



Unit 4 - Lecture 9

RF-accelerators: RF-cavities

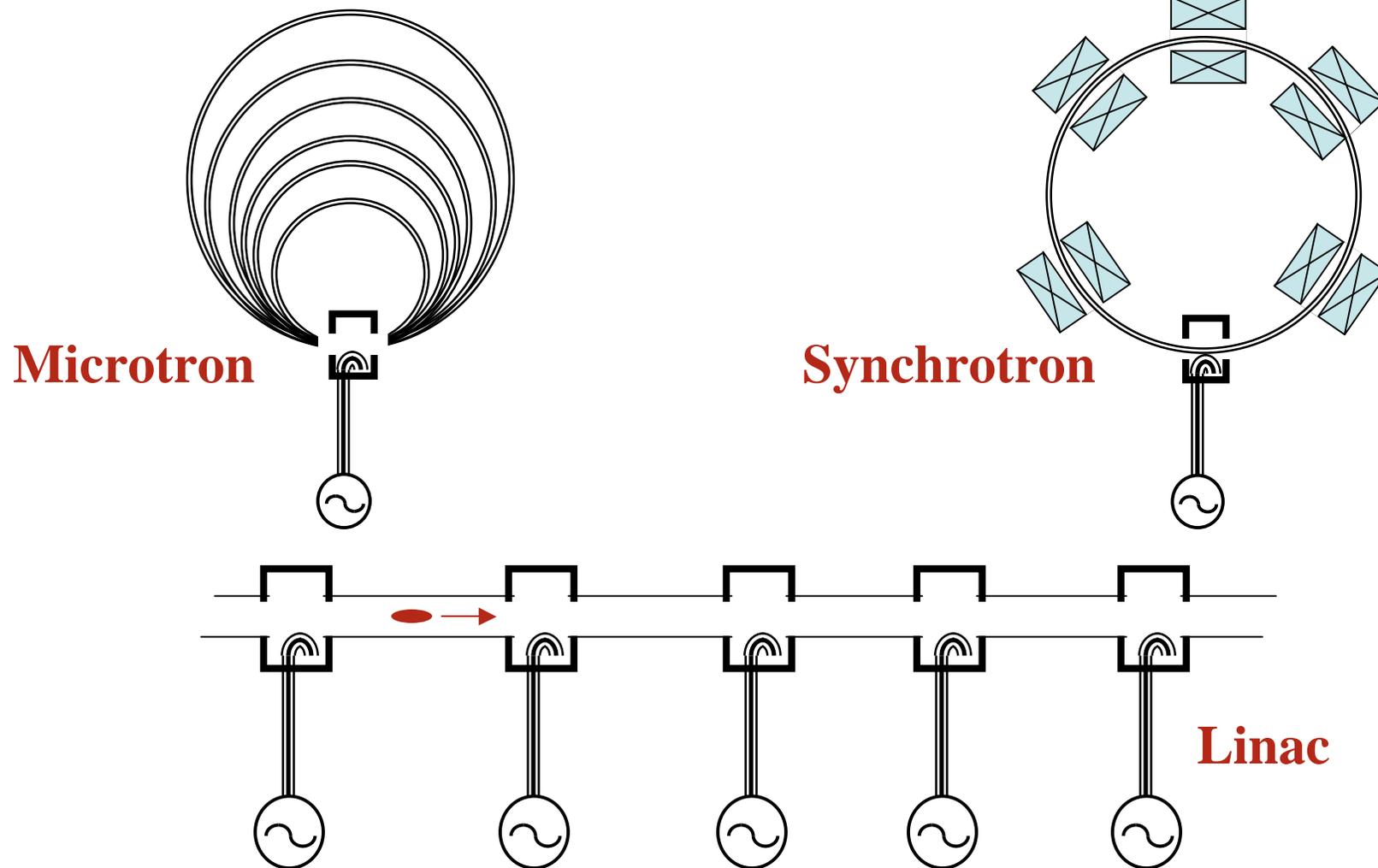
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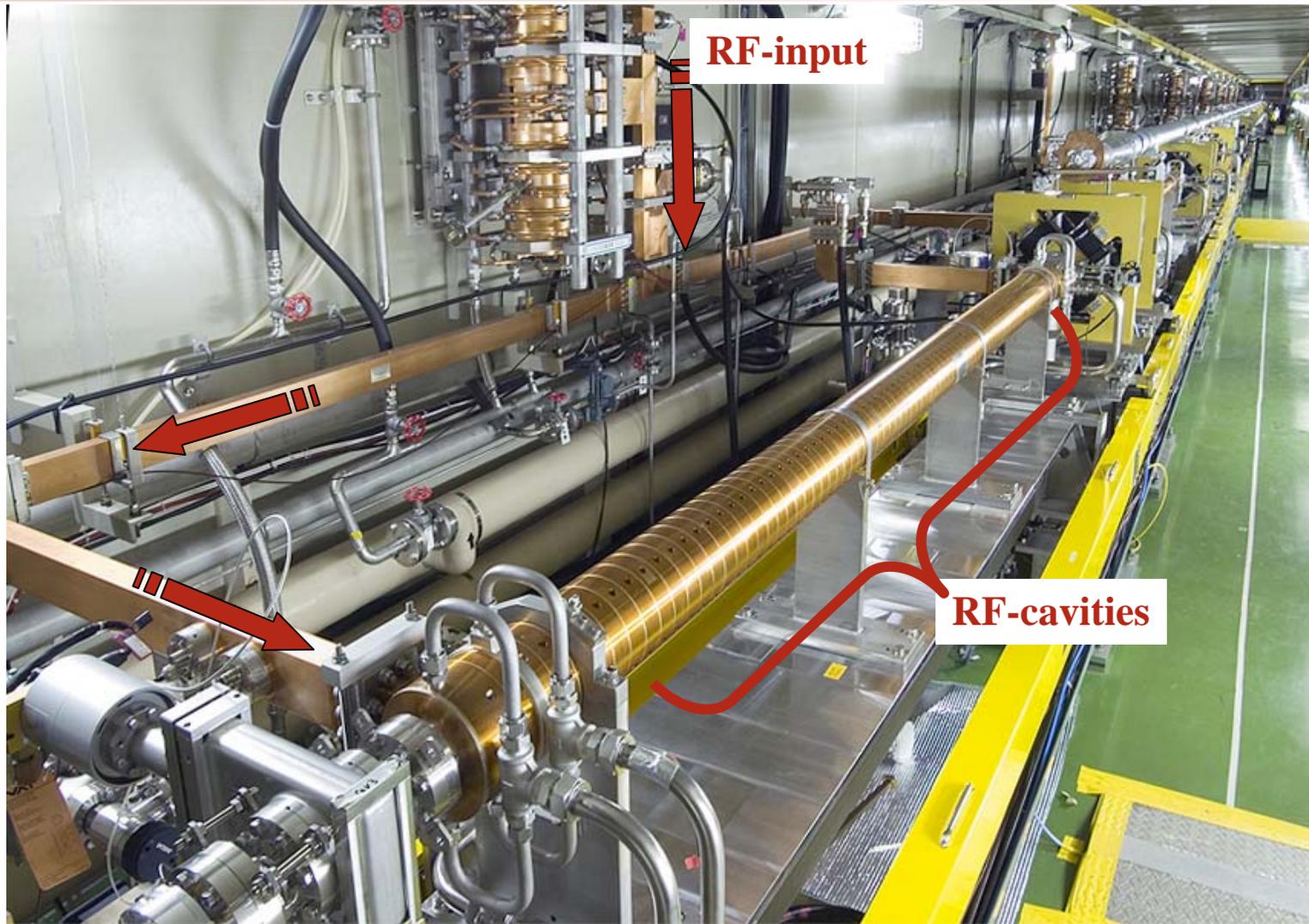


RF-cavities for acceleration





S-band (~ 3 GHz) RF linac





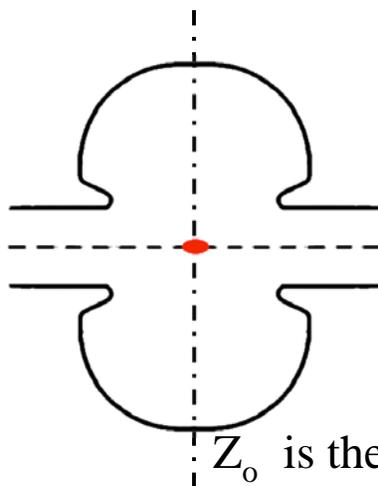
RF cavities: Basic concepts



* Fields and voltages are complex quantities.

