



Pulsed Power Engineering Switching Devices

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Ideal Switch

- $V = \infty$
- $I = \infty$
- Closing/opening time = 0
- $L = C = R = 0$
- Simple to control
- No delay or jitter
- Lasts forever
- Never fails



Switches

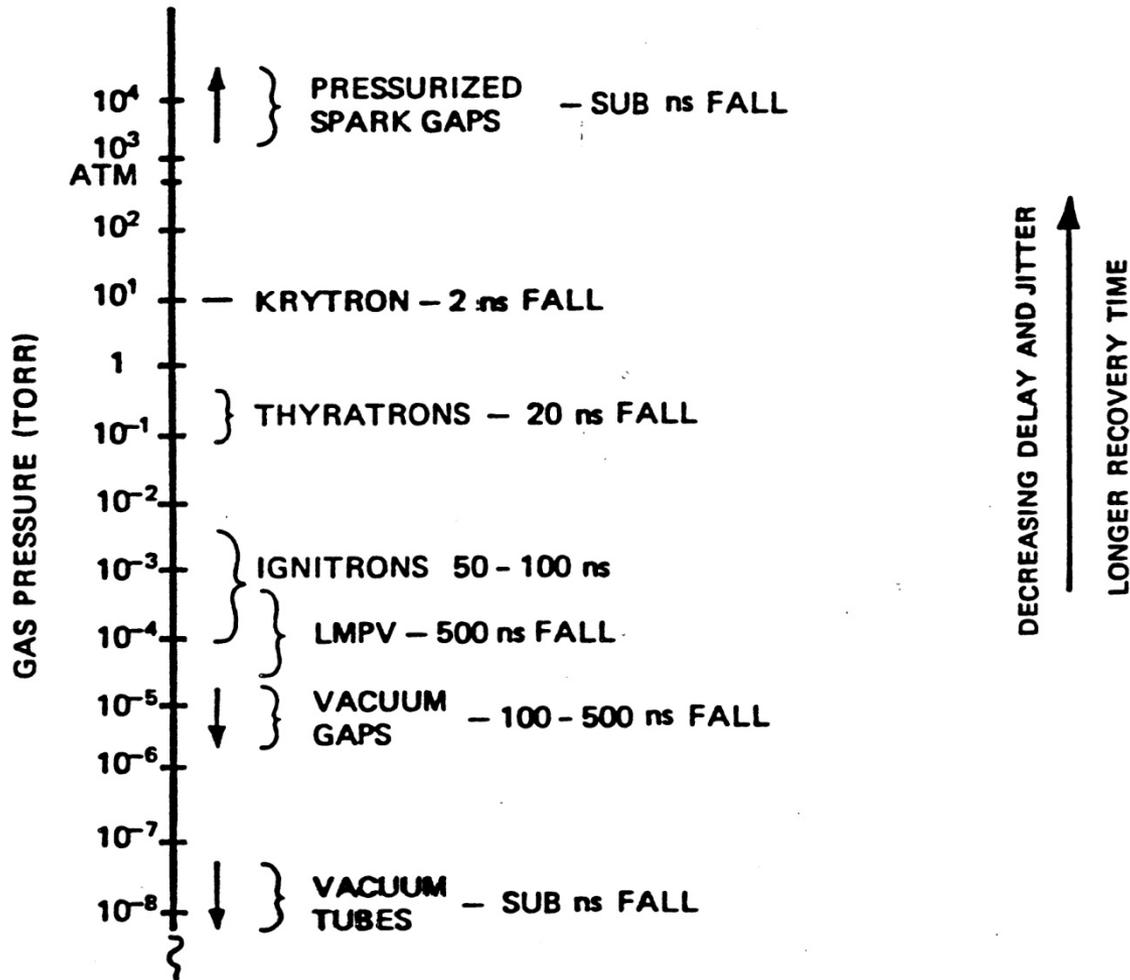
- Electromechanical
- Vacuum
- Gas
 - Spark gap
 - Thyatron
 - Ignitron
 - Plasma Opening
- Solid state
 - Diodes
 - Diode opening switch
 - Thyristors
 - Electrically triggered
 - Optically triggered
 - dV/dt triggered
 - Transistors
 - IGBT
 - MOSFET

Switches

- Electromechanical
 - Open relay
 - To very high voltages, set by size of device
 - Commercial devices to ~0.5 MV, ~50 kA
 - Ross Engineering Corp.
 - Closing time ~10's of ms typical
 - Large jitter, ~ms typical
 - Closure usually completed by arcing
 - Poor opening switch
 - Commonly used as engineered ground
 - Vacuum relay
 - Models that can open under load are available
 - Commercial devices
 - Maximum voltage ~0.1 MV
 - Maximum current ~0.1 kA
 - Tyco-kilovac
 - Gigavac



Gas/Vacuum Switch Performance vs. Pressure





Vacuum Tube (Switch Tube)

- Space-charge limited current flow
 - $V_{ON} \propto V^{1.5}$
 - High power tubes have high dissipation
- Similar opening/closing characteristics
- Maximum voltage ~0.15 MV
- Maximum current ~0.5 kA, more typically $\ll 100$ A
- HV grid drive
- Decreasing availability
- High Cost



Spark Gaps

- Closing switch
- Generally inexpensive - in simplest form: two electrodes with a gap
- Can operated from vacuum to high pressure (both sides of Paschen Curve)
- Can use almost any gas or gas mixture as a dielectric. (air, dry nitrogen, SF₆, CO₂, etc.)
There are also liquid spark gaps (shock wave).
- Wide operating range
 - kV to MV
 - Amps to MA
- Time jitter ranges from *ns* for triggered gaps to 100's of μ s (or longer) for self-breaking overvoltage gaps
 - Low jitter
 - Trigger voltage ~ switch voltage
 - High dV/dt trigger
- Repetition rates - usually single shot but low kHz possible for burst mode
- $L_{arc} \sim 15$ nH/cm
 - Rail-gap switch with multiple arc channels \rightarrow lower inductance
- Lifetime limited
 - Erosion of electrodes (tungsten, copper, stainless steel, steel, brass, molybdenum, special alloys)
 - Debris across insulating surfaces
- Performance affected by temperature, pressure, electrode materials, surface condition of electrode, condition of insulators, operating conditions, etc.
- Devices are commercially available

Spark Gaps

PerkinElmer's Triggered Spark Gaps are a family of versatile high voltage switches. They consist of three electrodes in a hermetically sealed, pressurized ceramic envelope. Triggered Spark Gaps are generally characterized by a peak current capability of thousands to tens of thousands of amperes, delay times of tens of nanoseconds, arc resistance of tens of milliohms and inductance of 5 to 30 nanohenries. They are suitable for capacitor switching applications such as flash-lamps, electrically pumped gas lasers, medical lithotripters, and as crowbar protection devices.

Triggered Spark Gaps Ceramic-Metal



Features

- Fast switching operation
- High voltage holdoff
- Ceramic-metal construction
- No warm up period
- High current capability
- Long life

Triggered Spark Gap Ratings

PerkinElmer Model No.	O-A Range, kV Min/Max (1, 10)		SBV, kV (4)	V _T Min Trig (kV Open Circuit) (5)	Trigger Mode	Recommended PerkinElmer Transformer (6, 7)	Typical Delay Time* * when operated in mode A (Nanoseconds)		Simultaneous Ratings Crowbar Service, Typical Life: 5000-20,000 Shots (11)	Simultaneous Ratings Repetitive Switching Typical Life: 1-5 Million Shots (11)
	At 70% SBV	At 40% SBV								
GP-89	0.7	2.1	2.6	10	C	TR-148A	100	1000	5 kA peak 0.1 coulomb	3 millicoulombs/shot I _b = 35 mA dc I _p = 6 A ac
GP-90	1.3	3.4	4.2		C					
GP-91	4.4	10	12.5		A, C					
GP-93	8	20	25		A, C					
GP-82B	0.4	1.6	2	10	A, B	TR-148A	30	300	7.5 kA peak 0.2 coulomb	4 millicoulombs/shot I _b = 60 mA dc I _p = 8 A ac
GP-31B	2	6	7.5		A					
GP-20B	3.5	11	14		A					
GP-46B	8	20	25		A					
GP-85	2	6	8	20	A, B	TR-1795	30	300	25 kA peak 0.4 coulomb	4 millicoulombs/shot I _b = 100 mA dc I _p = 10 A ac
GP-86	6	15	20		A	TR-180B				
GP-87	10	24	30		A	TR1700				
GP-70	12	36	42(3)		A, B					
GP-30B	2	6	7.5	20	A, B	TR-1795	30	300	50 kA peak 0.5 coulomb	10 millicoulombs/shot I _b = 200 mA dc I _p = 15 A ac
GP-22B	6	15	19		A					
GP-12B	10	24	30		A					
GP-14B	12	36	42(3)		A, B	TR-1795				
GP-41B	12	36	42	20	A	TR-1700	30	300	Peak currents up to 100 kA and charge transfer up to 5 coulombs are obtainable at reduced life (100-1000 shots).	
GP-32B	20	48	60(3)		A					
GP-15B	25	60	86(3)		A					
GP-74B	40	100	120(3)		A	TR-1795				
GP-81B	40	100	120(9)	20	A	TR-1700	30	300		

Notes

1. Optimum operating voltage is typically 60 to 80% of SBV.
2. Operation below minimum value may result in erratic firing over time.
3. Operation at this value may result in self-firing over time.
4. Represents minimum main-gap breakdown voltage with no trigger applied.
5. Value shown contains safety factor for end-of-life requirements.
6. PerkinElmer TM-11A Trigger Module can be used to trigger all gaps.
7. Transformers listed vary mechanically and electrically. See PerkinElmer Transformer Data Sheet.
8. These units must be operated in a liquid or gas dielectric to prevent external flashover: GP-70 and GP-14B, above 24 kV; GP-32B and GP-15B, above 35 kV; GP-74B and GP-81B, above 60 kV.
9. Designed for high altitude, high holdoff conditions.
10. Other voltage ranges and mechanical configurations are available on request; for example, the GP-20B can be supplied with a 6 to 16 kV operating range by specifying GP-20B-20. The 20 would be the SBV and E-E maximum would be 90% of SBV - 16kV.
11. E = Stored energy in joules ($\frac{1}{2}CV^2$), I_b = average current in amperes, I_p = RMS current in amperes, R = total circuit resistance in ohms, P = average power in watts.

