



U.S. Particle Accelerator School
Education in Beam Physics and Accelerator Technology



Elettra
Sincrotrone
Trieste

Transverse Geometric Wakefields, RF and Collimators

S. Di Mitri (90min.)

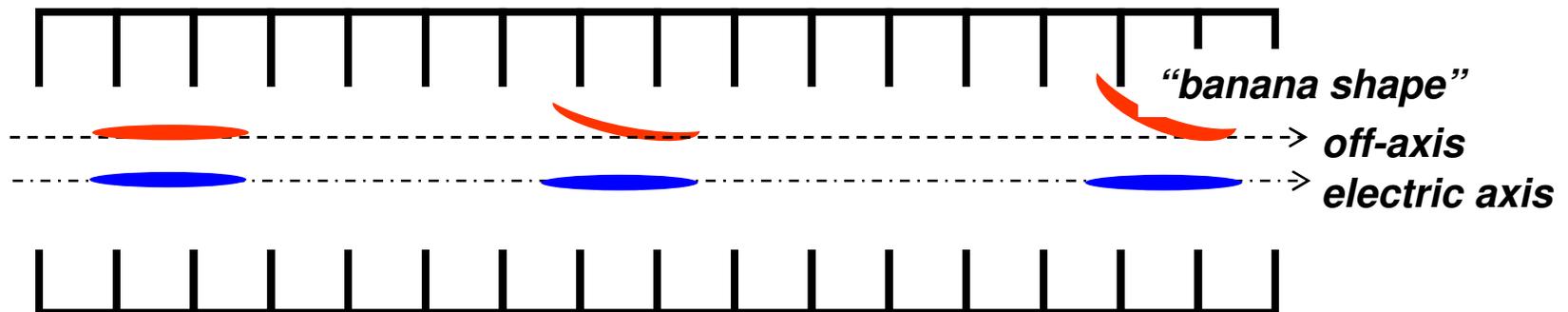
Geometric Transverse Wakefield in RF Structures

Picture courtesy
of S. Milton

Geometric Transverse Wakefield (GTW) describes the lateral kick imparted by the image charges to the e-beam as it passes in proximity of a (metallic) surface.

- The «causality principle» holds: beam leading particles “hurt” trailing ones. The **wake kick is correlated with the longitudinal particle position along the bunch.**

GTW is generated as the radial symmetry of the e.m. field brought by the beam is broken (“dipole mode”). Namely, it is generated by a **relative misalignment of the beam respect to the cavity electric axis** (coherent betatron oscillations).



The induced transverse **projected emittance growth** can be counteracted by “damping” the trailing particles’ oscillation amplitude:

- 1) by manipulating the particles’ energy distribution so that the bunch tail is focused back onto the axis (**BNS damping, chromatic effect**);
- 2) by pushing the beam off-axis on purpose so that multiple wake kicks eventually cancel each other (**emittance bumps, geometric effect**).

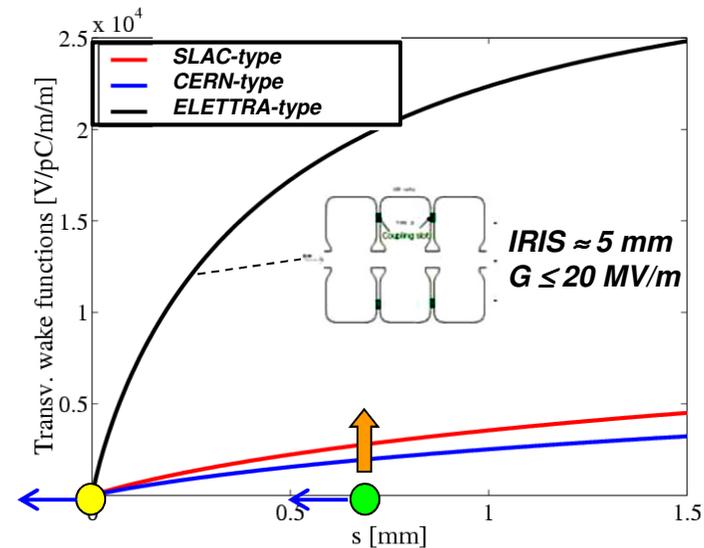
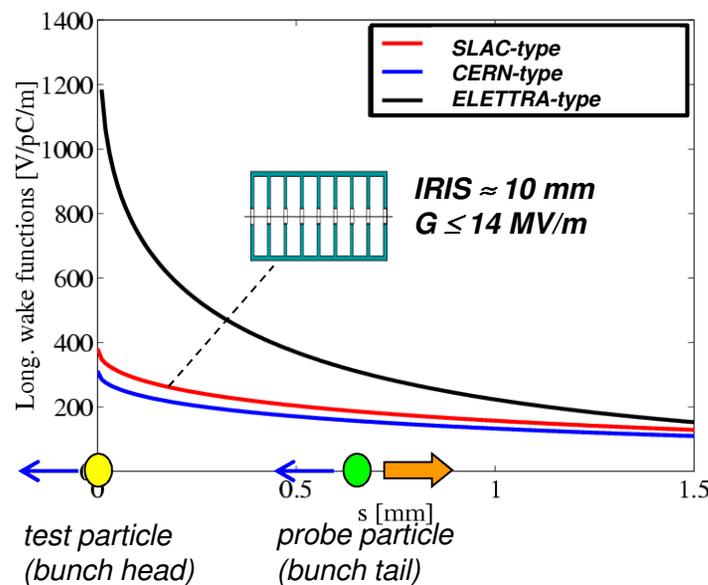
Short-Range Wakefield

Ignore transient regimes of GTW and assume a cylindrically symmetric, periodic accelerating structure. Then, the following model applies for most of the practical cases (especially for short bunches) if $a^2/2L \ll \sigma_z \ll s_1$:

$$w_T(z) = A \left[1 - \left(1 + \sqrt{\frac{z}{s_1}} \right) e^{-\sqrt{\frac{z}{s_1}}} \right] \left[\frac{V}{C \cdot m^2} \right], \quad \text{where } A \approx \frac{Z_0 C s_1}{\pi a^4} \approx 10^3 \div 10^5 \frac{V}{pC \cdot m^2}$$

and $s_1 \approx 0.3 \div 0.8 \text{ mm}$ is a cell geometric parameter. w_T is the wakefield per unit length of the cavity, per unit length of (relative) lateral displacement.

N.B.: w_L is stronger for shorter bunches, w_T is stronger for longer ones.