→ For standing wave structures use phasor representation

$$\tilde{V} = V e^{i\omega t} \quad \text{where} \quad V = |\tilde{V}|$$



At $t = 0$ particle receives maximum voltage gain

Z_0 is the reference plane

* For cavity driven externally, phase of the voltage is

$$\theta = \omega t + \theta_0$$

* For electrons $v \approx c$; therefore $z = z_0 + ct$



Basic principles and concepts



- * Superposition
- * Energy conservation
- * Orthogonality (of cavity modes)
- * Causality



Basic principles: Reciprocity & superposition

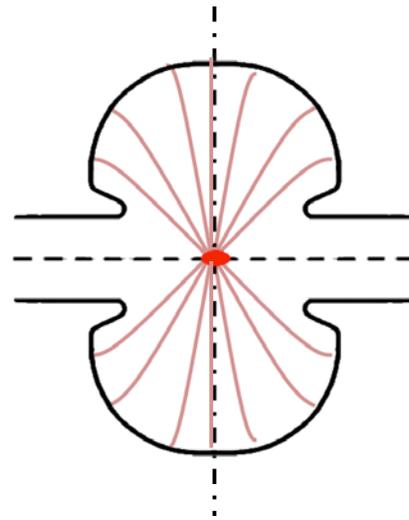


✱ If you can kick the beam, the beam can kick you

==>

$$\text{Total cavity voltage} = V_{\text{generator}} + V_{\text{beam-induced}}$$

$$\text{Fields in cavity} = \mathbf{E}_{\text{generator}} + \mathbf{E}_{\text{beam-induced}}$$

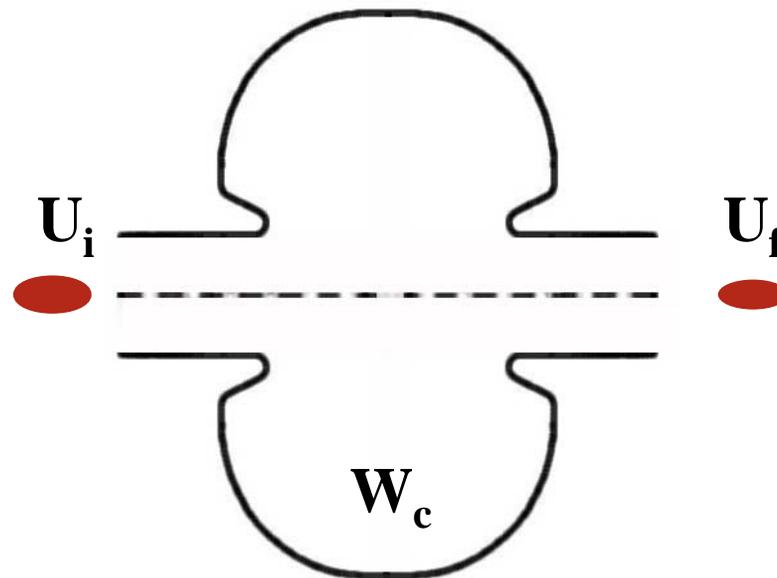




Basic principles: Energy conservation



- ✱ Total energy in the particles and the cavity is conserved
 - Beam loading



$$\Delta W_c = U_i - U_f$$



Basics: Orthogonality of normal modes



- ✱ Each mode in the cavity can be treated independently in computing fields induced by a charge crossing the cavity.
- ✱ The total stored energy is equals the sum of the energies in the separate modes.
- ✱ The total field is the phasor sum of all the individual mode fields at any instant.



Basic principles: Causality



- ✱ There can be no disturbance ahead of a charge moving at the velocity of light.
- ✱ In a mode analysis of the growth of the beam-induced field, the field must vanish ahead of the moving charge for each mode.



Example: Differential superposition



- * A point charge q induces a voltage V_o passing through a cavity, what voltage is induced by a Gaussian bunch of charge q ?
- * A differential charge induces the differential voltage

$$d\tilde{V} = \tilde{V}_o \frac{dq}{q} = V_o e^{j\omega_o t} \frac{dq}{q}$$

- * Say dq passes $z = 0$ at t_o ; at time t the induced voltage will be

$$d\tilde{V} = \frac{V_o}{q} e^{j\omega_o(t-t_o)} dq(t_o)$$

- * The bunch has a Gaussian distribution in time

$$dq(t_o) = \frac{q}{\sqrt{2\pi\sigma}} e^{-t_o^2/2\sigma^2} dt_o$$

$$V = V_o e^{j\omega_o t} e^{-\omega_o^2 \sigma^2 / 2} dt_o$$

Integrate



Basic components of an RF cavity



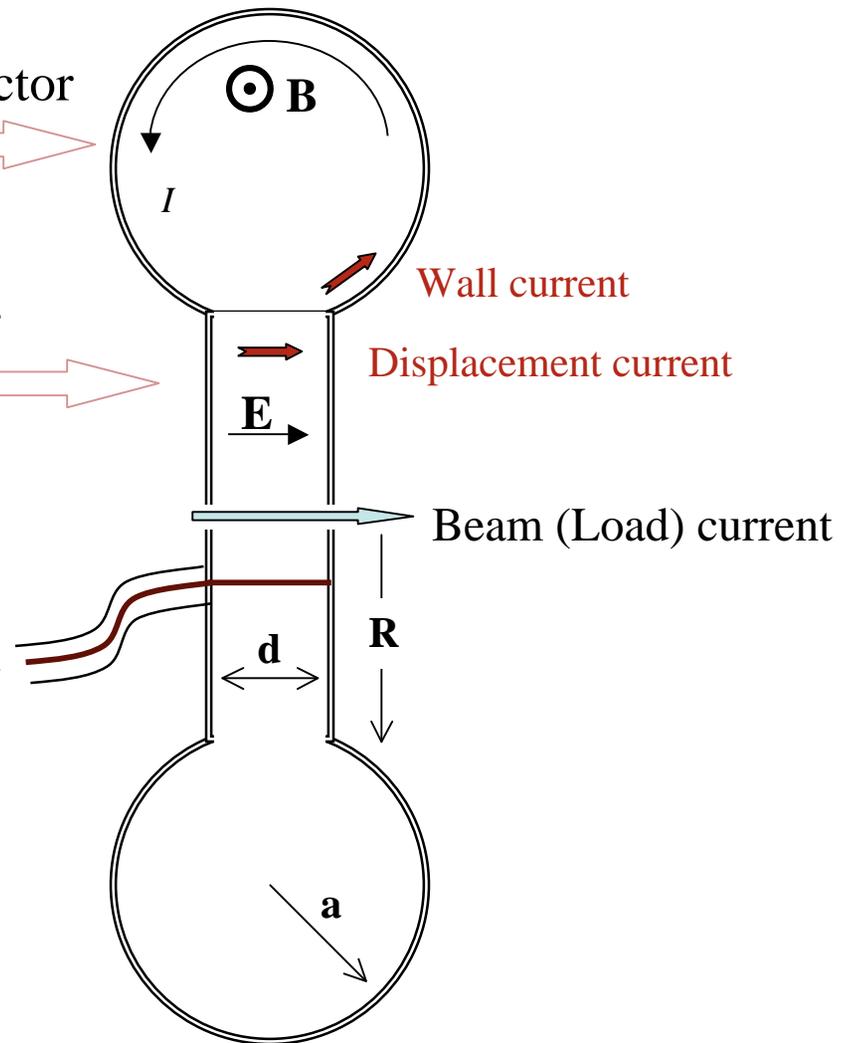
Outer region: Large, single turn Inductor