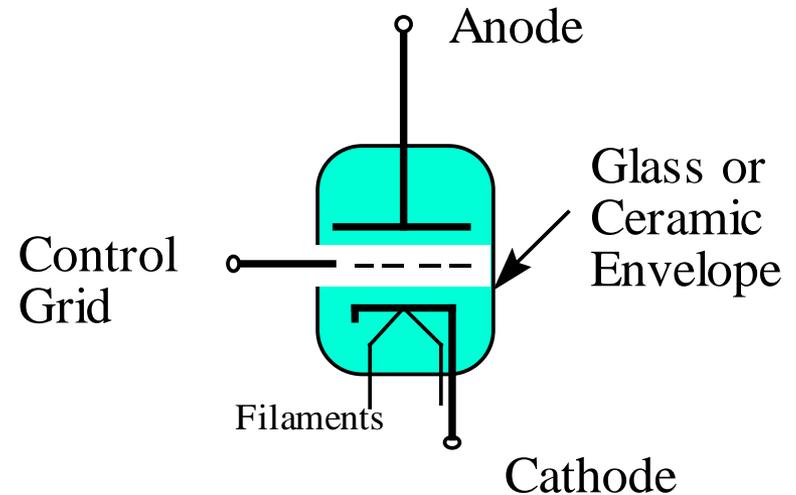


Thyratrons

- Closing switch, forward drop ~ 100 V
- High voltage: kV to ~ 100 kV (normally ~ 30 - 40 kV per internal gap)
- Maximum peak current 20-40 kA
- Gas filled: 0.1-5.0 torr hydrogen or deuterium and hot cathode
 - Operate on the low pressure side of Paschen minimum
- High repetition rate: limited by recovery time after conduction of 30-100 μ s
- Low jitter (<1 ns) with appropriate trigger
- Limited di/dt (emission limitations of hot cathode)
- Turn-on time (anode voltage fall time)
 - 20 ns typical
 - ~ 5 ns for special tubes
- Lifetime usually limited by cathode depletion (1-2 years of continuously on operation) or loss of ability to control gas pressure (causes misfires, reduction of standoff voltage capability)
- Limited pulse duration
- Low average current rating
- Significant voltage reversal (>4 kV) during recovery can damage tube

Thyratrons

- Envelope: glass or ceramic (high power tubes)
- Anode materials: molybdenum, copper
- Grid materials: copper, molybdenum
- Cathode material: BaO, SrO, CaO coating on tungsten or barium aluminate impregnated tungsten
- Reservoir (maintains gas pressure over life of tube) is a hydride material such as titanium, tantalum, etc.



Thyratrons



Thyratrons are fast acting high voltage switches suitable for a variety of applications including radar, laser and scientific use.

PerkinElmer's thyratrons are constructed of ceramic and metal for strength and long life. Over 300 thyratron types are available from PerkinElmer. The types listed in this guide are a cross section of the broad line available. We encourage inquiries for thyratrons to suit your particular application.

Features

- Wide operating voltage range
- High pulse rate capability
- Ceramic-metal construction
- High current capability
- Long life

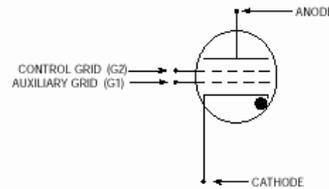


Figure 1. Thyratron with auxiliary grid (heater detail not shown)

How a Thyratron works

The operation of the device can be divided into three phases: triggering and commutation (closure), steady-state conduction, and recovery (opening), each of which is discussed below.

Triggering and Commutation

When a suitable positive triggering pulse of energy is applied to the grid, a plasma forms in the grid-cathode region from electrons. This plasma passes through the apertures of the grid structure and causes electrical breakdown in the high-voltage region between the grid and the anode. This begins the process of thyratron switching (also called commutation). The plasma that is formed between the grid and the

anode diffuses back through the grid into the grid-cathode space. "Connection" of the plasma in the anode-grid space with the plasma in the cathode-grid space completes the commutation process. The commutation process is simply modeled as shown in Figure 2.

The time interval between trigger breakdown of the grid-cathode region and complete closure of the thyratron is called the anode delay time. It is typically 100-200 nanoseconds for most tube types.

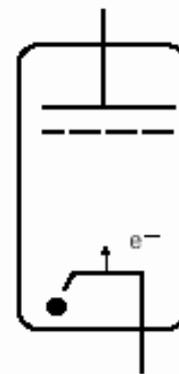
During commutation, a high voltage spike appears at the grid of the thyratron. This spike happens in the time it takes for the plasma in the grid-anode space to "connect" to the plasma in the grid-cathode space. During this time, the anode is momentarily "connected" to the grid thereby causing the grid to assume a voltage nearly that of the anode's.

Although the grid spike voltage is brief in duration, usually less than

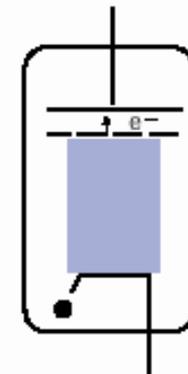
Thyratron -Operation

100 nS, it can damage the grid driver circuit unless measures are taken to suppress the spike before it enters the grid driver circuit. The location of the grid spike suppression circuit is shown in Figure 3, Grid Circuit.

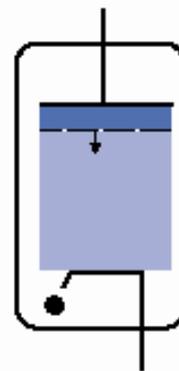
Figure 4, Typical Grid Spike Suppression Circuits, shows the more common methods used to protect the grid driver circuit. In using any of these types of circuits, care must be exercised to assure that the Grid Driver Circuit pulse is not attenuated in an unacceptable manner. The values for the circuit components are dependent on the characteristics of the thyatron being driven, the



1. Trigger pulse applied to control grid.

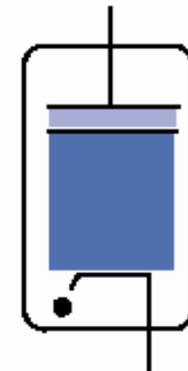


2. Grid-cathode breakdown.



Propagating Plasma Front

3. Electrons from grid-cathode region create a dense plasma in the grid-anode region. The plasma front propagates toward the cathode via breakdown of gas.



4. Closure

Figure 2. Thyatron commutation

Thyratron - Operation

grid driver circuit design, and the performance required from the thyratron itself. Contact the applications engineering department at PerkinElmer to discuss the specific details of your requirement.

Conduction

Once the commutation interval has ended, a typical hydrogen thyratron will conduct with nearly constant voltage drop on the order of 100 volts regardless of the current through the tube.

Recovery

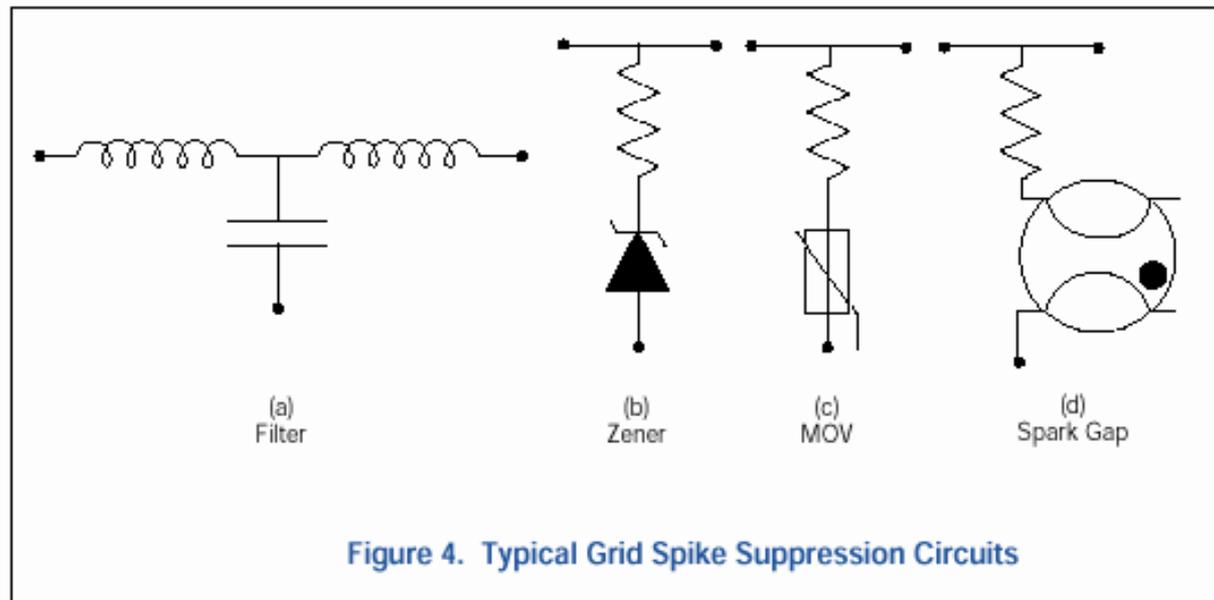
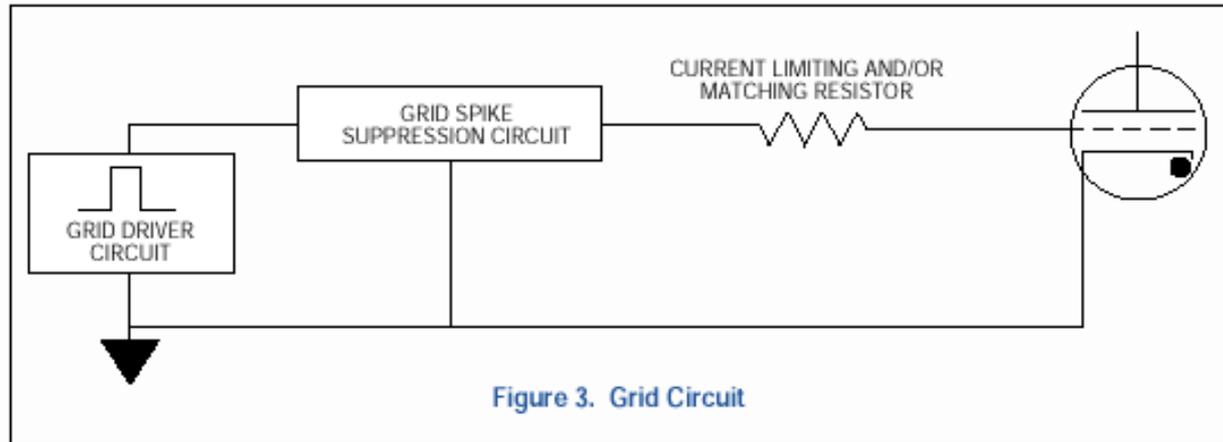
Thyratrons open (recover) via diffusion of ions to the tube inner walls and electrode surfaces, where the ions can recombine with electrons. This process takes from 30 to 150 microseconds, depending on the tube type, fill pressure, and gas (hydrogen or deuterium). The theoretical maximum pulse repetition rate is the inverse of the recovery time.