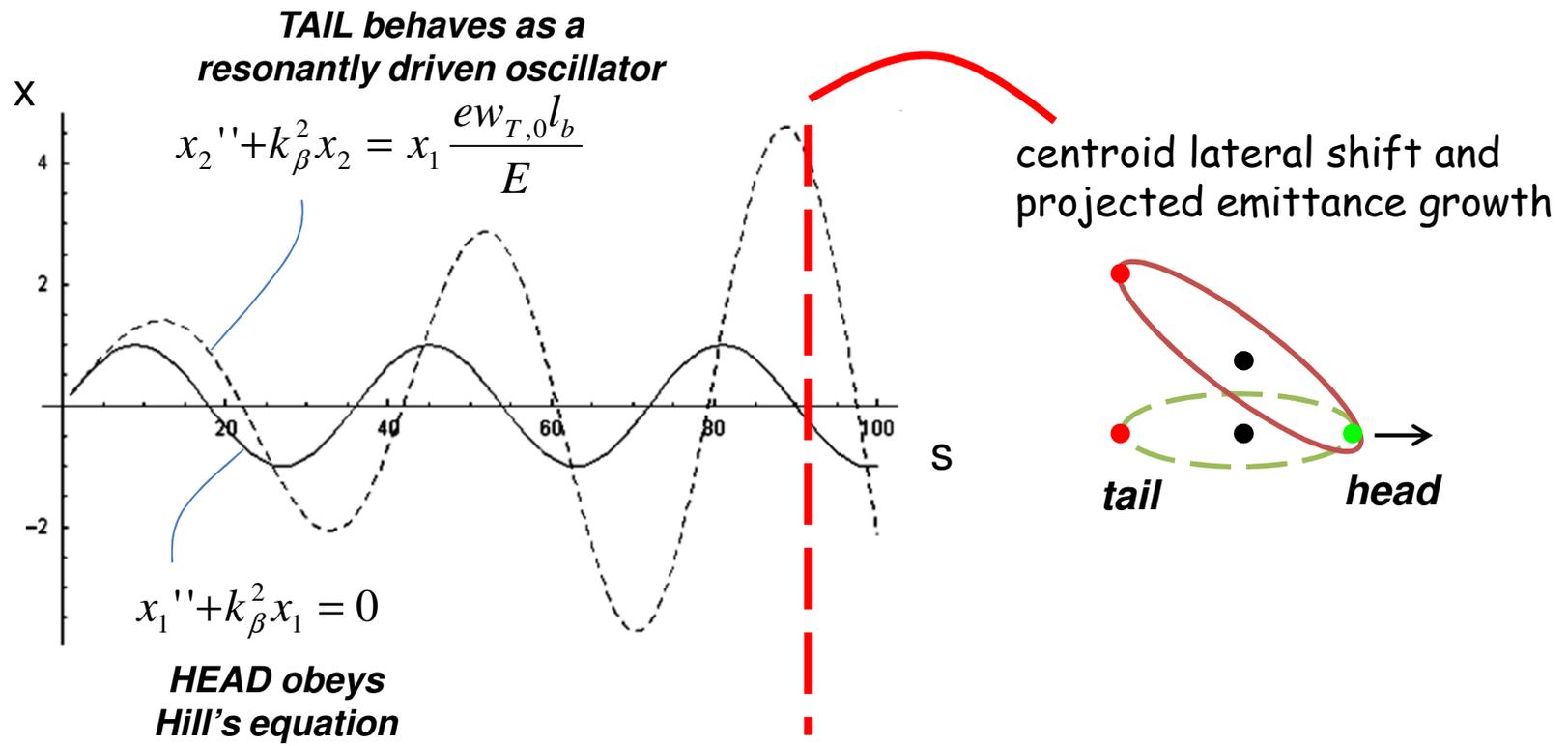
Single-Bunch Beam Break-Up

Pictures courtesy of
A. Chao

Equation of motion for $x(z,s)$ in the presence of w_T (exact):

$$\frac{d}{ds} \left[\underbrace{\gamma(s)}_{\text{acceleration}} \frac{d}{ds} x(z,s) \right] + \underbrace{k_\beta^2}_{\beta\text{-focusing}} \gamma(s) x(z,s) = r_e \int_z^\infty \underbrace{dz' \rho(z')}_{\text{charge distribution}} \underbrace{w_T(z'-z)}_{\text{wake function}} \underbrace{[x(z',s) - d_c(s)]}_{\text{cavity displacement relative to the particle free } \beta\text{-oscillation}}$$

In a 2-particle model at fixed energy, the bunch head drives resonantly the tail:



Coupling Strength

- The analytical solution can be found iteratively (perturbative theory). At the lowest order, it is the product of the unperturbed x_β times the wake driving term. For an **off-axis injection** into a **perfectly aligned linac**, constant accelerating gradient and focusing $\mathbf{k}(s)=\mathbf{k}_\beta$, we have:

$$x^1(z, s) = \sqrt{2J\beta} \left[\frac{1}{q} \cos(k_\beta s) + \left(\frac{\ln q}{\sqrt{q}(q-1)} \right) s \sin(k_\beta s) \cdot \left(\frac{r_e}{4\gamma_0 k_\beta} \right) \int_z^\infty dz' \rho(z') w_T(z'-z) \right], \quad q := \frac{\gamma_f}{\gamma_0}$$

unperturbed β -oscillation
additional out-of-phase oscillation, which grows monotonically with s
the integral goes like $\sim Nw_T(l_b)/l_b$

- From r.h.s. we extract a coefficient that measures the **coupling strength** of the wake to the bunch:

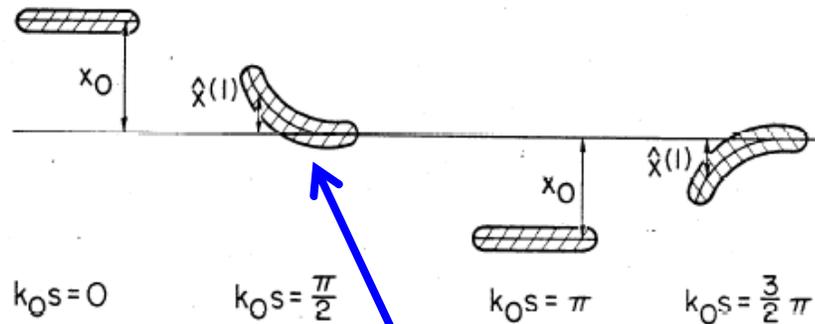
$$\varepsilon_r = \frac{4\pi\varepsilon_0 w_{T,0} I_b L^2}{I_A \gamma_0}$$

- The higher the value of ε_r ($\gg 1$) is, the more important the higher order terms (in s) are for the particle motion. Additional oscillation terms grow with **powers of s** .

EXERCISE: ε_r is given for a linac 200 m long. What is the bunch current that would imply the same coupling strength for a 50 times longer linac?

“Banana Shape”

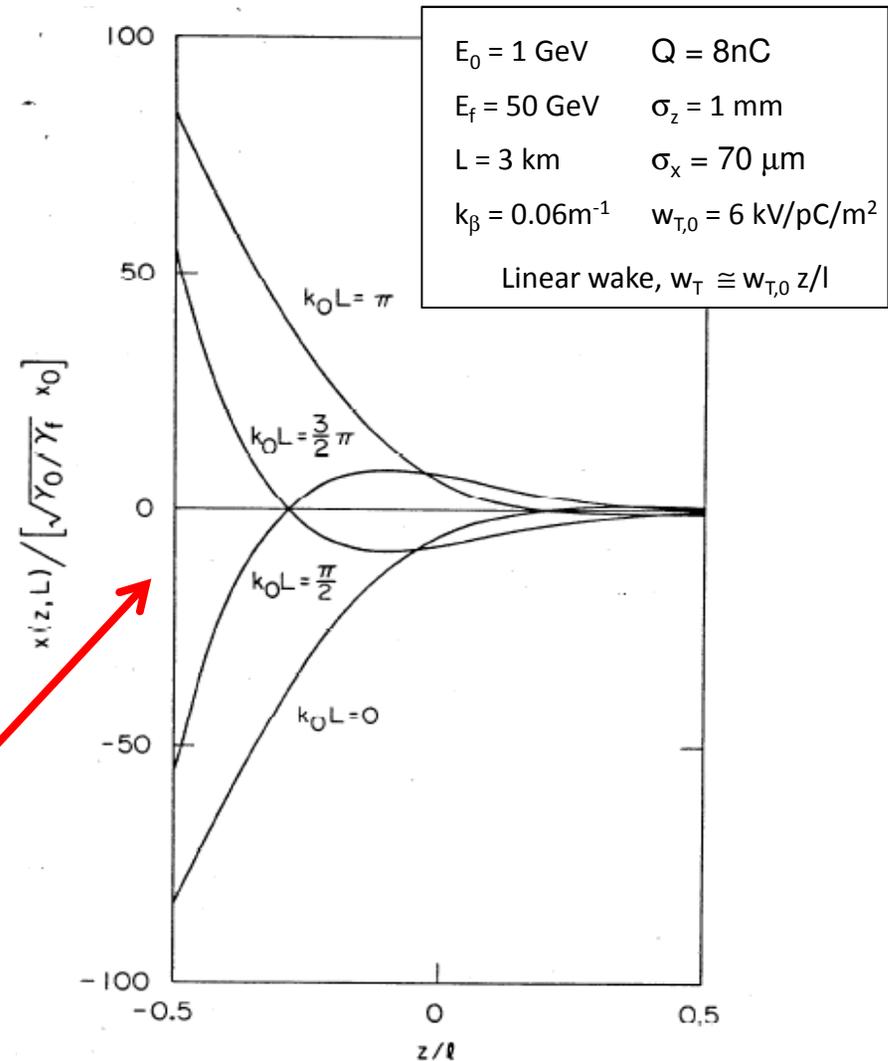
- Bunch shape for weak instability ($\epsilon_r \approx 1$), at four betatron phase advances $\Delta\mu = k_0 s$:



Different bunch slices feel different wake kicks, which displace them in the transverse phase space, one respect to the other.

As a result, the projected emittance grows and “oscillates” along the linac according to the wake strength and the betatron phase advance.

- “Banana shape” in the SLAC linac for strong instability ($\epsilon_r \gg 1$):



Emittance Growth, Analysis

In real facilities, beam-to-linac misalignment is the result of different and simultaneous error sources. Sometimes, some of them dominate over the others.

