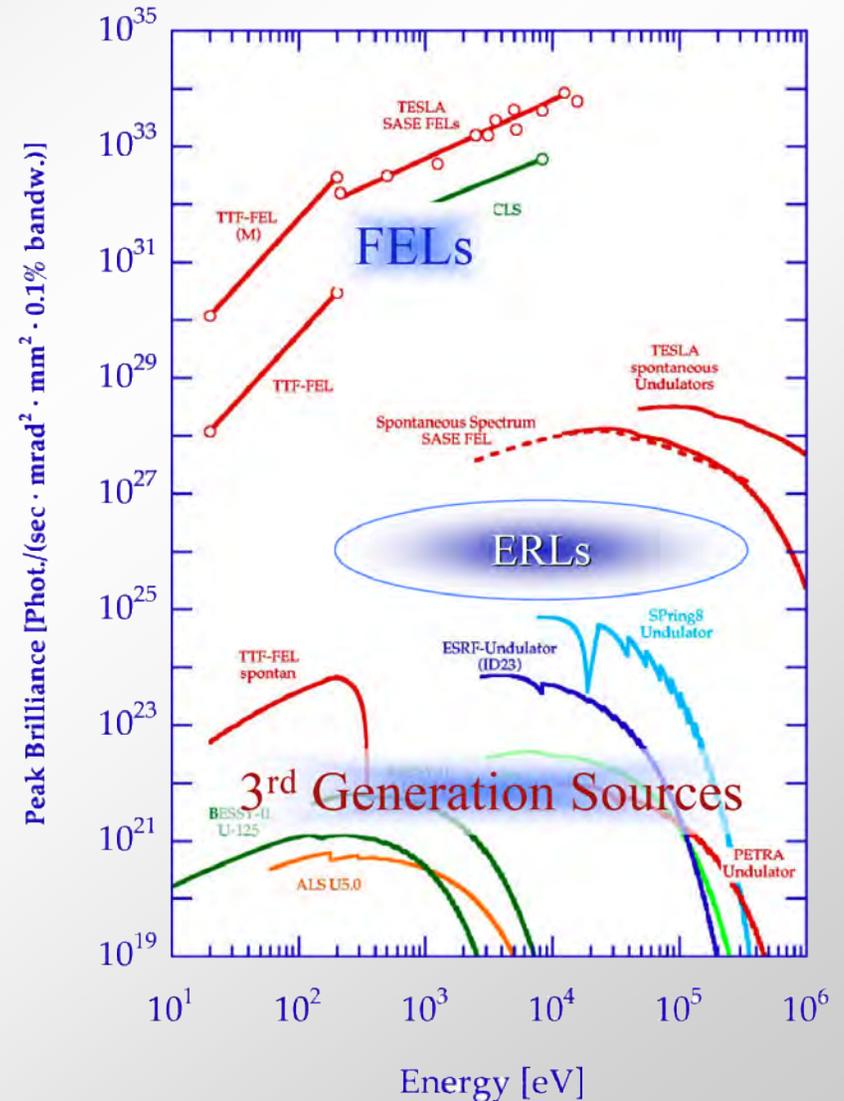
$$B = \text{ph/s/mm}^2/\text{mrad}^2/0.1\% \text{BW}$$

Pulse duration

Science with X-rays

Imaging

Spectroscopy





Matter to energy: Energy Recovery Linacs

Hard X-rays $\implies \sim 5$ GeV

Synchrotron light source
(pulsed incoherent X-ray emission)