Recovery can be promoted by arranging to have a small negative DC bias voltage on the control grid when forward conduction has ceased. A bias voltage of 50 to 100 volts is usually sufficient.

Recovery can also be improved by arranging to have small negative voltage on the anode after forward conduction has ceased. In many radar circuits, a few-percent negative mismatch between a pulse-forming network and the load ensures a residual negative anode voltage. In laser circuits, classical pulse-forming networks are seldom used, so inverse anode voltage may not be easily generated. Recovery then strongly depends on the characteristics of the anode charging circuit. In general, charging schemes

involving gently rising voltages (i.e., resonant charging and ramp charging) favor thyratron recovery, and therefore allow higher pulse repetition rates. Fast ramping and resistive charging put large voltages on the anode quickly, thus making recovery more difficult. The ideal charging scheme from the viewpoint of thyratron recovery is command charging, wherein voltage is applied to the thyratron only an instant before firing.

Thyratrons





Thyratrons

Type	Peak Anode Voltage (kV)	Peak Anode Current (a)	Average Anode Current (Adc)	RMS Anode Current (Aac)	Plate Dissipation Factor Pb ($\times 10^9$)	Cathode Heater V/A	Reservoir Heater V/A	Peak Forward Grid Voltage (V)	Impedance of Grid Circuits (Max)	EIA Type & Comments	Notes	Seated Height x Tube Width (Inches)
HY-2	8	100	0.1	2	2.7	6.3/3.5	Note 1	175	1200	JAN 7621	1	2.35 x 1.0
HY-6	16	350	0.5	6.5	5	6.3/7	6.3/2.5	150	1500	JAN 7782		2 x 1.4
HY-60	16	350	0.5	6.5	5	6.3/7	6.3/7	150	1500	JAN 7865A		2.4 x 1.4
HY-61	16	350	0.5	6.5	5	6.3/8.5	Note 1	150	1500		1	3.6 x 1.4
HY-10	20	500	0.5	8	10	6.3/7.5	6.3/4	200	500	JAN 7620		3.4 x 2
HY-11	18	1600	0.5	8	10	6.3/7.5	6.3/4	200	500			2.2 x 2.25
HY-1A	18	500	0.5	8	10	6.3/11	Note 1	175	500	JAN8613	1	5 x 2
HY-1102	18	1000	0.5	16	10	6.3/7.5	6.3/8	20	500		2	2 x 2
HY-3192	32	1000	2.2	47.5	50	6.3/12.5	6.3/5.5	1500	250		3	3.75 x 3.25
HY-32	32	1500	2.2	47.5	50	6.3/18	6.3/5.5	450	400		4	4 x 3.25
HY-3204	32	1500	1	25	40	6.3/18	6.3/8	450	400	ib to 10kA @ <1usec	4	3 x 6
1802	25	5000	2.2	47.5	50	6.3/12.5	6.3/5.5	500	400	JAN 7322	4	4 x 3.25
HY-3002	25	5000	2.2	47.5	50	6.3/12.5	6.3/5.5	500	400			4 x 3.25
HY-3003	35	5000	2.2	47.5	50	6.3/12.5	6.3/5.5	500	400			4 x 3.25
HY-3004	25	5000	2.2	47.5	50	6.3/12.5	6.3/5.5	500	400			4.75 x 3.25
HY-3005	35	5000	2.2	47.5	50	6.3/12.5	6.3/5.5	500	400		3	4.75 x 3.25
HY-3025	28	5000	2.2	47.5	50	6.3/12.5	6.3/5.5	500	250			4.25 x 3.25
HY-3189	32	5000	2.2	47.5	50	6.3/12.5	6.3/5.5	500	250			3.75 x 3
HY-5	40	5000	8	125	180	6.3/30	4.5/11	1300	100	8614		5 x 4.5
HY-53	40	5000	4	90	100	6.3/30	4.5/11	1300	100		3	5 x 4.5
LS-3101S	35	5000	2	45	50	6.3/18	6.3/8	500	250		6	5.25 x 3
LS-4101	40	12000	3	55	50	6.3/28	6.3/8	500	250		3,6	8 x 3.5
LS-4111	40	12000	3	55	100	6.3/28	6.3/8	500	250		3,5,6	8.25 x 3.5
HY-3246	45	15000	2	45	50	6.3/16	6.3/8	500	250	Two gap tetrode		5.75 x 3
LS-3229	70	15000	2	45	50	6.3/16	6.3/8	450	400		3,6	6.4 x 3
HY-3202	32	20000	0.5	47.5	50	6.3/18	6.3/13	500	250		2,6	6.4 x 3
LS-5001	40	20000	4	90	100	6.3/29	4.5/10	2500	50		3	6.75 x 4.5
LS-5002	50	20000	4	70	100	6.3/35	4.5/15	2500	100	Two gap tetrode	3	9.5 x 4.5
LS-5101	40	20000	4	90	100	6.3/29	4.5/10	2500	50		3,6	6.75 x 4.5
LS-5111	40	20000	4	90	200	6.3/29	4.5/10	2500	50		3,5,6	7.2 x 4.5



Thyratrons - Definition of Terms

TERMS USED TO CHARACTERIZE INDIVIDUAL PULSES

Peak Anode Voltage (epy): maximum positive anode voltage, with respect to the cathode.

Peak Inverse Anode Voltage (epx): maximum negative anode voltage, with respect to the cathode.

Peak Forward Anode Current (ib): maximum instantaneous positive anode current.

Peak Inverse Current (l_{bx}): maximum instantaneous negative anode current.

Pulse Width (t_p): current pulse full-width at half-maximum.

Pulse Repetition Rate (pr): average number of pulses/second.

Current Rise Time (t_r): time for the forward current to rise from 10% to 90% of its peak value.

Anode Fall Time: time for the forward anode voltage to collapse from 90% to 10% of its maximum value.

Anode Delay Time (t_{ad}): time interval between triggering and commutation (commutation is defined below). The precise reference points for this interval vary with the application.

Anode Delay Time Drift (Δt_{ad}): gradual decrease in anode delay time that occurs as the thyatron warms up.

Jitter (t_j): pulse-to-pulse variation in anode delay time.

TIME AVERAGED QUANTITIES

DC Average Current (I_b): forward current averaged over one second.

RMS Average Current (I_p): root-mean-square current averaged over one second.

Plate Breakdown Factor (P_b): numerical factor proportional to the power dissipated at the anode, averaged over one second. $P_b = epy \times ib \times pr$.



Thyratrons - Definition of Terms

STRUCTURAL PARTS OF THE THYRATRON

Auxiliary Grid: grid placed between the control grid and cathode in some thyratrons. A small DC current (or a larger pulsed current) applied between Auxiliary Grid and cathode can be used to control the anode delay time. (Anode delay time is defined above). Thyratrons with auxiliary grids are called Tetrode Thyratrons.

Reservoir: maintains the gas pressure in the tube at a level which depends on the reservoir heater voltage.

GENERAL TERMINOLOGY

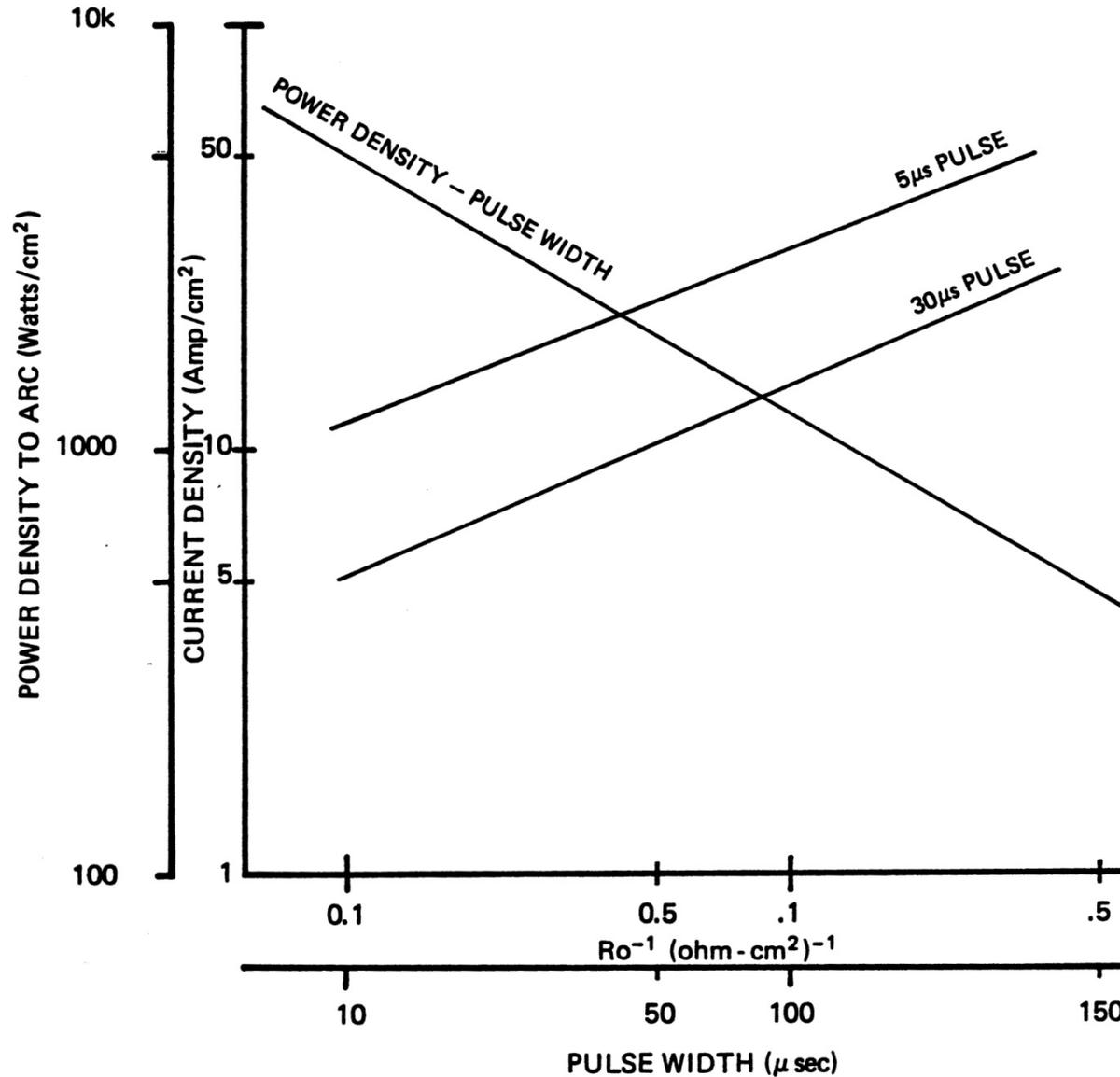
Static (Self) Breakdown Voltage (SBV): applied voltage at which a thyratron will break down spontaneously, without being triggered.