- **Quadrupoles misalignment:** beam is kicked off-axis. Assume 1-to-1 trajectory correction at all BPMs, located close to focusing and de-focusing quadrupoles,

$$\Delta(\gamma\mathcal{E}) \approx \sigma_{y,BPM}^2 [\pi\epsilon_0 r_e NW_{\perp} (2\sigma_z)]^2 \frac{L_{cell}^2}{16\alpha(\Delta\gamma_{str}/L_{str})} \left[\left(\frac{\gamma_f}{\gamma_i} \right)^{2\alpha} - 1 \right] \frac{\cos(\Delta\mu_{cell}/2)}{\sin^3(\Delta\mu_{cell}/2)}$$

$$L_{cell}(s) \propto \gamma^{\alpha}(s)$$

**under auto-phasing, see next slides.*

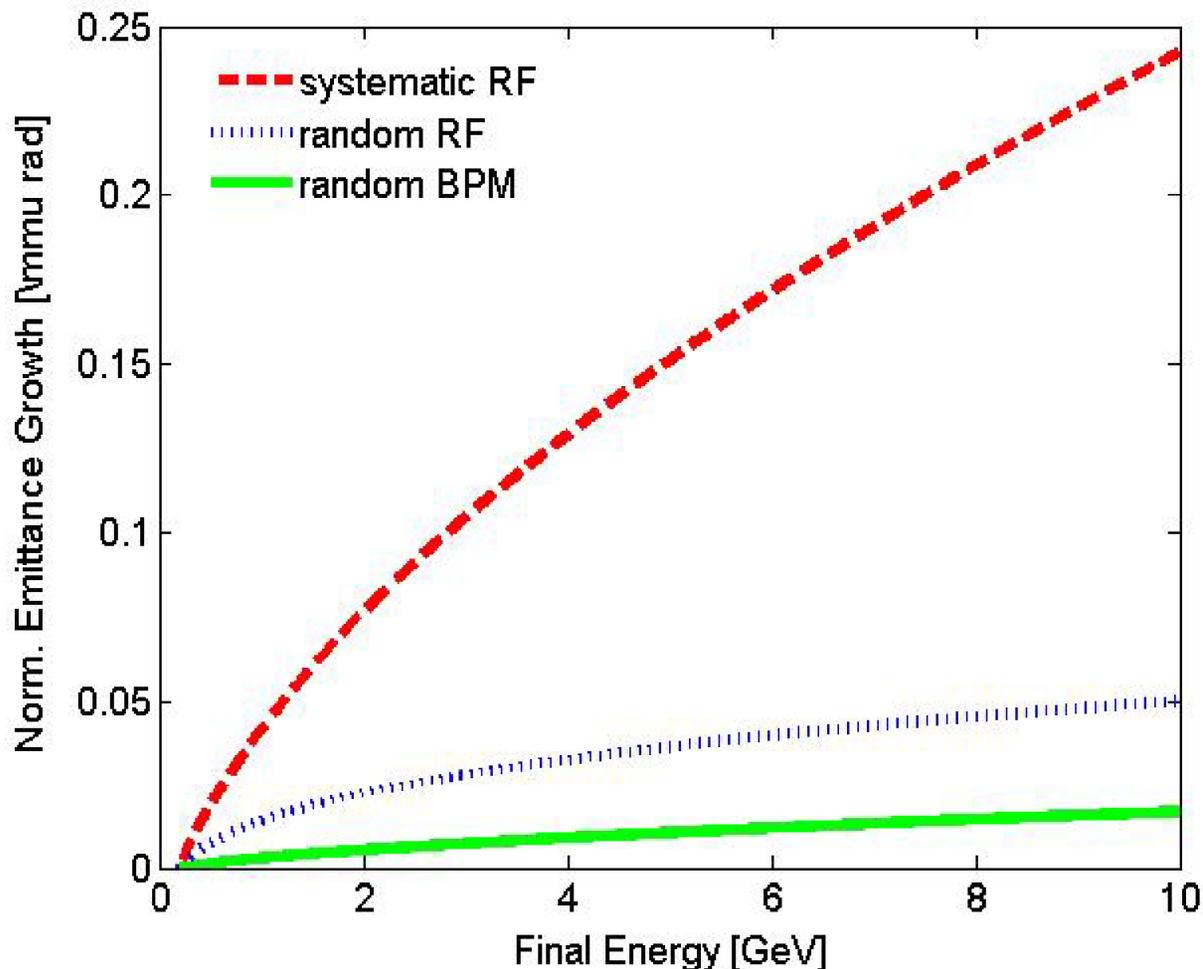
- **Linac random misalignment:** beam centered in the quads, but off-axis in the structures,

$$\Delta(\gamma\mathcal{E}) \approx \sigma_{str}^2 [\pi\epsilon_0 r_e NW_{\perp} (2\sigma_z)]^2 \frac{L_{str} \bar{\beta}}{2\alpha(\Delta\gamma_{str}/L_{str})} \left[\left(\frac{\gamma_f}{\gamma_i} \right)^{\alpha} - 1 \right]$$

- Systematic misalignment of **2 consecutive structures:** slightly stronger effect because more structures are contributing with same sign of the kick,

$$\Delta(\gamma\mathcal{E}) \approx \sigma_{str}^2 [\pi\epsilon_0 r_e NW_{\perp} (2\sigma_z)]^2 \frac{L_{cell} \bar{\beta}}{4\alpha(\Delta\gamma_{str}/L_{str})} \left[\left(\frac{\gamma_f}{\gamma_i} \right)^{2\alpha} - 1 \right]$$

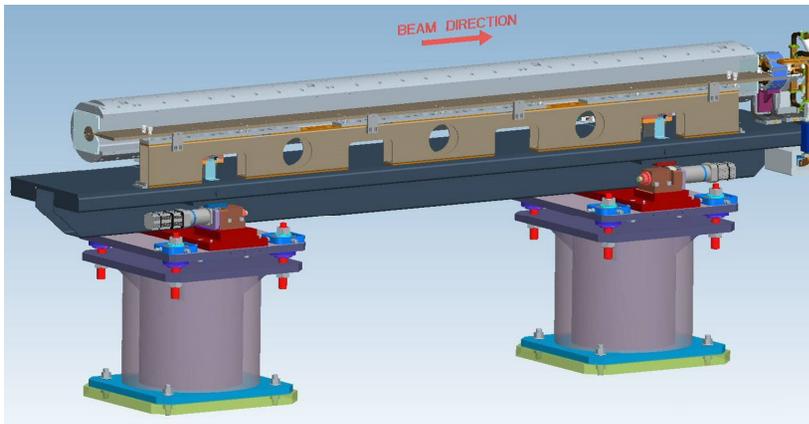
Emittance Growth, Comparison



$Q=300\text{pC}$, $\sigma_z=120\mu\text{m}$, $I=1\text{kA}$, $L_{\text{str}}=3.5\text{m}$, $L_{\text{cell}}=8\text{m}$, $\Delta\mu_{\text{cell}}=45^\circ$, $\langle\beta\rangle=30\text{m}$,
 $E_0=200\text{MeV}$, $G_{\text{acc}}=15\text{MV/m}$, $W_{0,\perp}=10^{16}\text{V/C/m}^2$, $\Delta_{\text{str}}=200\mu\text{m}$, $\Delta_{\text{bpm}}=50\mu\text{m}$, $\alpha=0.3$.

Linac Alignment and Layout

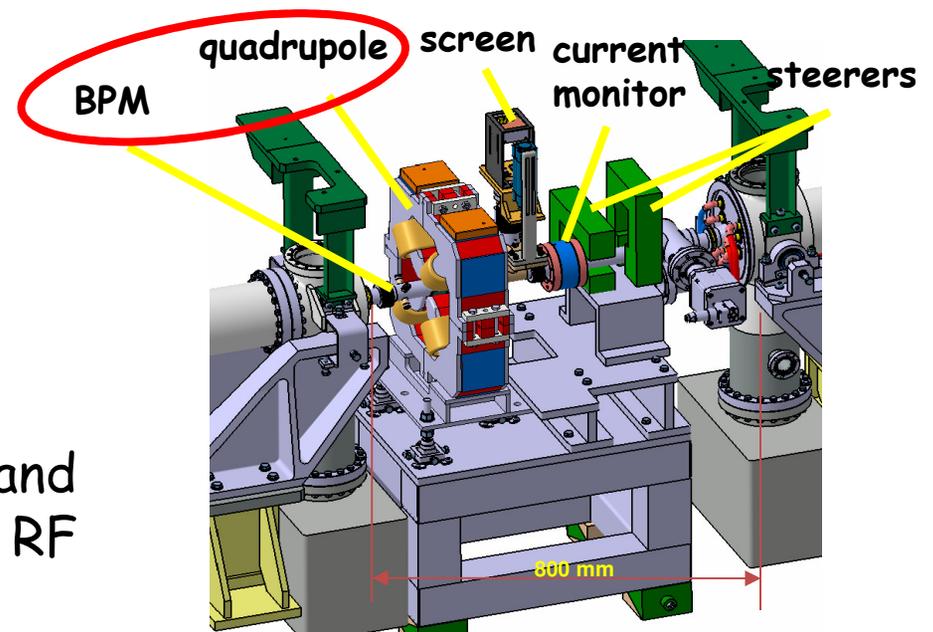
Previous slide points out the importance of the *static* alignment of the main linac components. Some technical solutions may help for reducing the initial wake effect and allow an accurate trajectory control.