Pulse rates – kHz \implies MHz

X-ray pulse duration ≤ 1 ps

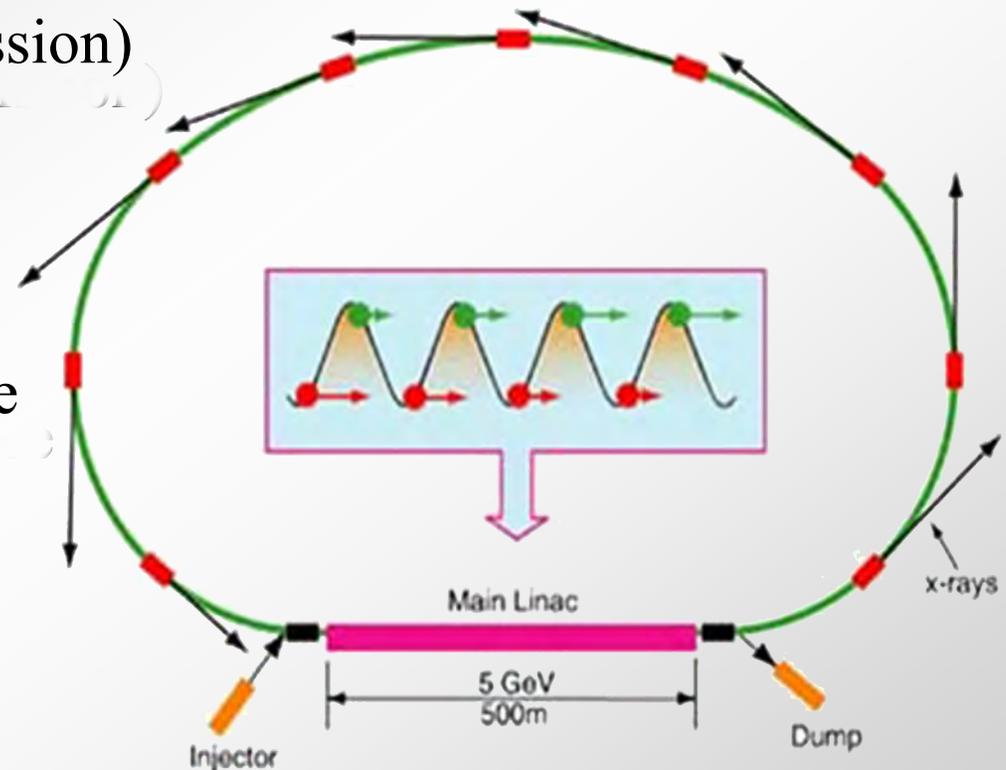
High average e-beam brilliance
& e-beam duration ≤ 1 ps

\implies One pass through ring

\implies Recover beam energy

\implies High efficiency

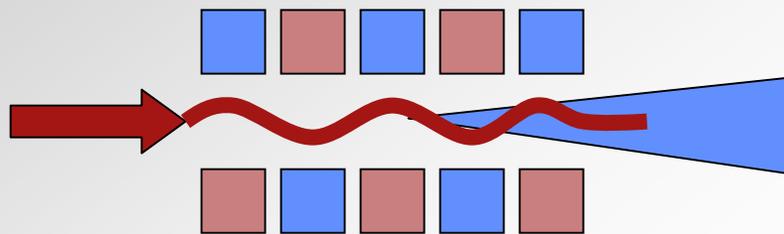
\implies **SC RF**



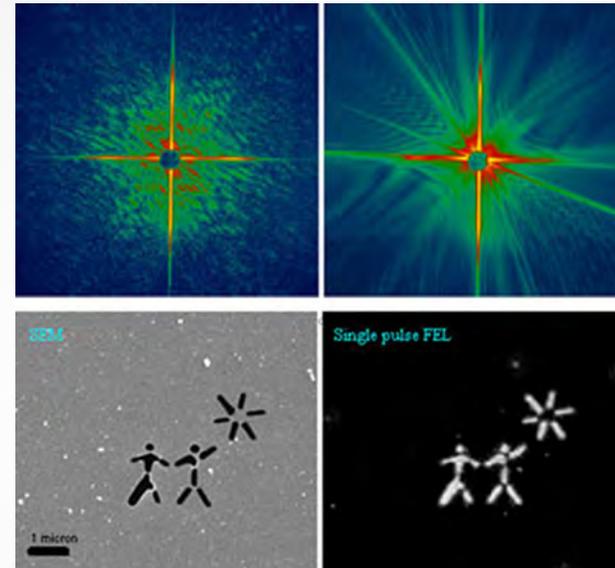
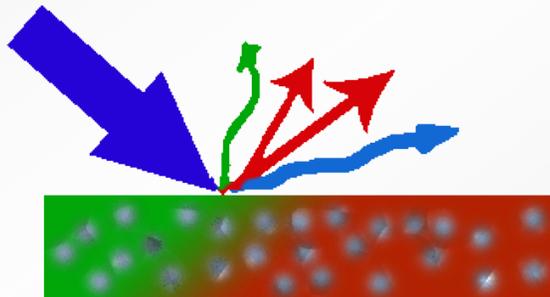


Even higher brightness requires coherent emission \implies FEL

Free electron laser



FOM: Brightness v. λ
Time structure





Full range of FEL-based science requires...

- ❖ Pulses rates 10 Hz to 10 MHz (NC limited to ~ 100 Hz)
 - High efficiency
 - ❖ Pulse duration 10 fs - 1 ps
 - ❖ High gain
 - Excellent beam emittance
 - ==> Minimize wakefield effect
 - ==> large aperture
 - ==> low frequency
 - Stable beam energy & intensity
 - ==> large stored energy in cavities
 - ==> high Q
- ====> SC RF