Commutation: transition from trigger breakdown to full closure of the thyratron.

Recovery Time: time which must elapse after decay of the circuit current before anode voltage can be reapplied to the thyratron without causing self-breakdown. The maximum possible pulse repetition rate is the inverse of the recovery time.

Grid Bias: negative DC voltage which may be applied to the control grid to speed up recovery.

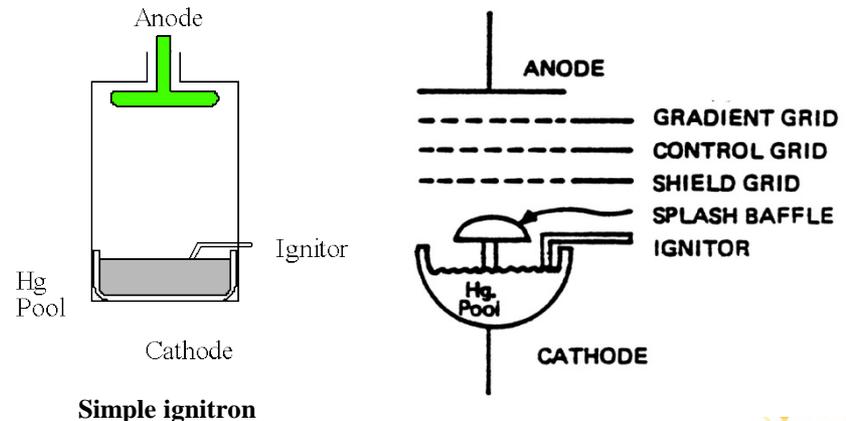
Thyratron Tradeoffs



Ignitron

- Mercury filled switch
- Low pressure device: ~ 0.001 Torr @ 70° F
- High voltage, high current (kA to 100's kA)
- Very simple device with many operational issues
 - Mounting (must be mounted vertically)
 - Vibration
 - Anode needs to be heated to keep mercury evaporated off
 - Ringing discharge affects lifetime
 - Has rep-rate limits and requires temperature control
- Operating voltage affected by tube pressure and electrode condition
- Current affected by plasma instabilities
- Jitter and turn-on delays issues

Anode material - molybdenum or graphite
 Grids - graphite
 Igniter - boron carbide





Plasma Opening Switch (POS)

- Initially, a high density plasma forms a low-conductivity channel (switch closed)
- Plasma conductivity is rapidly increased, ~10 to 100 ns, opening the switch
- Opening mechanisms
 - Plasma erosion switch: plasma source is turned off, conductive particles are swept out by applied fields (plasma erodes), switch opens
 - Applied fields inhibit the flow of conductive particles (electrons) across switch
- Used primarily in effects simulators
- Voltage: >MV
- Current: >MA

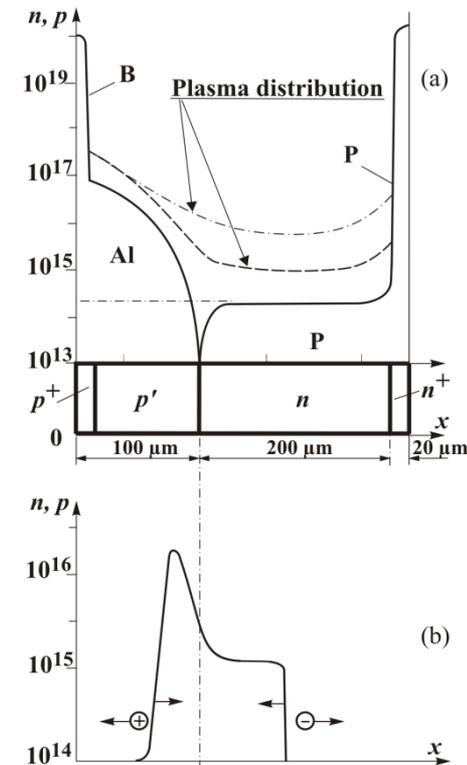


Solid-state Devices - General Observations

- Low jitter (ns)
- Switching speed varies from very fast (ns) to slow(100's μ s)
- Limited in peak power capability. High voltage requires series stacks and high peak current requires parallel arrays.
- Usually high average current capability (compared with thyratrons)
- Both closing devices and opening devices available
- Most can operate at high repetition rate
- Low cost in terms of average power rating
- Long lifetime if operated within peak ratings, but usually catastrophic failure when voltage ratings exceeded

Diode Opening Switch

- Solid state equivalent to POS
- Forward bias junction, switch closed
- Reverse bias switch, carriers swept from junction, when carriers are depleted, switch is open
- Any diode will work, but, ideally junction carrier density remains constant until all remaining carriers are swept out of gap
 - Dependent on doping profile across junction
 - Carrier crossing time (500 V, Si junction): ~ 0.5 ns
 - Electrons $\sim 3X$ faster than holes
 - Drift Step Recovery Diode/Device (DSRD), approximates ideal



DSRD: (a) design and “plasma” distribution, --- dc bias, ---- pulse bias, (b) “plasma” distribution at start of reverse bias

Grekhov, et.al., 2004 PMC



Thyristors

- Closing switch
- Maximum voltage:
 - Silicon: ~6.5 kV, limited by defects
 - Silicon carbide: ~20 kV, not commercially available
- Maximum current
 - RMS: ~5 kA
 - Pulsed: 10 to 100X (or more) greater (pulse length dependent)
- Low forward drop, <3 V (typical), low loss
- Simple to trigger
- All types of thyristors can be triggered by applying high dV/dt
- Generally, slow switch for pulsed power applications

Thyristors (cont.)

- Silicon Controlled Rectifier (SCR)
 - Simple, powerful, relatively inexpensive
 - Switching speed
 - Phase Control: intended for 50/60 Hz operation
 - Inverter grade: $\sim 10 \mu\text{s}$ (typical)
 - Triggering
 - Low energy trigger switches device, will remain on as long as $I_{\text{conducted}} > I_{\text{threshold}}$
 - Electrical
 - $\sim 3 \text{ V}$
 - $< \text{mA}$ small devices, $< \text{A}$ largest devices
 - Optical
- Closing/opening devices
 - Gate turn-off thyristor (GTO)
 - Integrated gate commutated thyristor (IGCT)
 - Limited use in pulsed power

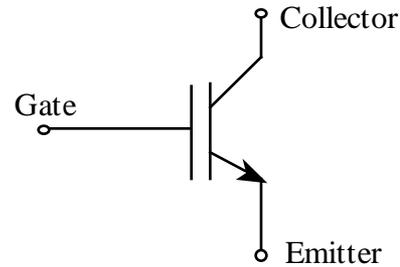


Bulk Semiconductor Switches

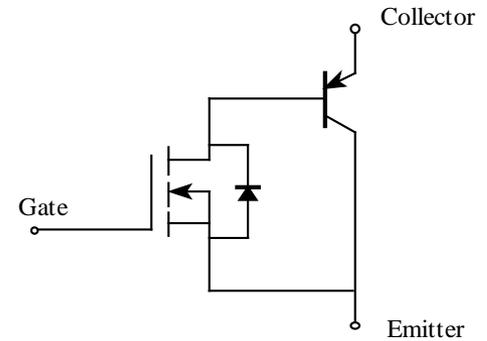
- Bulk semiconductor materials; Si, GaAs, diamond-like carbon, can be used as a switch
- Carriers can be produced through the bulk of the material by depositing energy; photons (laser) or electron beam, to trigger the switch
- If trigger induces carrier avalanching, then can only operate as a closing switch, if not avalanching, then removal of trigger source will cause switch to open
- Not commercially available at present, but subject to ongoing investigation and development
- Potential for very high power solid state switch

Power Transistors

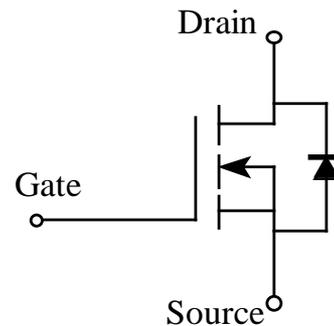
- Hard switch: closes and opens
- Bi-polar devices
 - Minority carrier devices
 - Conduction characterized by $V_{CE} < 3 \text{ V}$ (typical)
 - NPN/PNP power transistors generally replaced by Insulated Gate Bipolar Transistors (IGBT)
 - Lower drive power
 - Available at higher voltage, current and power
- Field effect transistors
 - Majority carrier devices
 - Metal Oxide Semiconductor Field Effect Transistor (MOSFET)
 - Conduction characterized by $R_{DS-ON} \sim \Omega$



Symbol



Equivalent Circuit



Symbol (N-type)



IGBT

- Wide-spread use in power electronics → availability of high power modules
 - Voltages: 600 V, 1.2 kV, 1.7 kV, 3.3 kV, 4.5 kV, 6.5 kV
 - Currents: to ~kA average
 - Pulsed current, ~ μ s pulse duration, to ~10X greater
 - Configurations: single die, single switch-parallel die, chopper, bridge
- Switching characteristics
 - Turn on
 - Ultra-fast (single die): as fast as ~50 ns
 - Power modules: ~0.5 μ s (with sophisticated triggering)
 - Turn off
 - Initial turn off is fast, ~turn on time
 - Tail: following initial turn off, a low current tail (~ A to 10's of A) due to carrier recombination may persist for μ s to 10's of μ s, full voltage across device → high dissipation
 - Switching losses typically dominate device dissipation, small devices may operate to ~MHz, power modules typically operate at 10 to 50 kHz or less



IGBT (cont.)