Central region: Large plate Capacitor

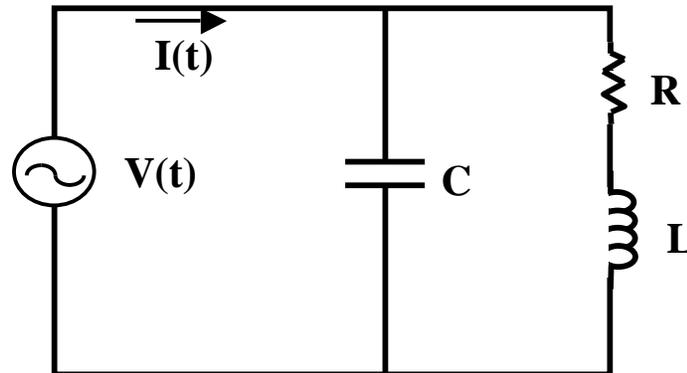


Power feed from rf - generator





Lumped circuit analogy of resonant cavity



$$Z(\omega) = [j\omega C + (j\omega L + R)^{-1}]^{-1}$$

$$Z(\omega) = \frac{1}{j\omega C + (j\omega L + R)^{-1}} = \frac{(j\omega L + R)}{(j\omega L + R)j\omega C + 1} = \frac{(j\omega L + R)}{(1 - \omega^2 LC) + j\omega RC}$$

The resonant frequency is $\omega_o = \frac{1}{\sqrt{LC}}$

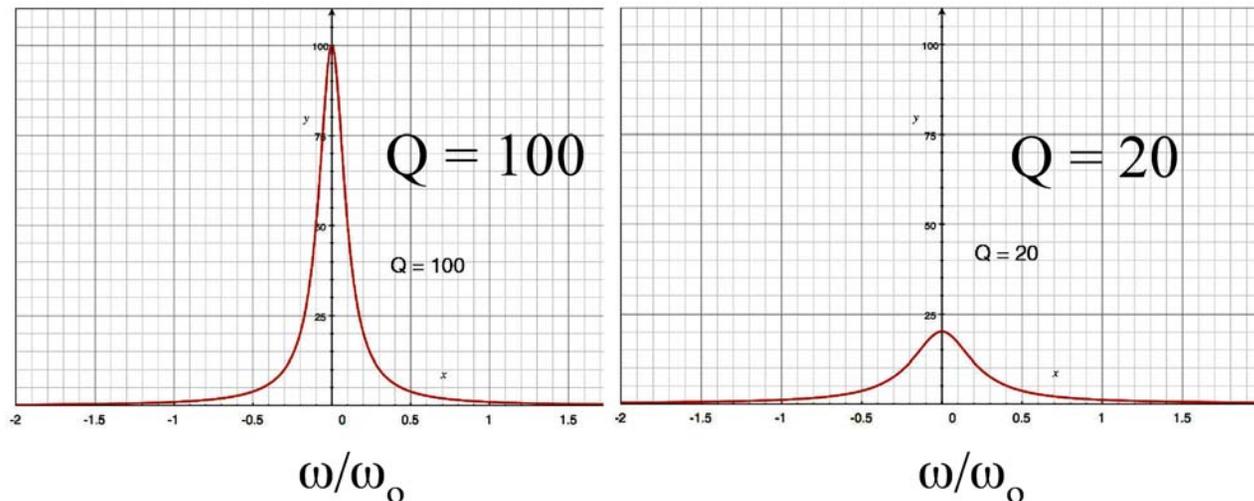


Q of the lumped circuit analogy



Converting the denominator of Z to a real number we see that

$$|Z(\omega)| \sim \left[\left(1 - \frac{\omega^2}{\omega_0^2} \right)^2 + (\omega RC)^2 \right]^{-1}$$



The width is $\frac{\Delta\omega}{\omega_0} = \frac{R}{\sqrt{L/C}}$



More basics from circuits - Q



$$Q = \frac{\omega_o \circ \text{Energy stored}}{\text{Time average power loss}} = \frac{2\pi \circ \text{Energy stored}}{\text{Energy per cycle}}$$

$$\mathcal{E} = \frac{1}{2} L I_o I_o^* \quad \text{and} \quad \langle \mathcal{P} \rangle = \langle i^2(t) \rangle R = \frac{1}{2} I_o I_o^* R_{\text{surface}}$$

$$\therefore Q = \frac{\sqrt{L/C}}{R} = \left(\frac{\Delta\omega}{\omega_o} \right)^{-1}$$



Translate circuit model to a cavity model: Directly driven, re-entrant RF cavity



Outer region: Large, single turn Inductor

$$L = \frac{\mu_0 \pi a^2}{2\pi(R+a)}$$



Central region: Large plate Capacitor

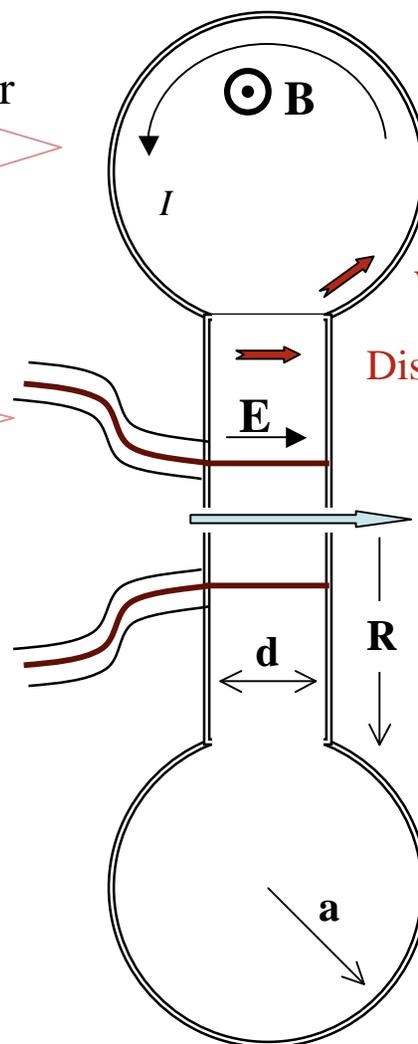
$$C = \epsilon_0 \frac{\pi R^2}{d}$$



$$\omega_o = \frac{1}{\sqrt{LC}} = c \left[\frac{2((R+a)d)}{\pi R^2 a^2} \right]^{1/2}$$