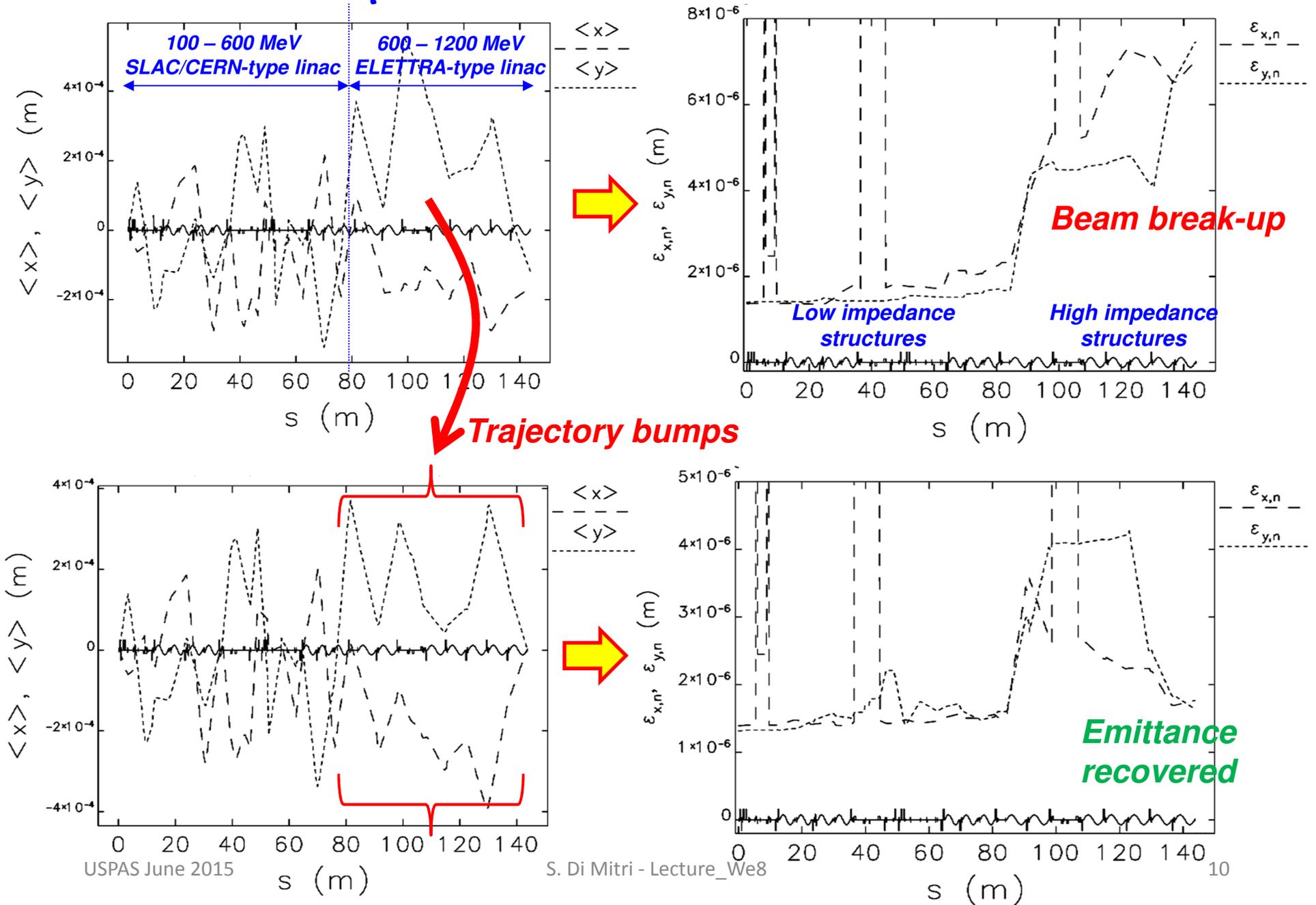
1. Use fixed, stable support (especially for RF structures) and girder with 3-D movers on the top of it.

2. *Fiducialize* magnets, RF structures and BPMs (both for piezo and laser tracker)

3. Insert BPM inside the Quad, and one Quad (possibly) after every RF structure.



«Emittance Bumps»



Trajectory Jitter

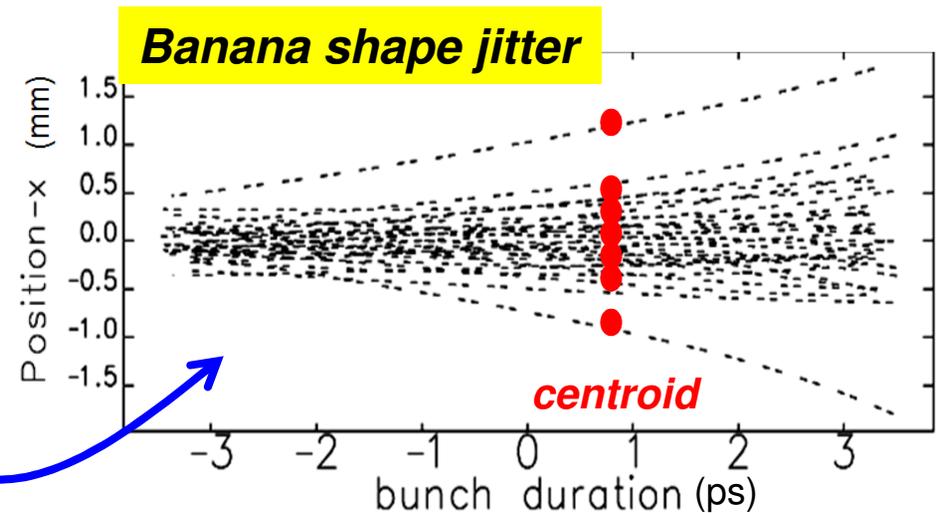
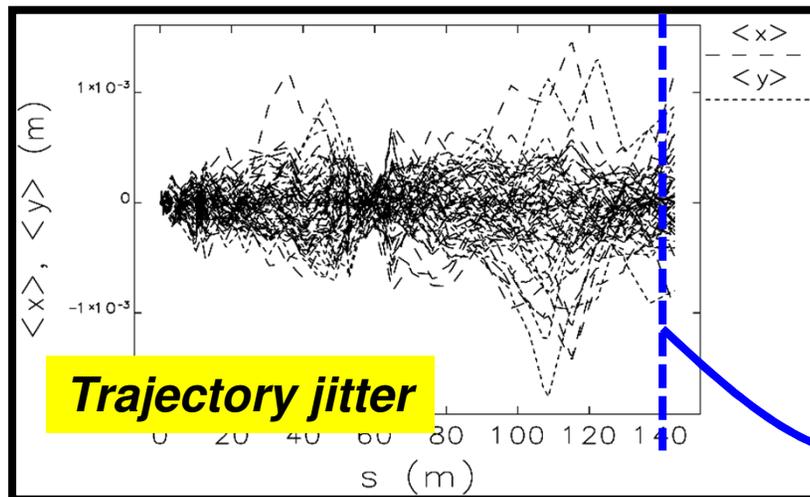
Emittance bumps rely on the trajectory manipulation in a certain linac region. If the beam optics or trajectory changes, the wake suppression is expected to start failing. So, how much is this *scheme sensitive to trajectory jitter*?

□ Common short-term sources (say, $f \leq 10\text{Hz}$):

- beam launching (injector jitters),
- mean energy (RF jitter),
- magnets' power supply, vibrations (e.g., due to magnet water cooling).

□ Different trajectories imply (all along the linac and at its end):

- different banana shape,
- different bunch centroid position.