- Switching
 - Insulated gate structure, capacitive load to trigger circuit
 - Threshold (to turn on) ~ 5 V
 - Maximum gate voltage ~ 30 V (higher voltage may punch through oxide)
 - Typically bias gate to 10 – 15 V
 - Saturation current (V_{CE} increases dramatically for $I > I_{SAT}$) $\propto V_{GE}$
 - Low I_{SAT} limits fault current, protects device/system
 - V_{CE} only weakly dependent on V_{GE}
 - Optimum (fastest, lowest loss) triggering
 - 2-stage:
 - HV (50 to >100 V): initiates current flow to gate (parasitic L)
 - 2nd ary drive holds gate at 10 – 15 V
 - Bi-polar, fast turn off requires inverse pulse
 - Does not significantly reduce tail
 - Turn off slowly from fault condition, may lose control if $L \, di/dt$ is too high



IGBT (cont.)

- Easily damaged by reverse voltage (>100 V)
 - Include anti-parallel diode in circuit
 - Integrated into modules
- “Traction motor” modules
 - “Single wide”: 12 chips: 8 IGBT/4 diode
 - Internal interconnections may promote oscillations between chips under fault conditions
- Exercise caution when connecting in parallel
 - Often have negative coefficient of V_{CE} with temperature
 - Device carrying excess current than neighbors will get hotter, forward voltage will drop, and it will carry even more current



IGBT Reliability Considerations

- Collector-Emitter voltage, V_{CE}
 - Exceeding, even momentarily, will damage/destroy device
 - Usually limit nominal off-state voltage to 67% of V_{CE}
- Cosmic ray withstand voltage
 - Statistical probability dies will be struck by cosmic ray, if $V >$ withstand voltage, die will fail. Limits “normal” voltage across device.
 - Not always on data sheet, ask manufacturer, typically ~60% of V_{CE}
- Partial discharge rating/insulation capability
 - International standard sets minimum voltage cycle that results in 10 pC internal discharge for package rating (e.g. 3.3 kV device). Exceeding voltage will shorten device life.
- Thermal
 - Exceeding maximum die temperature will result in rapid failure of device
 - Thermal cycling
 - Die temperature variations (as device cycles on/off) fatigue bond wires
 - Manufacturer can provide data to determine impact on life for a calculated cycle



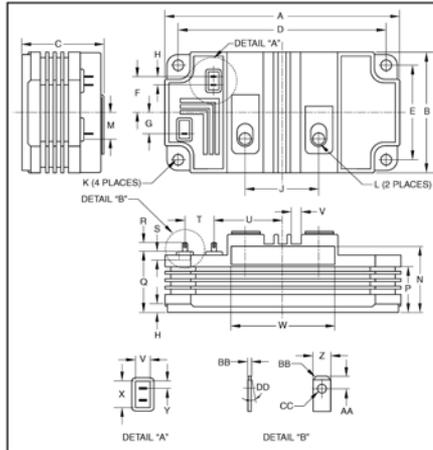
IGBT Data Sheet



Powerex, Inc., 200 E. Hillis Street, Youngwood, Pennsylvania 15697-1800 (724) 925-7272

CM200HG-130H

Single IGBTMOD™
HVIGBT Module
200 Amperes/6500 Volts



Outline Drawing and Circuit Diagram

Dimensions	Inches	Millimeters	Dimensions	Inches	Millimeters
A	5.51	140.0	Q	1.44	36.5
B	2.87	73.0	R	0.22	5.5
C	1.89±0.04/-0.0	48.0±1.0±0.0	S	0.16	4.0
D	4.88	124.0	T	0.68	17.4
E	2.24	57.0	U	1.61	41.0
F	0.85	21.6	V	0.24	6.0
G	0.51	12.9	W	2.44	62.0
H	0.20	5.0	X	0.47	12.0
J	1.73	44.0	Y	0.14	3.5
K	M8 Metric	M6	Z	0.11	2.8
L	M8 Metric	M8	AA	0.06	1.6
M	0.64	16.2	BB	0.02	0.5
N	1.59	40.4	CC	0.05 Dia.	1.2 Dia.
P	1.10	28.0	DD	10°	10°



Description:
Powerex IGBTMOD™ Modules are designed for use in switching applications. Each module consists of one IGBT Transistor in a reverse-connected super-fast recovery free-wheel diode. All components and interconnects are isolated from the heat sinking baseplate, offering simplified system assembly and thermal management.

Features:

- Low Drive Power
- Low V_{CE(sat)}
- Super-Fast Recovery Free-Wheel Diode
- Isolated Baseplate for Easy Heat Sinking

Applications:

- Traction
- Medium Voltage Drives
- High Voltage Power Supplies

Ordering Information:

Example: Select the complete part module number you desire from the table below -i.e. CM200HG-130H is a 6500V (V_{CE(s)}), 200 Ampere Single IGBTMOD™ Power Module.

Type	Current Rating Amperes	V _{CE(s)} Volts (±50)
CM	200	130



Powerex, Inc., 200 E. Hillis Street, Youngwood, Pennsylvania 15697-1800 (724) 925-7272

CM200HG-130H
Single IGBTMOD™ HVIGBT Module
200 Amperes/6500 Volts

Absolute Maximum Ratings, T_J = 25 °C unless otherwise specified

Ratings	Symbol	CM200HG-130H	Units
Junction Temperature	T _J	-40 to 150	°C
Storage Temperature	T _{stg}	-40 to 125	°C
Operating Temperature	T _{opr}	-40 to 125	°C
Collector-Emitter Voltage (V _{GE} = 0V, T _J = -40°C)	V _{CE(s)}	5800	Volts
Collector-Emitter Voltage (V _{GE} = 0V, T _J = +25°C)	V _{CE(s)}	6300	Volts
Collector-Emitter Voltage (V _{GE} = 0V, T _J = +125°C)	V _{CE(s)}	6500	Volts
Gate-Emitter Voltage (V _{CE} = 0V)	V _{GES}	±20	Volts
Collector Current (DC, T _C = 80°C)	I _C	200	Amperes
Peak Collector Current (Pulse)	I _{CM}	400*	Amperes
Emitter Current** (T _C = 25°C)	I _E	200	Amperes
Emitter Surge Current** (Pulse)	I _{EM}	400*	Amperes
Maximum Collector Dissipation (T _C = 25°C, IGBT Part, T _{J(max)} ≤ 125°C)	P _C	2900	Watts
Partial Discharge (V ₁ = 6900 V _{rms} , V ₂ = 5100 V _{rms} , 60 Hz (Acc. to IEC 1287))	Q _{pd}	10	pC
Max. Mounting Torque M8 Main Terminal Screws	-	133	in-lb
Max. Mounting Torque M6 Mounting Screws	-	53	in-lb
Module Weight (Typical)	-	0.52	kg
Isolation Voltage (Charged Part to Baseplate, AC 60Hz 1 min.)	V _{iso}	10200	Volts
Maximum Turn-Off Switching Current (V _{CC} ≤ 4500V, V _{GE} = ±15V, R _{θ(jc)} ≥ 720, T _J = 125°C)	-	400	Amperes
Short Circuit Capability, Maximum Pulse Width (V _{CC} ≤ 4500V, V _{GE} = ±15V, R _{θ(jc)} ≥ 720, T _J = 125°C)	-	10	µs
Maximum Reverse Recovery Instantaneous Power (V _{CC} ≤ 4500V, di _{dv} /dt ≤ 1000A/µs, T _J = 125°C)	-	1200	kW

* Pulse width and repetition rate should be such that device junction temperature (T_J) does not exceed T_{opr(max)} rating (125°C).
** Represents characteristics of the anti-parallel, emitter-to-collector free-wheel diode (FWD).



IGBT Data Sheet (cont.)



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CM200HG-130H
Single IGBTMOD™ HVIGBT Module
200 Amperes/6500 Volts

Static Electrical Characteristics, $T_j = 25^\circ\text{C}$ unless otherwise specified

Characteristics	Symbol	Test Conditions	Min.	Typ.	Max.	Units
Collector-Cutoff Current*	I_{CES}	$V_{CE} = V_{CES}, V_{GE} = 0V, T_j = 25^\circ\text{C}$ $V_{CE} = V_{CES}, V_{GE} = 0V, T_j = 125^\circ\text{C}$	–	–	3.0 10 30.0	mA
Gate-Emitter Threshold Voltage	$V_{GE(th)}$	$I_C = 20\text{mA}, V_{CE} = 10V$	5.0	6.0	7.0	Volts
Gate Leakage Current	I_{GES}	$V_{GE} = V_{GES}, V_{CE} = 0V$	–	–	0.5	μA
Collector-Emitter Saturation Voltage	$V_{CE(sat)}$	$I_C = 200\text{A}, V_{GE} = 15V, T_j = 25^\circ\text{C}$ $I_C = 200\text{A}, V_{GE} = 15V, T_j = 125^\circ\text{C}$	–	5.1 5.0	–	Volts
Input Capacitance	C_{iB}	$V_{CE} = 10V, V_{GE} = 0V,$ $f = 100\text{kHz}$	–	41.0	–	nF
Output Capacitance	C_{oES}	$T_j = 25^\circ\text{C}$	–	2.5	–	nF
Reverse Transfer Capacitance	C_{res}	$T_j = 25^\circ\text{C}$	–	0.7	–	nF
Total Gate Charge	Q_G	$V_{CC} = 3600V, I_C = 200\text{A}, V_{GE} = 15V$	–	3.3	–	μC
Emitter-Collector Voltage**	V_{EC}	$I_E = 200\text{A}, V_{GE} = 0V, T_j = 25^\circ\text{C}$ $I_E = 200\text{A}, V_{GE} = 0V, T_j = 125^\circ\text{C}$	–	4.0 3.6	–	Volts
Turn-On Delay Time	$t_{d(on)}$	$V_{CC} = 3600V, I_C = 200\text{A},$ $V_{GE1} = -V_{GE2} = 15V, R_{G(on)} = 30\Omega,$ $T_j = 125^\circ\text{C}, t_{off} = 60\mu\text{s},$ Inductive Load	–	1.2	–	μs
Turn-On Rise Time	t_r	$V_{GE1} = -V_{GE2} = 15V, R_{G(on)} = 30\Omega,$ $T_j = 125^\circ\text{C}, t_{off} = 60\mu\text{s},$ Inductive Load	–	0.35	–	μs
Turn-On Switching Energy	E_{on}	$T_j = 125^\circ\text{C}, t_{off} = 60\mu\text{s},$ Inductive Load	–	1.5	–	J/P
Turn-Off Delay Time	$t_{d(off)}$	$V_{CC} = 3600V, I_C = 200\text{A},$ $V_{GE1} = -V_{GE2} = 15V,$ $R_{G(off)} = 72\Omega,$ $T_j = 125^\circ\text{C}, t_{off} = 60\mu\text{s},$ Inductive Load	–	6.6	–	μs
Turn-Off Fall Time 1	t_{f1}	$V_{GE1} = -V_{GE2} = 15V,$ $R_{G(off)} = 72\Omega,$ $T_j = 125^\circ\text{C}, t_{off} = 60\mu\text{s},$ Inductive Load	–	0.5	–	μs
Turn-Off Fall Time 2	t_{f2}	$R_{G(off)} = 72\Omega,$ $T_j = 125^\circ\text{C}, t_{off} = 60\mu\text{s},$ Inductive Load	–	3.3	–	μs
Turn-Off Switching Energy	E_{off}	$T_j = 125^\circ\text{C}, t_{off} = 60\mu\text{s},$ Inductive Load	–	1.2	–	J/P
Reverse Recovery Time 1**	t_{rr1}	$V_{CC} = 3600V, I_C = 200\text{A},$ $dI_C/dt = -670\text{A}/\mu\text{s},$ $T_j = 125^\circ\text{C}$	–	1.0	–	μs
Reverse Recovery Time 2**	t_{rr2}	$dI_C/dt = -670\text{A}/\mu\text{s},$ $T_j = 125^\circ\text{C}$	–	2.4	–	μs
Reverse Recovery Charge**	Q_{rr}	$T_j = 125^\circ\text{C}$	–	370	–	μC
Reverse Recovery Energy**	E_{rr}	$t_{off} = 60\mu\text{s},$ Inductive Load	–	0.7	–	J/P