Q – set by resistance in outer region

$$Q = \sqrt{L/C} / R$$



Expanding outer region raises Q

Wall current

Displacement current

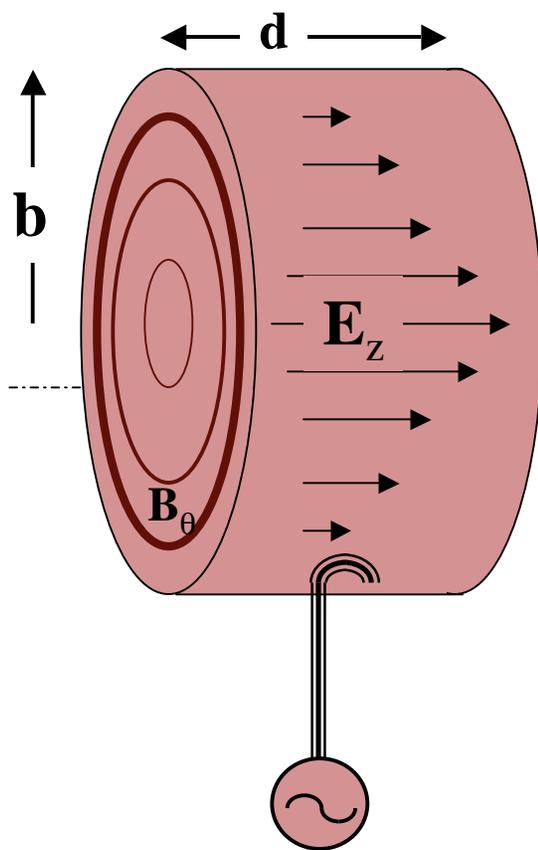
Beam (Load) current

Narrowing gap raises shunt impedance

Source: Humphries, Charged Particle Accelerators



Properties of the RF pillbox cavity



$$\sigma_{walls} = \infty$$

- * We want lowest mode: with only \mathbf{E}_z & \mathbf{B}_θ
- * Maxwell's equations are:

$$\frac{1}{r} \frac{\partial}{\partial r} (rB_\theta) = \frac{1}{c^2} \frac{\partial}{\partial t} E_z \quad \text{and} \quad \frac{\partial}{\partial r} E_z = \frac{\partial}{\partial t} B_\theta$$

- * Take derivatives

$$\frac{\partial}{\partial t} \left[\frac{1}{r} \frac{\partial}{\partial r} (rB_\theta) \right] = \frac{\partial}{\partial t} \left[\frac{\partial B_\theta}{\partial r} + \frac{B_\theta}{r} \right] = \frac{1}{c^2} \frac{\partial^2 E_z}{\partial t^2}$$

$$\frac{\partial}{\partial r} \frac{\partial E_z}{\partial r} = \frac{\partial}{\partial r} \frac{\partial B_\theta}{\partial t}$$

\Rightarrow

$$\frac{\partial^2 E_z}{\partial r^2} + \frac{1}{r} \frac{\partial E_z}{\partial r} = \frac{1}{c^2} \frac{\partial^2 E_z}{\partial t^2}$$



For a mode with frequency ω



✱
$$E_z(r, t) = E_z(r) e^{i\omega t}$$

✱ Therefore,
$$E_z'' + \frac{E_z'}{r} + \left(\frac{\omega}{c}\right)^2 E_z = 0$$

→ (Bessel's equation, 0 order)

✱ Hence,

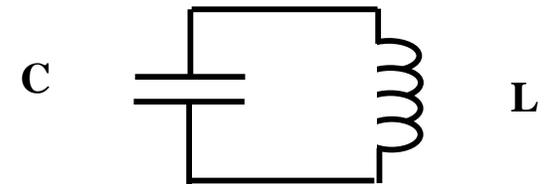
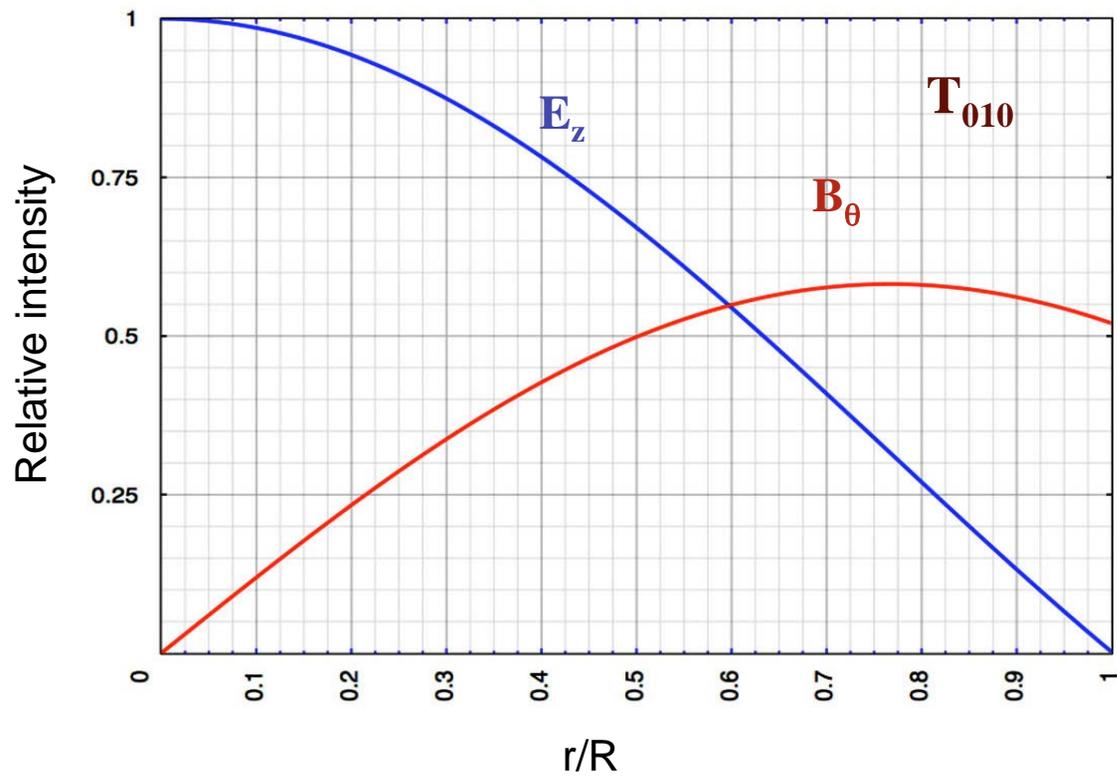
$$E_z(r) = E_o J_o\left(\frac{\omega}{c} r\right)$$