Tolerance Jitter Budget

- Now consider both centroid's position $\langle x \rangle$ and angular divergence $\langle x' \rangle \Rightarrow$ built the bunch **centroid Courant-Snyder invariant**.
- We can specify the tolerance jitter budget by imposing, e.g., that the **centroid invariant varies less than 10% of the (unperturbed) beam emittance**:

$$A_{T,x} = \sqrt{\frac{x_{CM}^2 + (\alpha_x x_{CM} + \beta_x x'_{CM})^2}{\epsilon_x \beta_x}} \leq 0.1$$

- The uncorrelated sum of error kicks ($j=1, \dots, M_n$, for n different jitter sources) must be less than 10%:

$$A_{T,x}^2 \cong \sum_1^M x_{CM,i}^2 \frac{\beta_x}{\epsilon_x} \cong 0.1^2 \left[\sum_1^{M_1} \left(\frac{\sigma_{t,1}}{\sigma_{s,j}} \right)^2 + \dots \sum_1^{M_n} \left(\frac{\sigma_{t,n}}{\sigma_{s,j}} \right)^2 \right] \leq 0.1^2$$

sum of normalized error kicks

ratio of "tolerance" over "sensitivity"

Sensitivity $\sigma_{s,j}$:= trajectory amplitude variation over jitter amplitude variation.

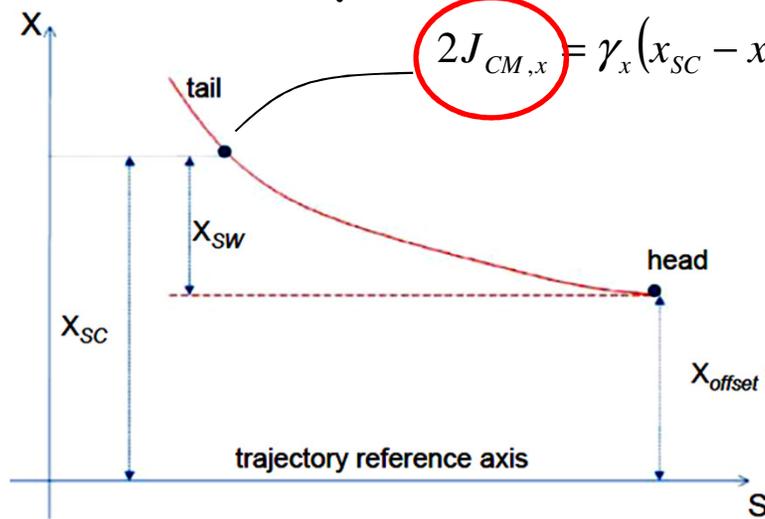
Tolerance $\sigma_{t,n}$:= maximum admitted over all sensitivity amplitudes (per source).

N.B.1: Sensitivities can be computed with tracking including *machine errors*.

N.B.2: Tolerances are «arbitrary» *weights* for different jitter sources and, to be physical, have to fit technological limits.

Slice Centroid Courant-Snyder Invariant

- We additionally require that the position of **each slice centroid varies less than one unperturbed RMS beam size**:



$$2J_{CM,x} = \gamma_x (x_{SC} - x_{offset})^2 + 2\alpha_x (x_{SC} - x_{offset})(x'_{SC} - x'_{offset}) + \beta_x (x'_{SC} - x'_{offset})^2 \equiv \epsilon_{SW,x}$$

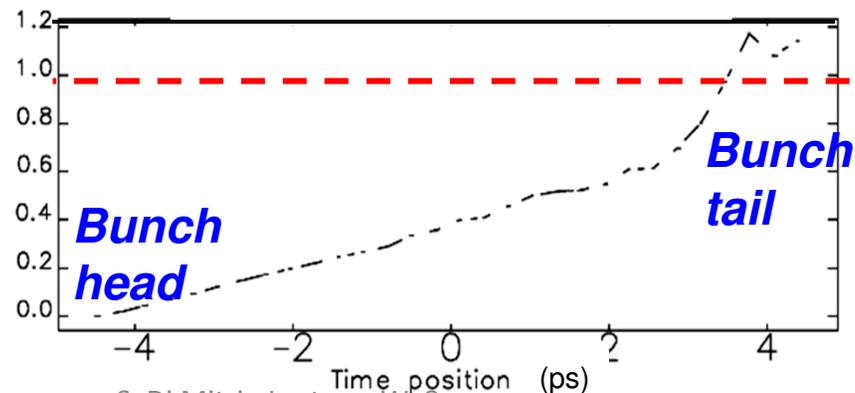
$$\frac{\sigma_{x,SC}}{\sqrt{\epsilon_x \beta_x}} \leq 1, \text{ where:}$$

$$\begin{aligned} \sigma_{x,SC} &= \sqrt{\langle x_{SC}^2 - \bar{x}_{SC}^2 \rangle} \simeq \sqrt{\frac{1}{N} \sum_{i=1}^N (x_{SW}^i - \bar{x}_{SW})^2} = \\ &= \sqrt{\frac{1}{N} \sum_{i=1}^N \left[\sqrt{\beta_x \epsilon_{SW,x}^i} \cos \phi_x - \frac{1}{N} \sum_{i=1}^N \sqrt{\beta_x \epsilon_{SW,x}^i} \cos \phi_x \right]^2} = \\ &= \sqrt{\beta_x} \cos \phi_x \sqrt{\frac{1}{N} \sum_{i=1}^N \left[\sqrt{\epsilon_{SW,x}^i} - \frac{1}{N} \sum_{i=1}^N \sqrt{\epsilon_{SW,x}^i} \right]^2} \end{aligned}$$

- Assume same optics for all slices \Rightarrow the RMS variation of the *i*-th slice centroid invariant, computed over many shots (trajectories), must be less than the RMS unperturbed emittance, computed over all beam particles.

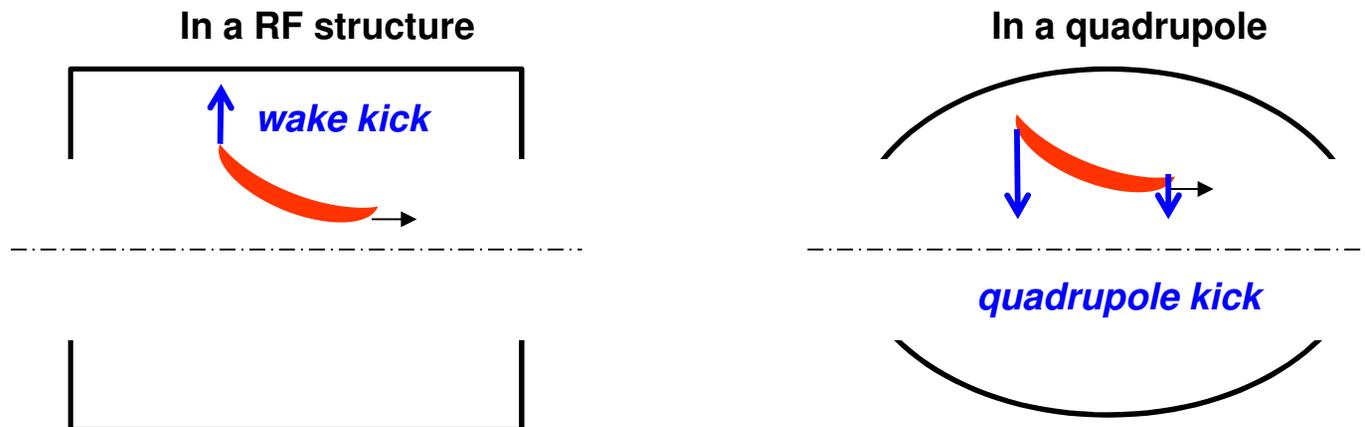
$$\frac{RMS(2J_{CM,x})}{\sqrt{\epsilon_x}} \leq 1$$

for each slice



Balakin–Novokhatsky–Smirnov Damping

1. GTW deflects the trailing particles of a bunch with positive offset in the positive direction. The idea is to focus back those particles with a negative kick, that is the **bunch tail** must be **over-focused relative to the head**.
2. In fact, by imposing a lower energy in the bunch tail than in the head, the trailing particles feel a stronger quadrupole focusing that tends to realign the bunch slices in the phase space.



3. Imagine two macroparticles with different β -frequencies (i.e., $k_{\beta,1}$ and $k_{\beta,2}$). The trajectory difference between the two particles is:

$$x_2 - x_1 \cong \hat{x} \left(1 - \frac{e^2 w_T(l_b)}{E} \frac{1}{k_{\beta,2}^2 - k_{\beta,1}^2} \right) (\cos k_{\beta,2} s - \cos k_{\beta,1} s)$$

Energy Spread and “Auto-phasing” Condition

4. The wake effect can be locally cancelled if (i.e., cancelled at all points in the linac downstream of the location where) the **“auto-phasing” condition** holds:

$$\frac{e^2 w_T(l_b)}{E} \frac{1}{k_{\beta,2}^2 - k_{\beta,1}^2} = 1$$

5. It can be achieved by introducing an **energy difference** between the head and the tail of the bunch. When discrete focusing such as FODO lattice is considered, the **auto-phasing RMS energy spread** is:

$$\sigma_{\delta, BNS} \approx \frac{Ne^2 w_T (2\sigma_z) \bar{\beta} L_{cell}}{E \tan(\Delta\mu_{cell} / 2)}$$

The BNS energy spread scales as $\sim \gamma^{2\alpha-1}$ along the linac, where $\beta \sim \gamma^\alpha$.