* Pulse width and repetition rate should be such that device junction temperature rise is negligible.
** Represents characteristics of the anti-parallel, emitter-to-collector free-wheel diode (FWD).

Thermal Characteristics, $T_j = 25^\circ\text{C}$ unless otherwise specified

Characteristics	Symbol	Test Conditions	Min.	Typ.	Max.	Units
Thermal Resistance, Junction to Case	$R_{th(j-c)}$	Per IGBT	–	–	42.0	K/W
Thermal Resistance, Junction to Case	$R_{th(j-c)}$	Per FWD	–	–	66.0	K/W
Contact Thermal Resistance, Case to Fin	$R_{th(c-f)}$	Per Module, Thermal Grease Applied	–	18.0	–	K/W

Mechanical Characteristics, $T_j = 25^\circ\text{C}$ unless otherwise specified

Characteristics	Symbol	Test Conditions	Min.	Typ.	Max.	Units
Comparative Tracking Index	CTI	–	–	600	–	–
Clearance	–	–	–	26.0	–	mm
Creepage Distance	–	–	–	56.0	–	mm
Internal Inductance	$L_C-E(\text{int})$	–	–	54.0	–	μH
Internal Lead Resistance	$R_C-E(\text{int})$	–	–	–	–	m Ω

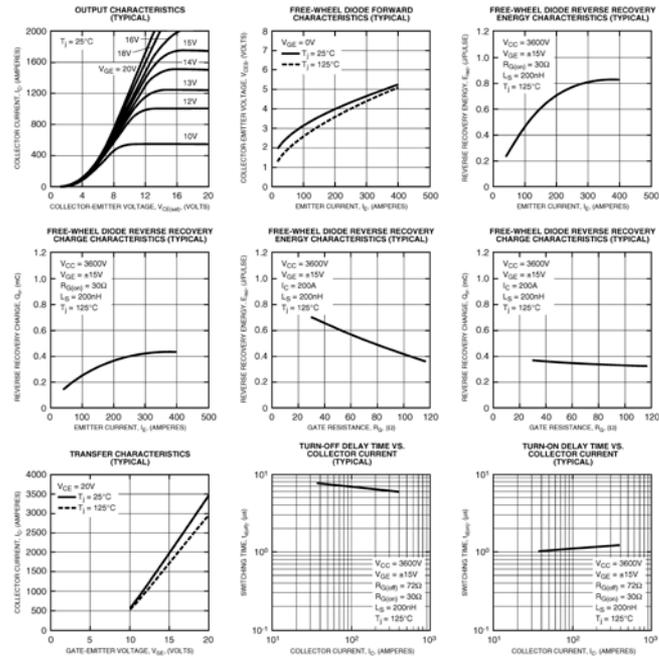
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CM200HG-130H
Single IGBTMOD™ HVIGBT Module
200 Amperes/6500 Volts



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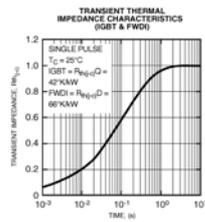
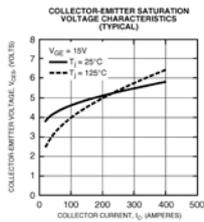
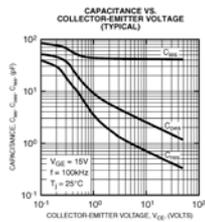
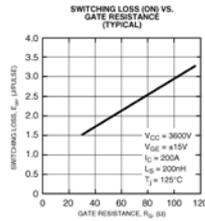
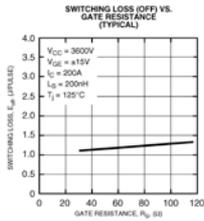
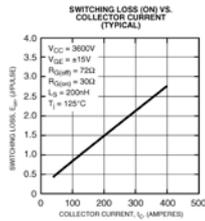
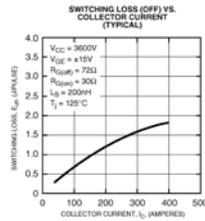
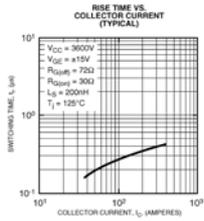
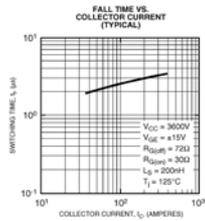


IGBT Data Sheet (cont.)



Powerex, Inc., 200 E. Hillis Street, Youngwood, Pennsylvania 15697-1800 (724) 925-7272

CM200HG-130H
Single IGBTMOD™ HVIGBT Module
200 Amperes/6500 Volts



805

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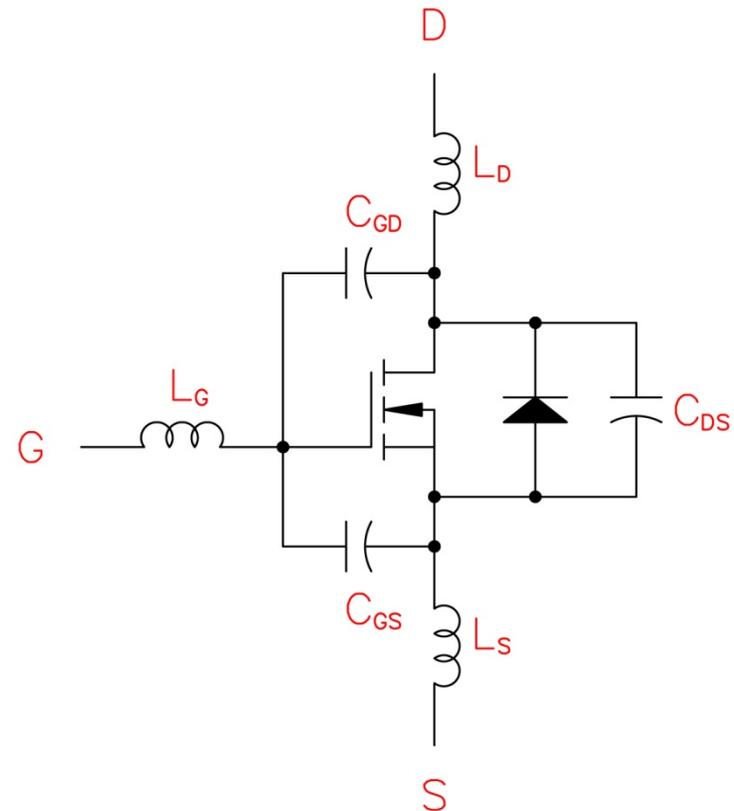


MOSFET

- Fastest commercial solid state switch available
 - Intrinsic turn on/off time \sim ns set by $R_{DS-ON}C_{OUTPUT}$ time constant (carrier junction crossing time much faster)
 - Effective switching time limited by input capacitance, stray packaging inductance, and dI_S/dt to ≥ 10 ns
- Maximum voltage: 1200 V
 - Avalanche rated, limited excursion to $V > V_{DSS}$ will not damage device
 - Can operate at near V_{DSS}
- Maximum current: ~ 0.1 kA (higher for modules and lower voltage FETs)
 - Pulsed current limited to $\sim 4X$ average rating due to increase in R_{DS-ON}
- “Intrinsic” reverse body diode, acts as anti-parallel diode
 - FREDFET: improved reverse body diode, soft recovery
- Well suited for parallel operation, positive coefficient of V_{DS} with temperature

MOSFET Model for Fast Switching

- Data sheet information
 - Drain-source breakdown voltage: V_{DSS}
 - Drain current
 - Continuous: I_D
 - Pulsed: I_{DM}
 - R_{DS-ON} @ I_D
 - Input capacitance: $C_{ISS} = C_{GD} + C_{GS}$
 - Output capacitance: $C_{OSS} = C_{DS}$
 - Reverse transfer capacitance (Miller capacitance): $C_{RSS} = C_{GD}$
- Typical values for 1 kV TO-247/264
 - L_D : <1 nH
 - L_G & L_S : ~6 nH
 - C_{ISS} : ~few nF
 - C_{OSS} & C_{RSS} : ~few 100 pF