✱ For conducting walls, $E_z(R) = 0$, therefore

$$\frac{2\pi f}{c} b = 2.405$$

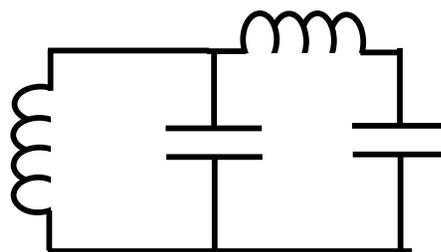
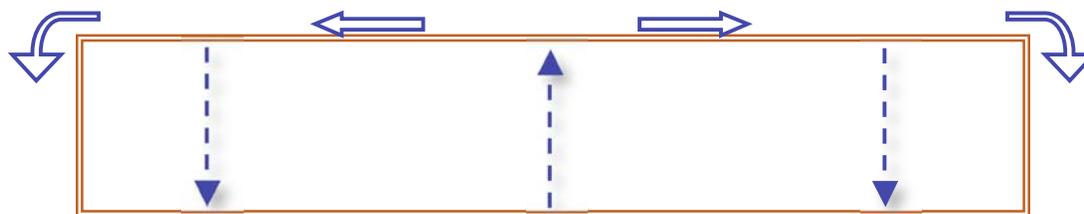
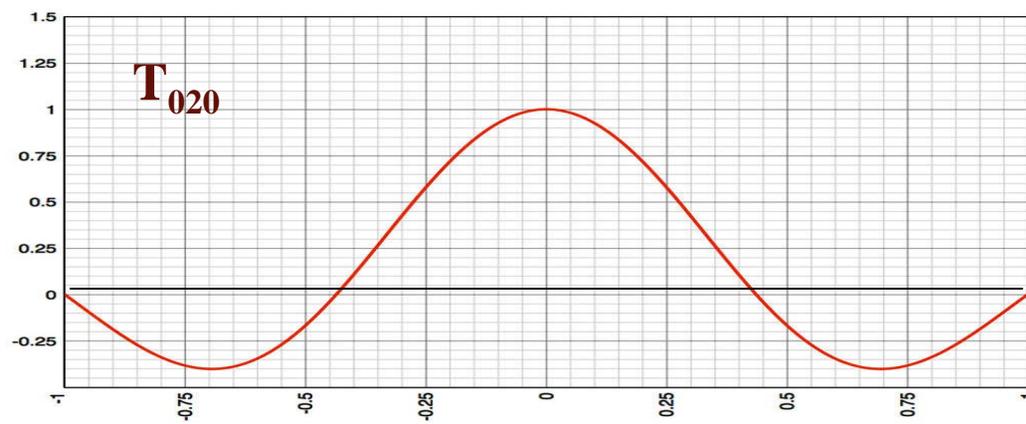


E-fields & equivalent circuit: T_{010} mode



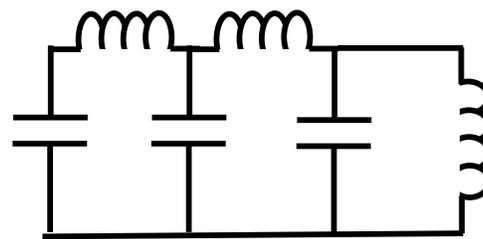
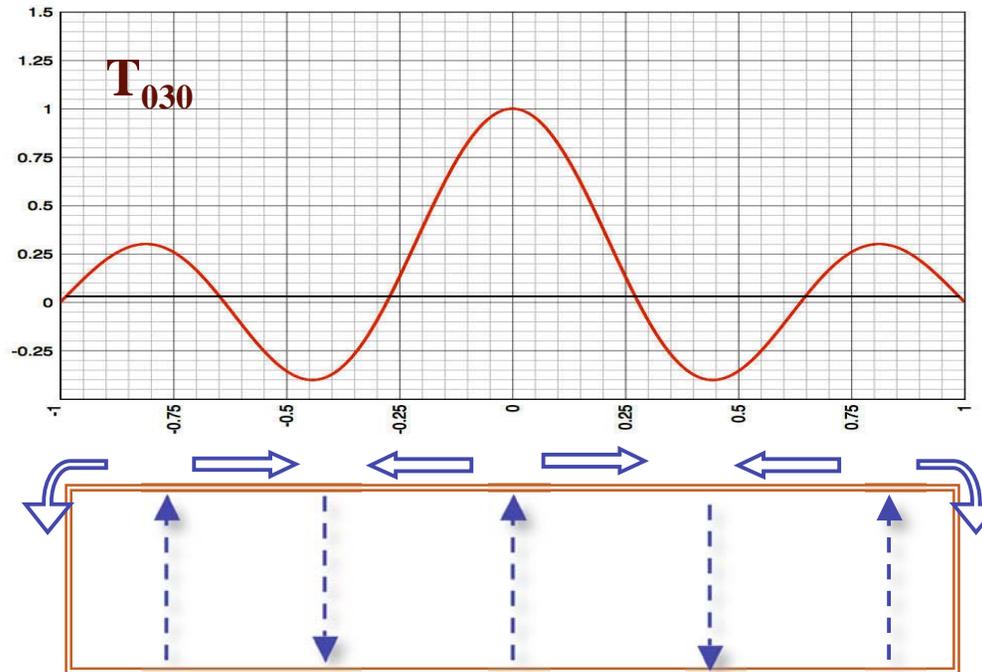


E-fields & equivalent circuits for T_{020} modes





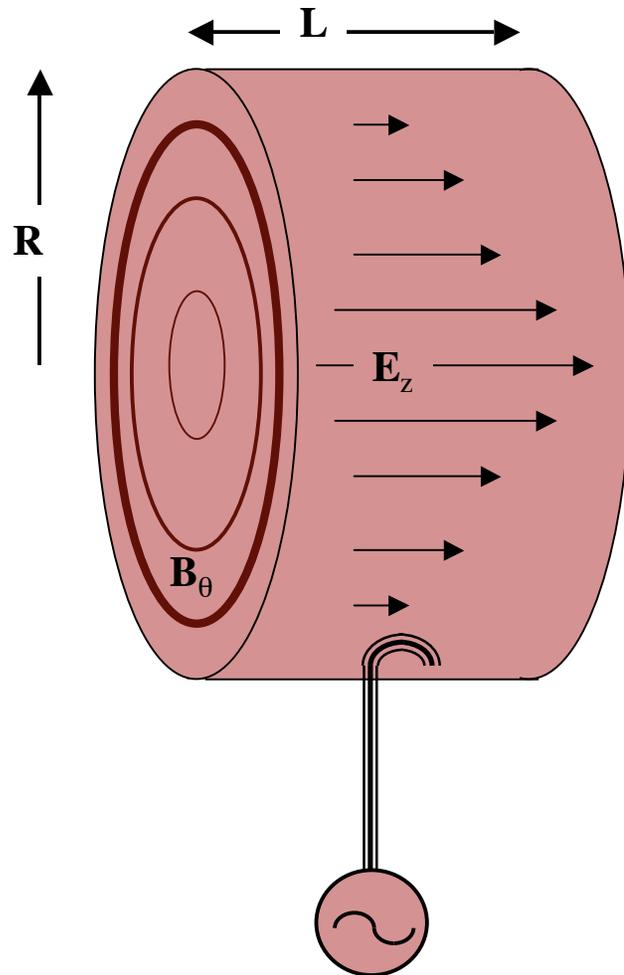
E-fields & equivalent circuits for T_{on0} modes