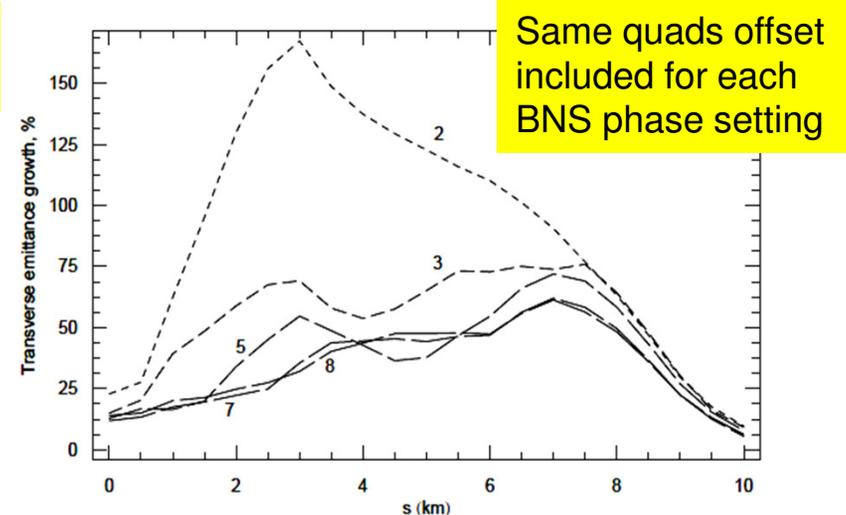
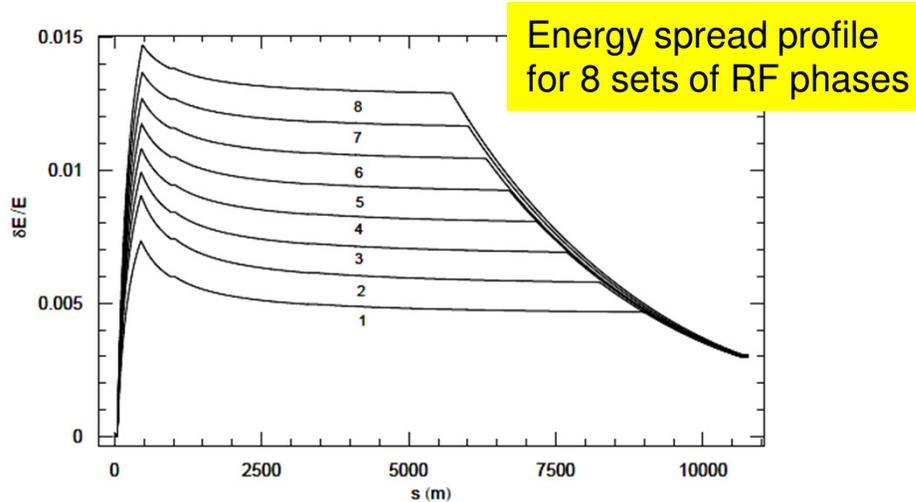
6. As a result of randomly misaligned accelerating structures (perfect FODO focusing along M-cells, with $\beta \sim \gamma^\alpha$) and *in the absence of any wake suppression scheme*, the final **projected emittance growth** due to transverse wake field instability is:

$$\Delta\mathcal{E} \approx \left(\frac{\pi r_e}{Z_0 c e} \right)^2 (Ne)^2 (w_T (2\sigma_z))^2 \Delta^2 L_{cell}^2 M \bar{\beta} \frac{(q^\alpha - 1)}{\alpha}$$

Linac Energy Budget

Pictures courtesy of
G. Stupakov

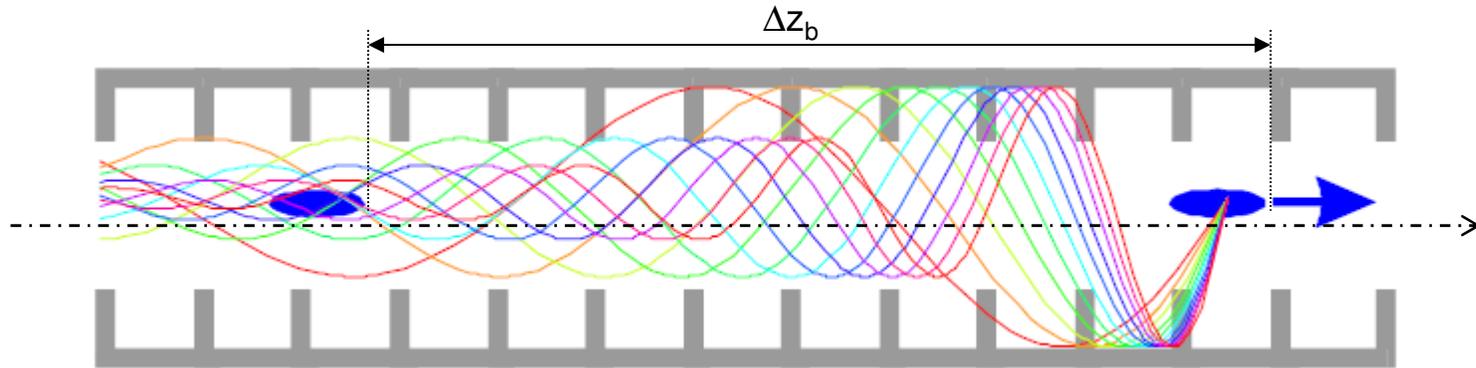
7. The BNS autophasing condition implies an optimization of the linac RF phasing, for any given quadrupole setting, in order to: i) reduce the **energy overhead** that is needed to impose the correlated energy spread, and ii) minimize the **final energy spread** at the undulator entrance.



- Typically, initial RF structures are run off-crest (+) to generate $\sigma_{\delta, \text{BNS}}$, while ending structures are run off-crest (-) to remove the residual energy spread. However, the BNS damping goes in conflict with emittance growth due to **spurious dispersion**, generated by misaligned quadrupoles.
- δ_{BNS} has opposite sign respect to δ required for magnetic compression. In practice, BNS damping has been mostly investigated for long, 10's of GeV linear colliders (e.g., NLC). Emittance bumps are routinely adopted in existing few GeV's linac-driven FELs.

Long-Range Wakefield

The long-range (transverse) wakefield is the extension of the short-range to multi-bunch patterns. Now, leading and trailing particles in the same bunch are substituted with leading and trailing **bunches** in the same **bunch train**.



For long-range wakes, tend to consider **field modes** rather than wake potential: this is the sum over several high order modes (HOMs) which are **excited by the first bunches of a train**, and **act on the subsequent ones**:

$$w_T(z) = \sum_k \frac{r_{s,k} \omega_k}{Q_k} e^{-\frac{\omega_k z}{2cQ_k}} \sin \frac{\omega_k z}{c} \left[\frac{V}{Cm^2} \right]$$

The trailing bunches are driven even more off axis leading to an even stronger excitation of the modes in the next accelerating section (**instability**).

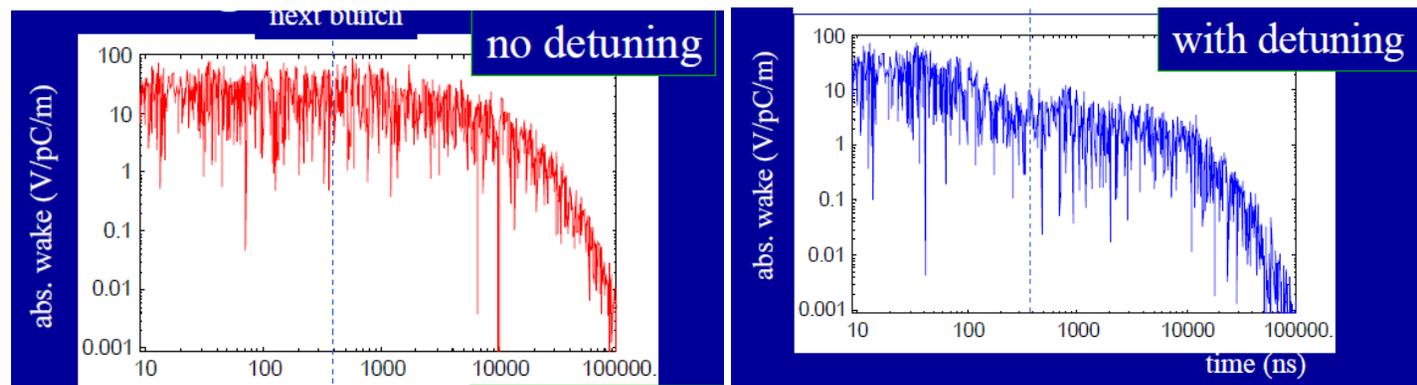
The **bunch offsets grow exponentially** according to: $\Delta x_f \propto e^{\sqrt{Q_{wT}}}$

Multi-Bunch Beam Break-Up

If the wake is negligible beyond more than one bunch spacing (*daisy chain model*), then the criterion for little or no emittance blow-up is, as in the single-bunch case, $\varepsilon_r < 1$, and the wake function is now evaluated over the single bunch length.