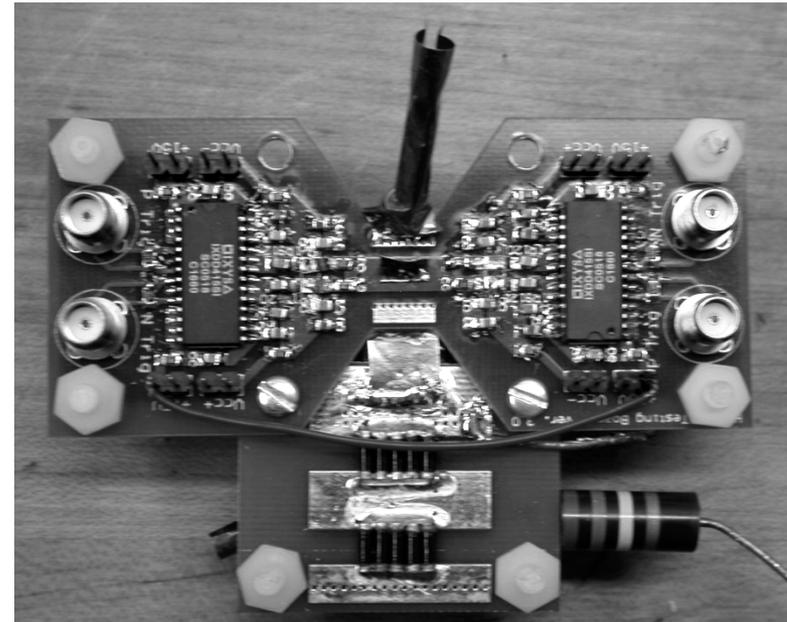
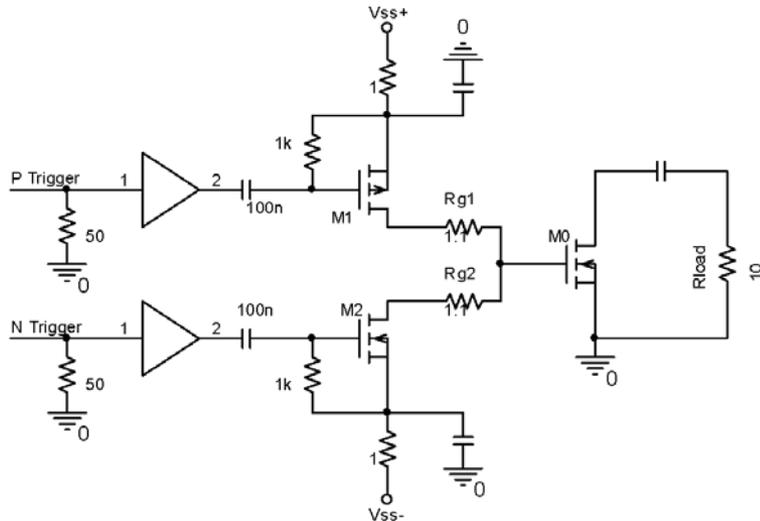




MOSFET Fast Switching

- Input capacitance and parasitic inductance form resonant circuit
 - $\omega < 10^9$, therefore $\tau_r \sim$ few ns will excite the resonance
 - $Z \sim$ few ohm, therefore need significant gate resistance to damp
- Inductive voltage due to rising source current: $L_S dI_S/dt$
 - 50 A in 10 ns would induce ~ 30 V across source inductance
 - Inductive voltage subtracts from applied gate voltage
- Effects are internal to package
 - May not see true causes of slow MOSFET turn on
- Remediations
 - Use a bi-polar high voltage gate drive (limited by gate breakdown)
 - Use high gate drive resistance (balance with drive current requirements)
 - Use a larger number of smaller MOSFETs in parallel
 - Integrate driver into MOSFET package
 - Commercial units show little gain
 - Hybrid circuits can achieve ~ 1 ns risetime

Hybrid MOSFET/Driver for Ultra-Fast Switching



Hybrid schematic: totem pole driver, output MOSFET, and load

Hybrid circuit; dual drivers on each side of PCB, MOSFET on bottom-side of PCB, load at bottom of photo

Tang & Burkhart, IPMC2008



MOSFET Data Sheet

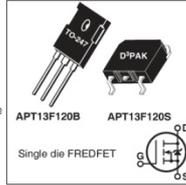


APT13F120B
APT13F120S

1200V, 13A, 1.40Q Max, t_{rr} ≤ 250ns

N-Channel FREDFET

Power MOS 8™ is a high speed, high voltage N-channel switch-mode power MOSFET. This "FREDFET" version has a drain-source (body) diode that has been optimized for high reliability in ZVS phase shifted bridge and other circuits through reduced t_{rr} , soft recovery, and high recovery dv/dt capability. Low gate charge, high gain, and a greatly reduced ratio of C_{rss}/C_{iss} result in excellent noise immunity and low switching loss. The intrinsic gate resistance and capacitance of the poly-silicon gate structure help control di/dt during switching, resulting in low EMI and reliable paralleling, even when switching at very high frequency.



FEATURES

- Fast switching with low EMI
- Low t_{rr} for high reliability
- Ultra low C_{rss} for improved noise immunity
- Low gate charge
- Avalanche energy rated
- RoHS compliant

TYPICAL APPLICATIONS

- ZVS phase shifted and other full bridge
- Half bridge
- PFC and other boost converter
- Buck converter
- Single and two switch forward
- Flyback

Absolute Maximum Ratings

Symbol	Parameter	Ratings	Unit
I_D	Continuous Drain Current @ $T_C = 25^\circ\text{C}$	13	A
	Continuous Drain Current @ $T_C = 100^\circ\text{C}$	8	
I_{DM}	Pulsed Drain Current ^①	50	
V_{GS}	Gate-Source Voltage	±30	V
E_{AS}	Single Pulse Avalanche Energy ^②	1070	mJ
I_{AR}	Avalanche Current, Repetitive or Non-Repetitive	7	A

Thermal and Mechanical Characteristics

Symbol	Characteristic	Min	Typ	Max	Unit
P_D	Total Power Dissipation @ $T_C = 25^\circ\text{C}$			625	W
$R_{\theta JC}$	Junction to Case Thermal Resistance			0.20	$^\circ\text{C}/\text{W}$
$R_{\theta CS}$	Case to Sink Thermal Resistance, Flat, Greased Surface		0.11		$^\circ\text{C}/\text{W}$
$T_{J,STG}$	Operating and Storage Junction Temperature Range	-55		150	$^\circ\text{C}$
T_L	Soldering Temperature for 10 Seconds (1.6mm from case)			300	$^\circ\text{C}$
W_T	Package Weight		0.22		oz
			6.2		g
Torque	Mounting Torque (TO-247 Package), 6-32 or M3 screw			10	in-lbf
				1.1	N·m

Microsemi Website - <http://www.microsemi.com>

050-8131 Rev. A 3-2007

050-8131 Rev. A 3-2007

Static Characteristics

$T_J = 25^\circ\text{C}$ unless otherwise specified

APT13F120B_S

Symbol	Parameter	Test Conditions	Min	Typ	Max	Unit
$V_{BR(DSS)}$	Drain-Source Breakdown Voltage	$V_{GS} = 0\text{V}, I_D = 250\mu\text{A}$	1200			V
$\Delta V_{BR(DSS)}/\Delta T_J$	Breakdown Voltage Temperature Coefficient	Reference to $25^\circ\text{C}, I_D = 250\mu\text{A}$		1.41		$\text{V}/^\circ\text{C}$
$R_{DS(on)}$	Drain-Source On Resistance ^③	$V_{GS} = 10\text{V}, I_D = 7\text{A}$		1.11	1.40	Ω
$V_{GS(th)}$	Gate-Source Threshold Voltage	$V_{DS} = V_{GS}, I_D = 1\text{mA}$		3	4	V
$\Delta V_{GS(th)}/\Delta T_J$	Threshold Voltage Temperature Coefficient			-10		$\text{mV}/^\circ\text{C}$
I_{DSS}	Zero Gate Voltage Drain Current	$V_{DS} = 1200\text{V}, T_J = 25^\circ\text{C}$			250	μA
		$V_{GS} = 0\text{V}, T_J = 125^\circ\text{C}$			1000	μA
I_{GSS}	Gate-Source Leakage Current	$V_{GS} = \pm 30\text{V}$			±100	nA

Dynamic Characteristics

$T_J = 25^\circ\text{C}$ unless otherwise specified

Symbol	Parameter	Test Conditions	Min	Typ	Max	Unit
g_{fs}	Forward Transconductance	$V_{DS} = 50\text{V}, I_D = 7\text{A}$		15		S
C_{iss}	Input Capacitance	$V_{GS} = 0\text{V}, V_{DS} = 25\text{V}$ $f = 1\text{MHz}$		4765		pF
C_{oss}	Reverse Transfer Capacitance			55		
C_{res}	Output Capacitance			350		
$C_{ref}^{\text{④}}$	Effective Output Capacitance, Charge Related	$V_{GS} = 0\text{V}, V_{DS} = 0\text{V to } 800\text{V}$		135		pF
$C_{ref}^{\text{⑤}}$	Effective Output Capacitance, Energy Related			70		
Q_g	Total Gate Charge	$V_{GS} = 0\text{ to } 10\text{V}, I_D = 7\text{A}$ $V_{DS} = 600\text{V}$		145		nC
Q_{gs}	Gate-Source Charge			24		
Q_{gd}	Gate-Drain Charge			70		
$t_{SD(on)}$	Turn-On Delay Time	Resistive Switching $V_{DD} = 800\text{V}, I_D = 7\text{A}$ $R_G = 4.7\Omega, V_{GS} = 15\text{V}$		26		ns
t_r	Current Rise Time			15		
$t_{SD(off)}$	Turn-Off Delay Time			85		
t_f	Current Fall Time			24		

Source-Drain Diode Characteristics

Symbol	Parameter	Test Conditions	Min	Typ	Max	Unit
I_S	Continuous Source Current (Body Diode)	MOSFET symbol showing the integral reverse p-n junction diode (body diode)			13	A
I_{SM}	Pulsed Source Current (Body Diode) ^⑥				50	
V_{SD}	Diode Forward Voltage	$I_{SD} = 7\text{A}, T_J = 25^\circ\text{C}, V_{GS} = 0\text{V}$			1.0	V
t_{rr}	Reverse Recovery Time	$T_J = 25^\circ\text{C}$			250	ns
		$T_J = 125^\circ\text{C}$			520	
Q_{rr}	Reverse Recovery Charge	$I_{SD} = 7\text{A}$			1.12	μC
		$d_{sw}/dt = 100\text{A}/\mu\text{s}$			3.03	
		$V_{DD} = 100\text{V}$			10	
I_{rm}	Reverse Recovery Current	$T_J = 25^\circ\text{C}$			10	A
		$T_J = 125^\circ\text{C}$			13.5	
dv/dt	Peak Recovery dv/dt	$I_{SD} \leq 7\text{A}, di/dt \leq 1000\text{A}/\mu\text{s}, V_{DD} = 800\text{V}, T_J = 125^\circ\text{C}$			25	V/ns

① Repetitive Rating: Pulse width and case temperature limited by maximum junction temperature.