T_{0n0} has
 n coupled, resonant
circuits; each L & C
reduced by $1/n$



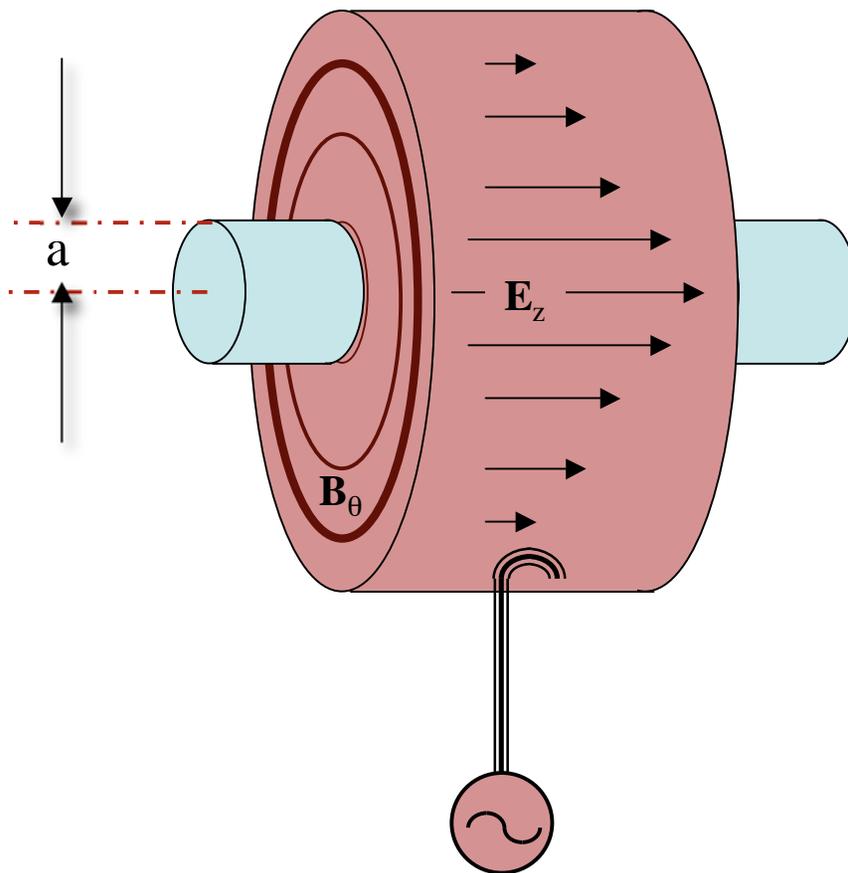
Simple consequences of pillbox model



- * Increasing R lowers frequency
==> Stored Energy, $\mathcal{E} \sim \omega^{-2}$
- * $\mathcal{E} \sim E_z^2$
- * Beam loading lowers E_z for the next bunch
- * Lowering ω lowers the fractional beam loading
- * Raising ω lowers $Q \sim \omega^{-1/2}$
- * If time between beam pulses,
 $T_s \sim Q/\omega$
almost all \mathcal{E} is lost in the walls



The beam tube makes the field modes (& cell design) more complicated



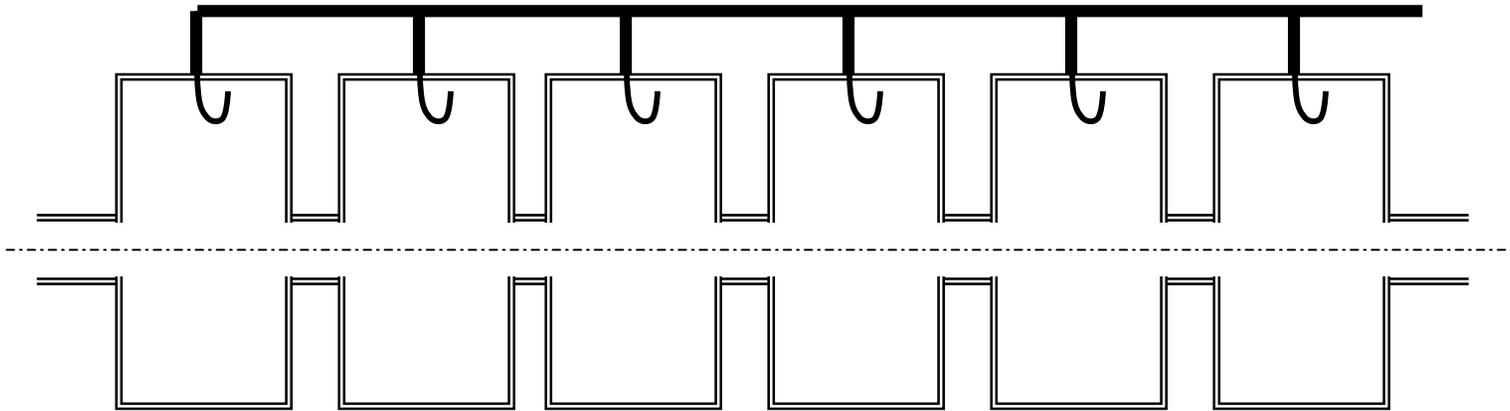
- * Peak E no longer on axis
 - $E_{pk} \sim 2 - 3 \times E_{acc}$
 - $FOM = E_{pk}/E_{acc}$
- * ω_0 more sensitive to cavity dimensions
 - Mechanical tuning & detuning
- * Beam tubes add length & ϵ 's w/o acceleration
- * Beam induced voltages $\sim a^{-3}$
 - Instabilities



Cavity figures of merit



Make the linac with a series of pillbox cavities



Power the cavities so that $E_z(z,t) = E_z(z)e^{i\omega t}$

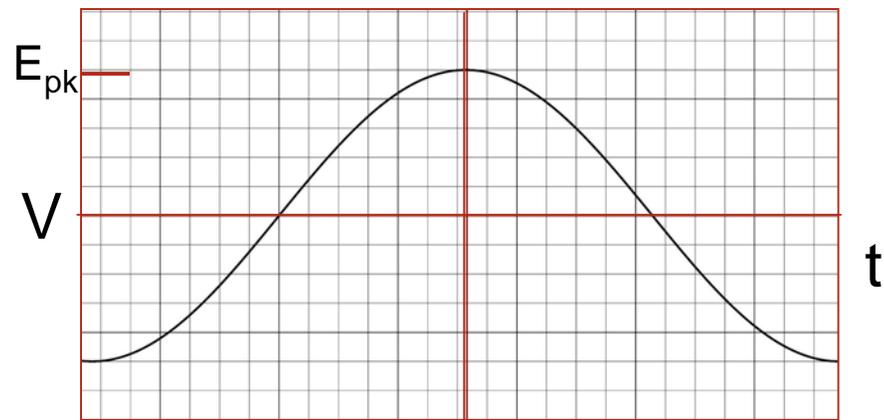
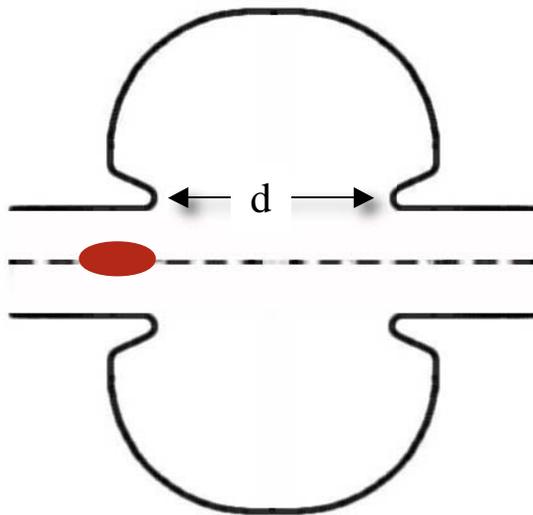


Figure of Merit: Accelerating voltage



- ✱ The voltage varies during time that bunch takes to cross gap
→ reduction of the peak voltage by Γ (transt time factor)

$$\Gamma = \frac{\sin(\vartheta/2)}{\vartheta/2} \quad \text{where } \vartheta = \omega d / \beta c$$



For maximum acceleration $T_{\text{cav}} = \frac{d}{c} = \frac{T_{\text{rf}}}{2} \implies \Gamma = 2/\pi$