The **multi-bunch instability** can be **suppressed** with a **special design of the structures**.

- **Detuned structures** have slightly different cell-to-cell dimensions to introduce a frequency spread of each mode, causing decoherence of the wake function. This is already present, albeit in principle not optimized, in constant-gradient structures.

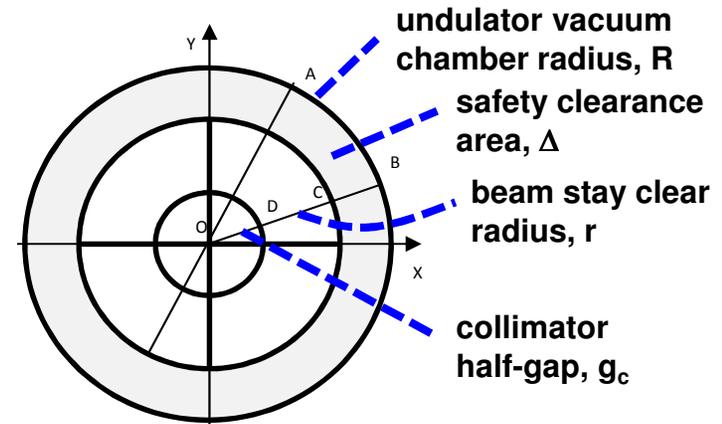
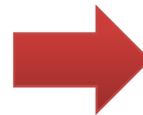
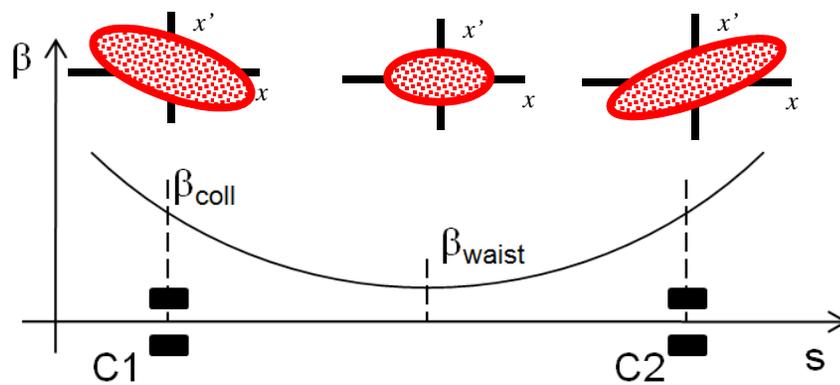


- For X-band linear colliders, very **low Q (~20) choke mode structures** have been designed, which suppress all the deflecting modes.
- In SC linacs, **HOM loop couplers** have been designed to couple out lower frequency modes (below a few GHz) and bring them to room temperature loads for absorption.

Geometric Collimation

Collimators are high-Z, metallic blocks with **apertures** to intercept, scatter and absorb undesired particles at large β -amplitudes ($|A| \geq 20\sigma$) or off-energy ($|\delta| \geq 2\%$). They **protect** the **undulator** from being hit by e.m. showers generated by primary (halo) or secondary particles (from vacuum chamber). The *beam core should pass through untouched*.

To stop halo particles both in position and angular divergence, at least two geometric collimators are needed and ideally separated by $\Delta\mu = \pi/2$.



In the linac: low- β insertion for 2-stage geometric collimation

❑ The optimum **collimator acceptance** and **half-gap** are:

$$a_{\pi/2} = \frac{(R - \Delta)^2}{2\hat{\beta}_{und}} \Rightarrow g_{\pi/2} = \sqrt{a_{\pi/2}\beta_{coll}}$$

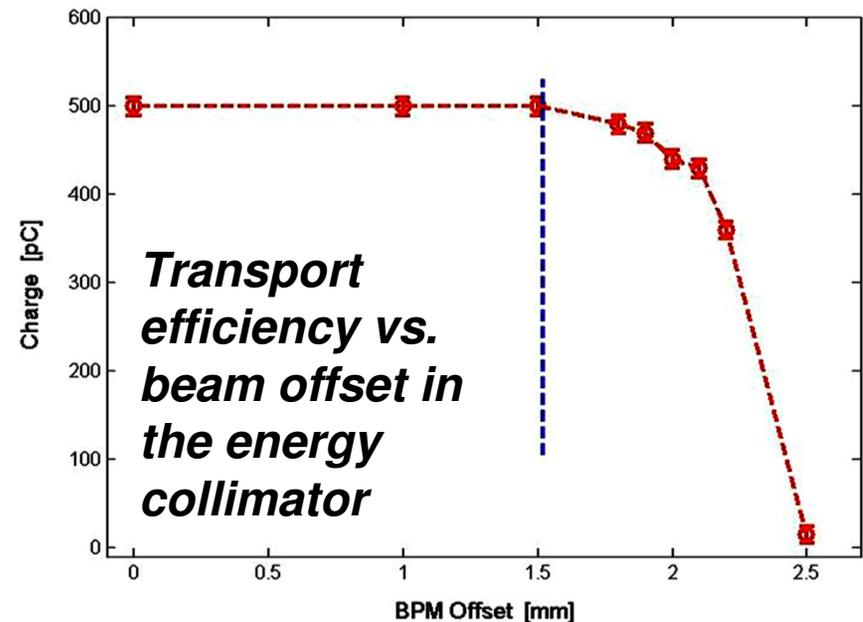
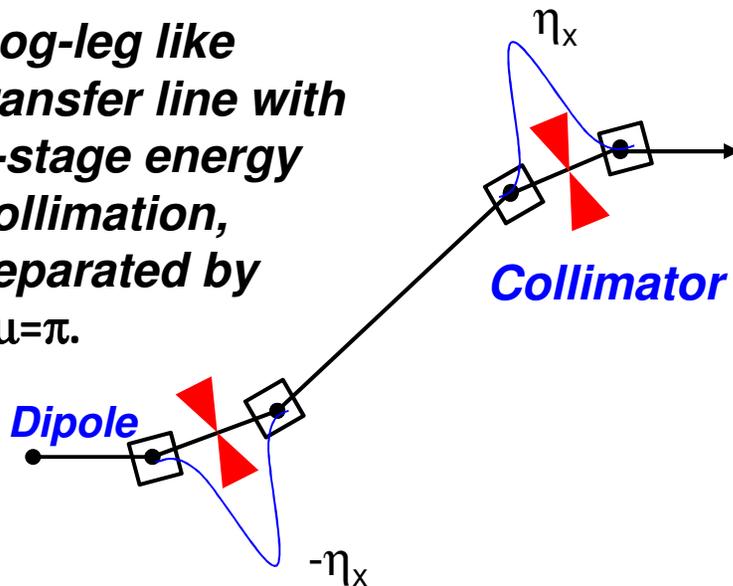
❑ Small gap means high collimation efficiency but also excites strong geometric wakefields. **Optics** tuning is required for a compromise.

Energy Collimation

To stop particles with both positive and negative energy deviation respect to the reference energy, at least two collimators placed in a dispersive region are needed, ideally separated by $\Delta\mu = \pi$.

The energy acceptance is $\frac{\Delta E}{E} = \frac{g_c}{\eta_x}$, so that one aims to have **small collimator's gap** and **large momentum dispersion**. If the particle motion is dominated by dispersion, i.e. $\frac{\eta_x \sigma_\delta}{\sqrt{\epsilon_x \beta_x}} \gg 1$, and if the the energy collimators are at $\Delta\mu = \pi$, then we will intercept all particles having $|\delta| \geq \frac{g_c}{|\eta_x|}$

Dog-leg like transfer line with 2-stage energy collimation, separated by $\Delta\mu = \pi$.