② Starting at $T_J = 25^\circ\text{C}$, $L = 43.59\text{mH}$, $R_G = 4.7\Omega$, $I_{AS} = 7\text{A}$.

③ Pulse test: Pulse Width < 380 μs , duty cycle < 2%.

④ $C_{ref}^{\text{④}}$ is defined as a fixed capacitance with the same stored charge as C_{oss} with $V_{DS} = 67\%$ of $V_{BR(DSS)}$.

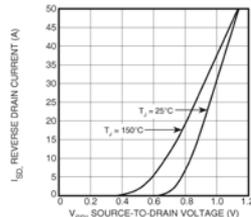
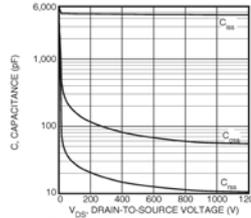
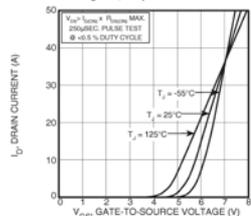
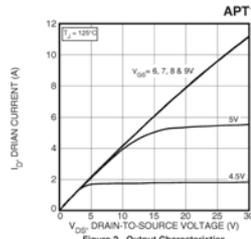
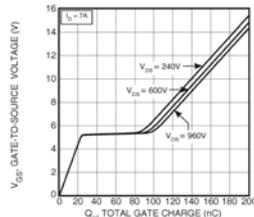
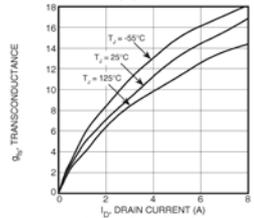
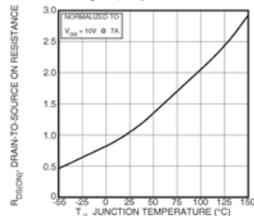
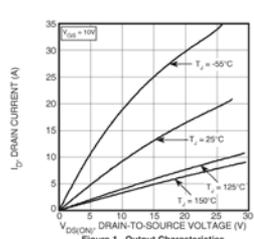
⑤ $C_{ref}^{\text{⑤}}$ is defined as a fixed capacitance with the same stored energy as C_{oss} with $V_{DS} = 67\%$ of $V_{BR(DSS)}$. To calculate $C_{ref}^{\text{⑤}}$ for any value of V_{DS} less than $V_{BR(DSS)}$, use this equation: $C_{ref}^{\text{⑤}} = -2.17E-7/V_{DS}^2 + 2.63E-8/V_{DS} + 3.74E-11$.

⑥ R_G is external gate resistance, not including internal gate resistance or gate driver impedance. (MIC4452)

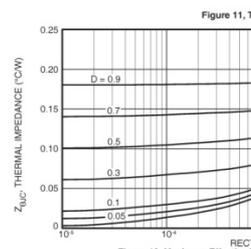
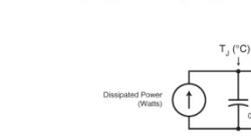
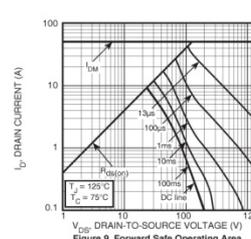
Microsemi reserves the right to change, without notice, the specifications and information contained herein.



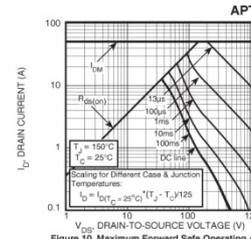
MOSFET Data Sheet



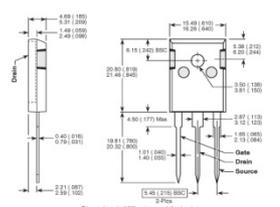
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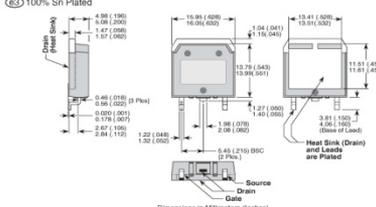
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TO-247 (B) Package Outline



D³PAK Package Outline



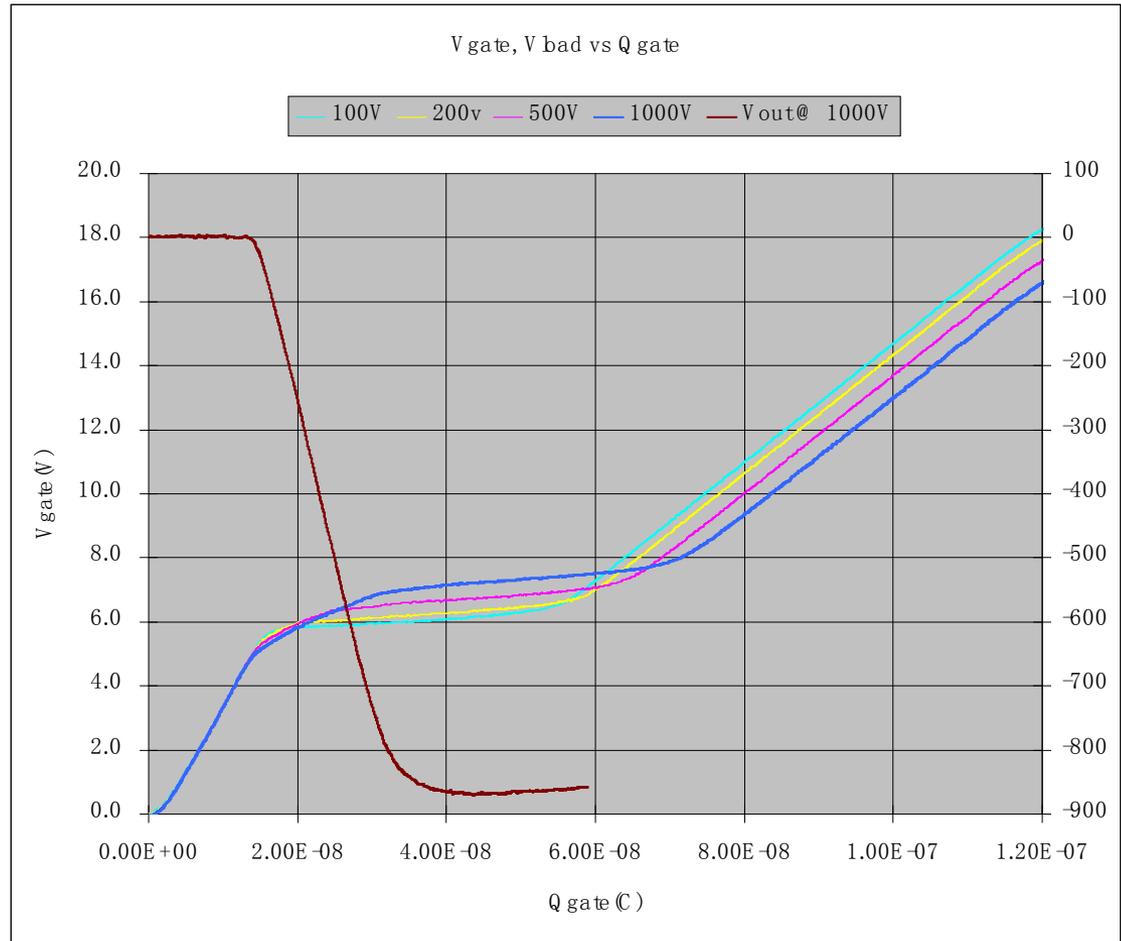
050-9131 Rev. A 3-2007

050-9131 Rev. A 3-2007

Microsemi's products are covered by one or more of U.S. patents 4,895,810 5,045,903 5,088,434 5,182,234 5,019,522 5,262,336 6,503,786 5,256,583 4,748,103 5,283,202 5,231,474 5,434,095 5,528,058 and foreign patents. US and Foreign patents pending. All Rights Reserved.

Interpretation of Hybrid MOSFET Data During Nanosecond Switching

- No switching until V_{GS} exceeds threshold
- Switching is effectively complete before Miller capacitance is fully charged ($\sim 20 \text{ nC} < Q < 60 \text{ nC}$)
- Ultra-fast is unlike normal MOSFET switching
 - Switching time depends on “linear” behavior of device
 - Sensitive to
 - Transistor gain, g_m
 - Die temperature
 - Device-to-device variations



Gate and drain-source voltage as a function of gate charge, for a range of initial MOSFET voltage

High Power Switching with Solid State Switches



- Peak switching power of commercial devices is limited
 - Array, series/parallel, devices to increase power
 - Use alternative topologies
- Arrays
 - Parallel
 - MOSFETs well suited
 - IGBTs may present challenges
 - Series
 - Prevent overvoltage of individual elements under ALL CONDITIONS
 - Derate device operating: reduces effective device power
 - Add protection (e.g. RC snubber): reduces switching speed

Commercial Suppliers

- Semiconductors
 - Power Semiconductors (MOSFETs, IGBTs, Thyristors)
 - APT: <http://www.advancedpower.com/> → Microsemi: <http://www.microsemi.com/>
 - EUPEC: <http://www.eupec.com/index.html> → Infineon: <http://www.infineon.com/>
 - Powerex/Mitsubishi: <http://www.pwrx.com/>
 - DYNEX: <http://www.dynexsemi.com/>
 - ST Microelectronics: <http://us.st.com/stonline/index.shtml>
 - Westcode: <http://www.westcode.com/>
 - International Rectifier: <http://www.irf.com/>
 - Toshiba: <http://www.toshiba.com>
 - ABB: <http://www.abb.com>
 - IXYS/DEI: <http://www.ixys.com/>
 - Driver Circuits
 - IXYS/DEI: <http://www.ixys.com/>
 - Vishay/Siliconix: <http://www.vishay.com/>
 - Intersil/Elantec: <http://www.intersil.com>