Figure of merit from circuits - Q



$$Q = \frac{\omega_o \circ \text{Energy stored}}{\text{Time average power loss}} = \frac{2\pi \circ \text{Energy stored}}{\text{Energy lost per cycle}}$$

$$\mathcal{E} = \frac{\mu_o}{2} \int_v |H|^2 dv = \frac{1}{2} L I_o I_o^*$$

$$\langle \mathcal{P} \rangle = \frac{R_{surf}}{2} \int_s |H|^2 ds = \frac{1}{2} I_o I_o^* R_{surf}$$

$$R_{surf} = \frac{1}{\text{Conductivity} \circ \text{Skin depth}} \sim \omega^{1/2}$$

$$\therefore Q = \frac{\sqrt{L/C}}{R_{surf}} = \left(\frac{\Delta\omega}{\omega_o} \right)^{-1}$$



Measuring the energy stored in the cavity allows us to measure



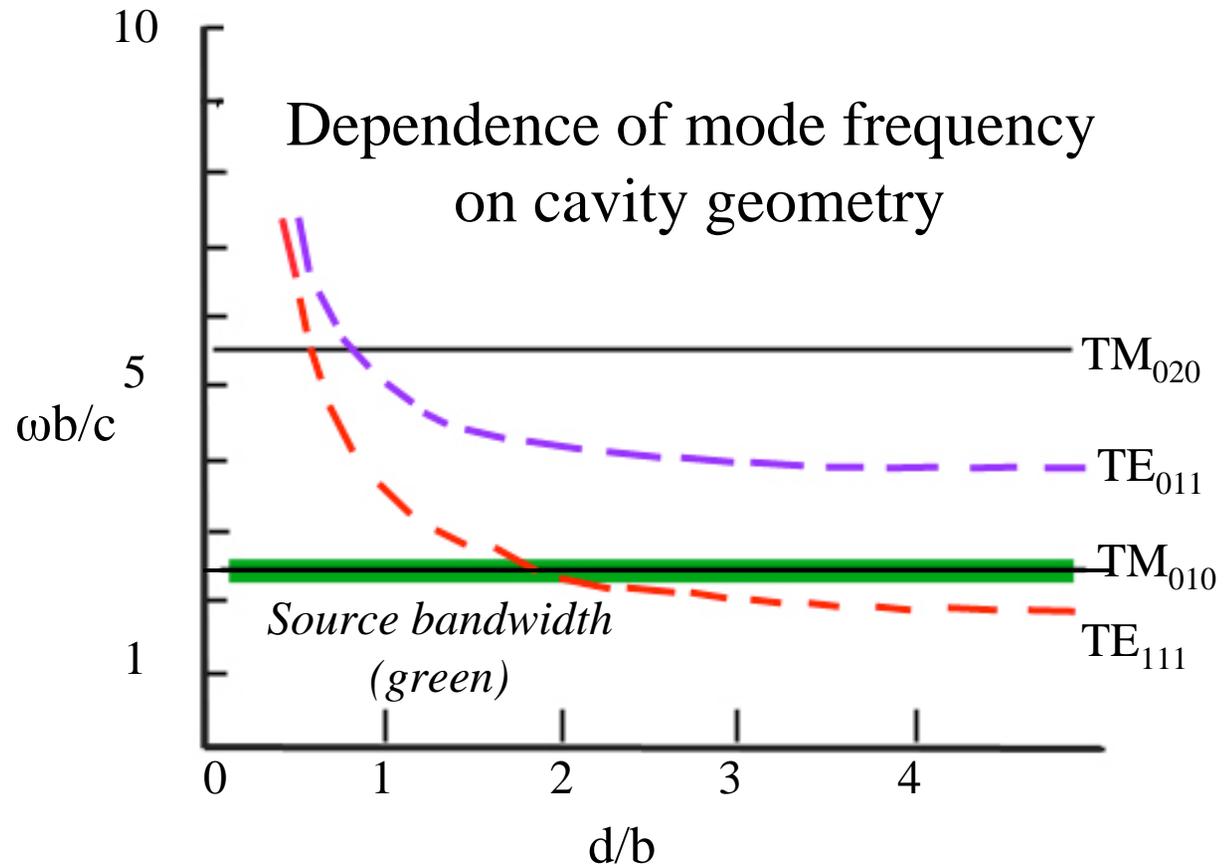
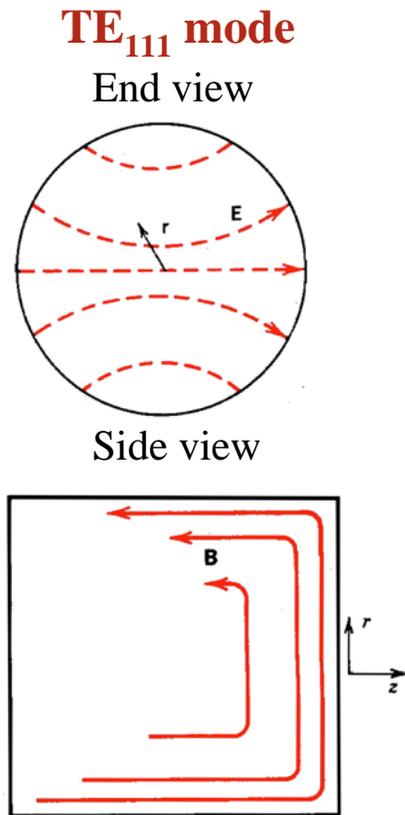
- ✱ We have computed the field in the fundamental mode

$$U = \int_0^d dz \int_0^b dr 2\pi r \left(\frac{\epsilon E_o^2}{2} \right) J_1^2(2.405r/b)$$
$$= b^2 d \left(\epsilon E_o^2 / 2 \right) J_1^2(2.405)$$

- ✱ To measure Q we excite the cavity and measure the E field as a function of time
- ✱ Energy lost per half cycle = $U\pi Q$
- ✱ Note: energy can be stored in the higher order modes that deflect the beam



Keeping energy out of higher order modes



Choose cavity dimensions to stay far from crossovers



Figure of merit for accelerating cavity: power to produce the accelerating field



Resistive input (shunt) impedance at ω_0 relates power dissipated in walls to accelerating voltage

$$R_{in} = \frac{\langle V^2(t) \rangle}{\mathcal{P}} = \frac{V_o^2}{2\mathcal{P}} = Q\sqrt{L/C}$$