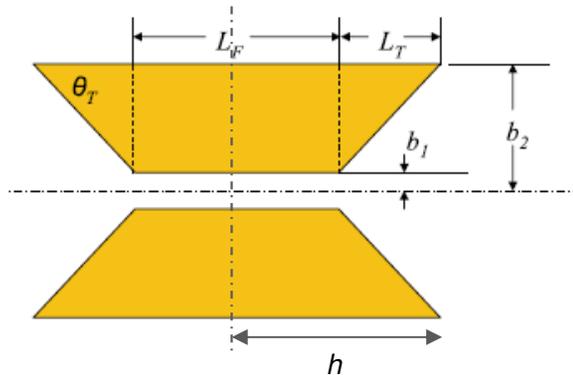
Geometric Transverse Wakefield in Collimators

An ultra-relativistic beam passing off-axis by $\Delta y_0 \ll b_1$ through a collimator with geometric symmetry in the plane of interest (see figure) receives a kick:

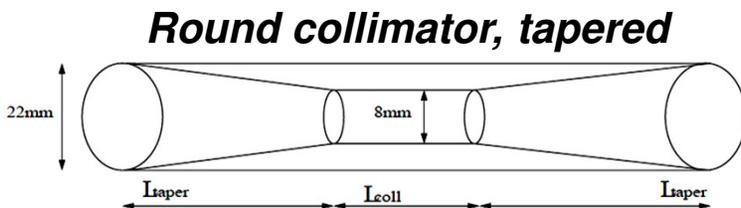
$$y' = \frac{\Delta y_0 Q}{E} \kappa$$

where κ is the “**transverse kick factor**” in $V/pC/mm$, namely the transverse kick averaged over the bunch length.

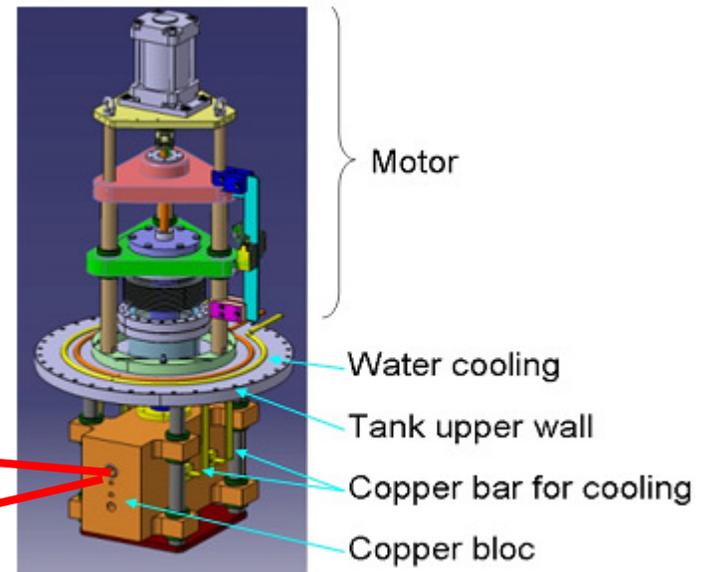
Analytical formulas for κ can be found whereas $\alpha \equiv \theta_T b_1 / \sigma_z$ is either small or large respect to 1, regimes which we are denoted as **inductive** and **diffractive**, respectively. For $\alpha \approx 1$, the analysis can only provide the orders of magnitude.



Flat collimator, tapered



Round collimator, tapered



Transverse Kick Factor

INDUCTIVE regime ($\alpha \ll 1, \theta_T \ll 1$)

$$\kappa = \frac{Z_0 c \alpha}{2\pi^{3/2} b_1^2} \left(1 - \frac{b_1}{b_2}\right) \quad \text{Gaussian bunch in round, tapered collimator}$$

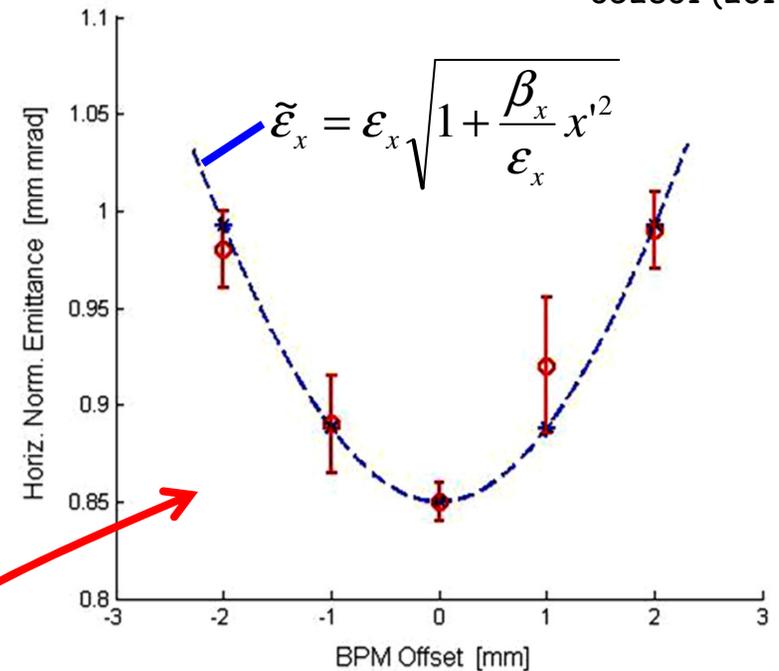
$$\kappa \approx \frac{Z_0 c \alpha h}{4\pi^{1/2} b_1^3} \quad \text{Gaussian bunch in flat, tapered collimator}$$

DIFFRACTIVE regime ($\alpha \gg 1$)

$$\kappa \approx \frac{Z_0 c}{2\pi} \left(\frac{1}{b_1^2} - \frac{1}{b_2^2}\right) \quad \text{Long } (L_F \rightarrow \infty) \text{ collimator}$$

$$\kappa = \frac{Z_0 c}{4\pi} \left(\frac{1}{b_1^2} - \frac{b_1^2}{b_2^4}\right) \quad \text{Short } (L_F \rightarrow 0), \text{ round collimator}$$

$$\kappa \approx \frac{Z_0 c}{4\pi b_1^2} \quad \text{Short } (L_F \rightarrow 0), \text{ flat collimator}$$

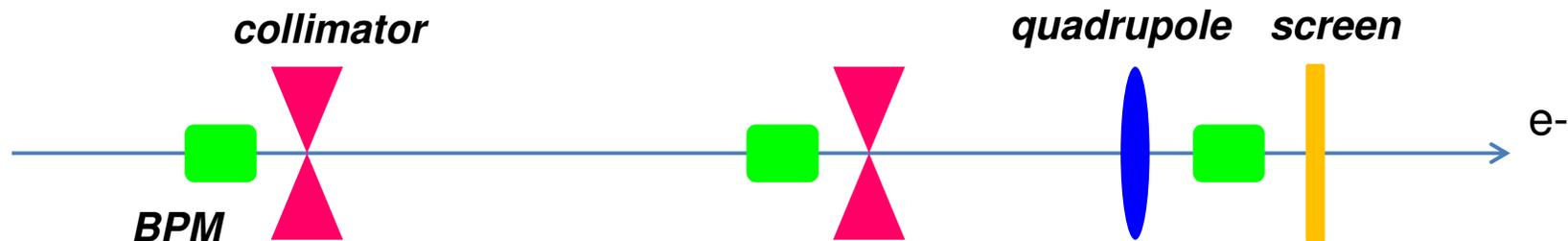


- Beam final normalized emittance vs. horizontal offset in the collimator.
- The geometric collimator is set to $g=2\text{mm}$. The quadratic term of the fitting corresponds to $k_{\text{fit}} = 2.20 \text{ V/pC/mm}$.
- The dashed curve shows Eq.2 evaluated for $k = k_{\text{fit}}$.

Collimation Insertion

- Collimation of high brightness beams ($I > 300 \text{ A}$, $\gamma \epsilon \sim 1 \mu\text{m}$) with $g \sim 1 \text{ mm}$, requires **trajectory control** with accuracy at $\sim 10 \mu\text{m}$ level, in order to avoid emittance degradation above $\sim 10\%$. This is normally feasible in modern linacs with standard BPMs.
- The **transverse kick factor** can be measured in (at least) two ways:
 1. looking to the emittance growth vs. beam offset in the collimator,
 2. looking to the downstream beam position vs. the beam offset in the collimator.

The analytical approximations work well for simple collimator geometries.



- N.B.: the **longitudinal kick factor** can usually be neglected because:
 - it is well absorbed by the longitudinal emittance which is usually ~ 100 times larger than the transverse one;
 - wakefield induced energy spread is dominated by the stronger wake potential due to the much longer linac structures.