Linac literature commonly defines “shunt impedance” without the “2”

$$\mathcal{R}_{in} = \frac{V_o^2}{\mathcal{P}} \sim \frac{1}{R_{surf}}$$

Typical values 25 - 50 M Ω



Computing shunt impedance



$$\mathcal{R}_{in} = \frac{V_o^2}{\mathcal{P}}$$

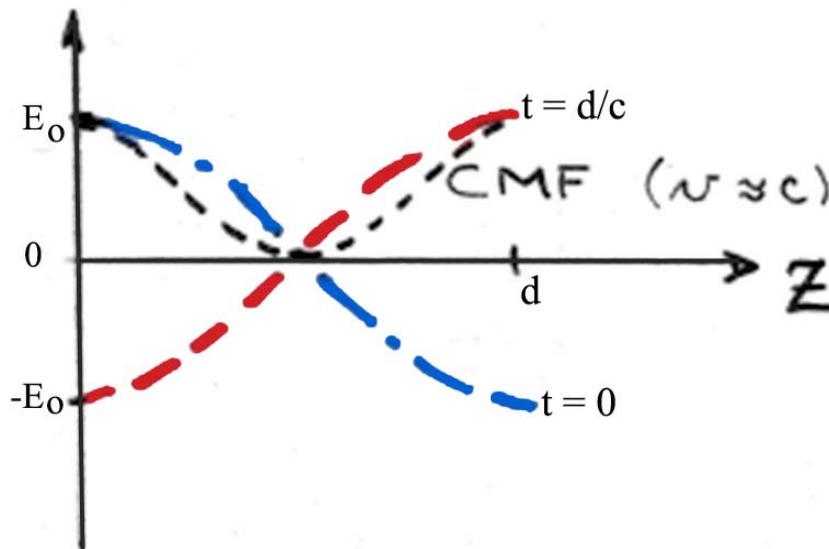
$$\langle \mathcal{P} \rangle = \frac{R_{surf}}{2} \int_s |H|^2 ds$$

$$R_{surf} = \frac{\mu\omega}{2\sigma_{dc}} = \pi Z_o \frac{\delta_{skin}}{\lambda_{rf}} \quad \text{where } Z_o = \sqrt{\frac{\mu_o}{\epsilon_o}} = 377\Omega$$

The on-axis field E and surface H are generally computed with a computer code such as SUPERFISH for a complicated cavity shape



Compute the voltage gain correctly



The voltage gain seen by the beam can be computed in the co-moving frame, or we can use the transit-time factor, Γ & compute V at fixed time

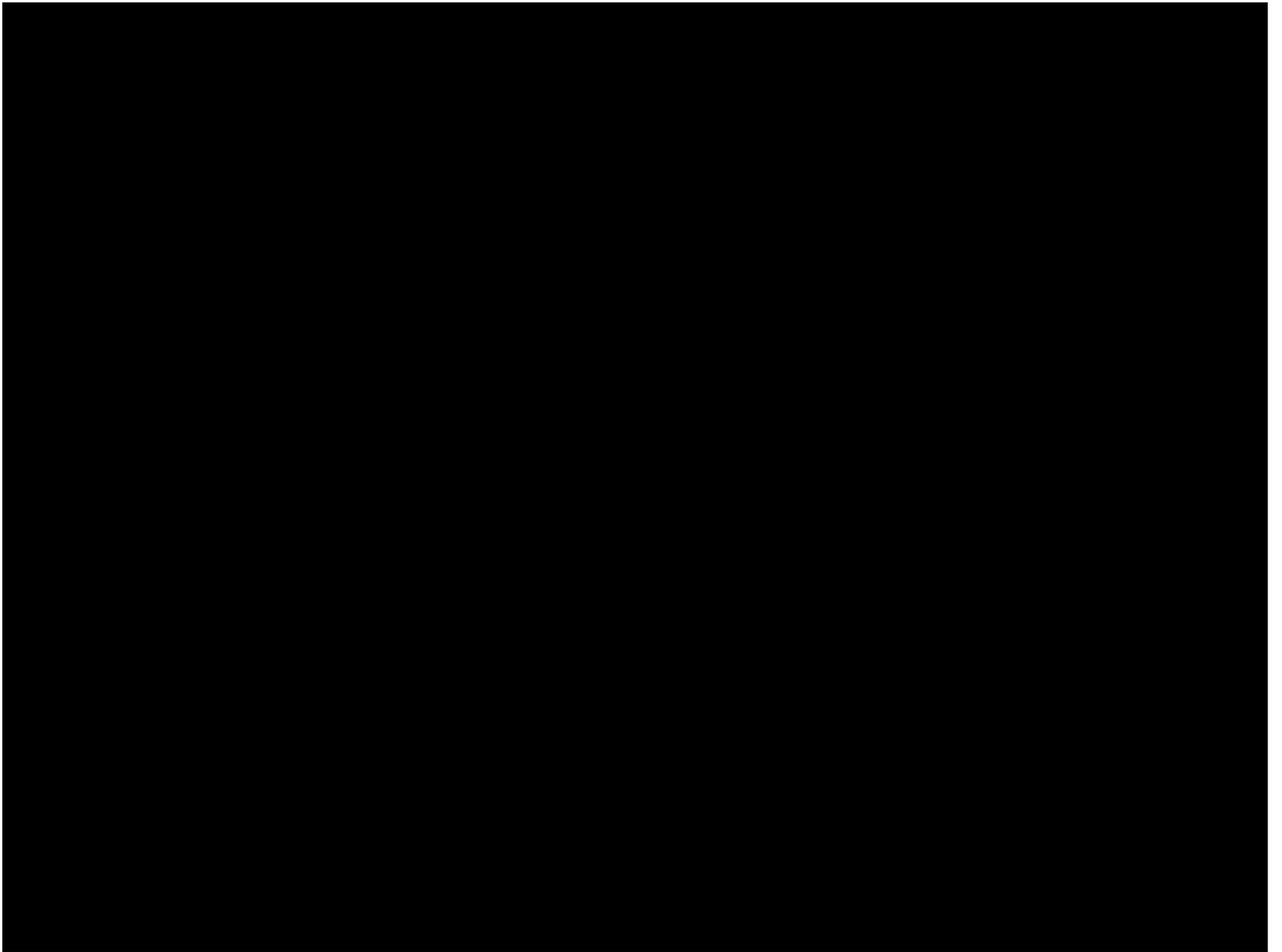
$$V_o^2 = \Gamma \int_{z_1}^{z_2} E(z) dz$$



Exercise: Pillbox array



- ✱ Derive the Q and R_{sh} for the pillbox cavity as a function of the dimensions of the cavity and the frequency of the fundamental mode





Note on previous slide



$$\begin{aligned} Z(\omega) &= \frac{1}{j\omega C + (j\omega L + R)^{-1}} = \frac{(j\omega L + R)}{(j\omega L + R)j\omega C + 1} = \frac{(j\omega L + R)}{(1 - \omega^2 LC) + j\omega RC} \\ &= \frac{(j\omega L + R)}{\left(1 - \frac{\omega^2}{\omega_o^2}\right)^2 + j\omega RC} = \frac{(j\omega L + R) \left[\left(1 - \frac{\omega^2}{\omega_o^2}\right) - j\omega RC \right]}{\left(1 - \frac{\omega^2}{\omega_o^2}\right)^2 + (\omega RC)^2} = \frac{j\omega \left[L \left(1 - \frac{\omega^2}{\omega_o^2}\right) - R^2 C \right] + R \left(1 - \frac{\omega^2}{\omega_o^2}\right) + \frac{\omega^2}{\omega_o^2} R}{\left(1 - \frac{\omega^2}{\omega_o^2}\right)^2 + (\omega RC)^2} \\ \frac{j\omega \left[L \left(1 - \frac{\omega^2}{\omega_o^2}\right) - R^2 C \right] + R}{\left(1 - \frac{\omega^2}{\omega_o^2}\right)^2 + (\omega RC)^2} &= \frac{1}{\left(1 - \frac{\omega^2}{\omega_o^2}\right)^2 + (\omega RC)^2} \left[R + j\omega \left(L \left(1 - \frac{\omega^2}{\omega_o^2}\right) - R^2 C \right) \right] \\ \Rightarrow |Z| &= \frac{1}{\left(1 - \frac{\omega^2}{\omega_o^2}\right)^2 + (\omega RC)^2} \left[R^2 + \omega^2 \left(L \left(1 - \frac{\omega^2}{\omega_o^2}\right) - R^2 C \right)^2 \right]^{1/2} \end{aligned}$$