

# Lecture 7 Thermal Insulation & Cryostat Basics

J. G. Weisend II



#### Goals



- Introduce conduction, convection & radiation heat transfer as they apply to cryogenics
- Describe design techniques to reduce heat transfer into cryogenic devices
- Allow the estimating and scaling of heat leaks into cryogenic devices
- Discuss the basics of cryostat design
- Warning! Not a full description of heat transfer
  - Many topics (boiling, detailed convection calculations, complicated geometries in radiation heat transfer etc) won't be covered
  - Should, however, be a good example of how heat transfer theory can be applied to practical problems.



### **Three Ways to Transfer Heat**



- Conduction
  - Heat transfer through solid material
- Convection
  - Heat transfer via a moving fluid
    - » Natural or free convection motion caused by gravity (i.e. density changes)
    - » Forced motion caused by external force such as a pump
- Radiation
  - Heat transferred by electromagnetic radiation/photons
- There is no such thing as a perfect insulator though we can design systems with very small heat leaks
- All matter above 0 K radiate heat
  - $\bullet$  Remember we can't get to 0 K  $3^{\text{rd}}$  Law of Thermodynamics though we can get vanishingly close
- Heat flows from high temperature to low
  - Heat leaks in, cold doesn't leak out



# **Conduction Heat Transfer**



Fundamental Equation – The Fourier Law in one dimension

$$Q = -K(T)A(x)\frac{\partial T}{\partial x}$$

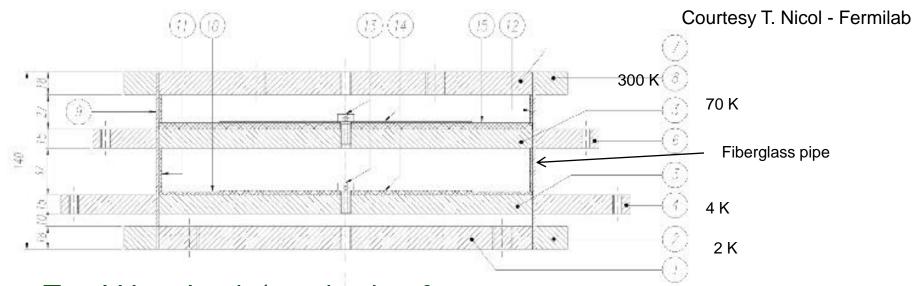
• If we assume constant cross section we get:  $Q = -A/L \int_{T}^{T_H} K(T) dT$ 

- Reduce conduction heat leak by:
  - Low conductivity material: make K(T) small
  - Reduce cross sectional area: make A small
  - Increase length: make L large
  - For a given T<sub>C</sub> make T<sub>H</sub> smaller: i.e. use intermediate temperature heat intercepts
    - » You still have heat leak from 300 K to this intermediate temperature but <u>remember</u> <u>Carnot</u>, It's more thermodynamically efficient to remove heat at higher temperatures

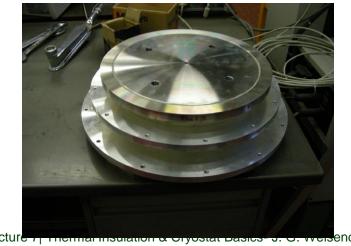


# **Design Example ILC Cryomodule Support Post**





- Total Heat Leak (conduction & radiation)
  - 70 K 10.5 W
  - 5 K 0.9 W
  - 2 K 0.03 W
- Can support up to 50 kN





### **Conduction Heat Transfer**



 Conduction heat leaks may be estimated by the use of Thermal Conductivity Integrals (Lecture 4)

$$Q = -G(\theta_1 - \theta_2)$$



### **Convection Heat Transfer**



Fundamental Equation: Newton's law of cooling

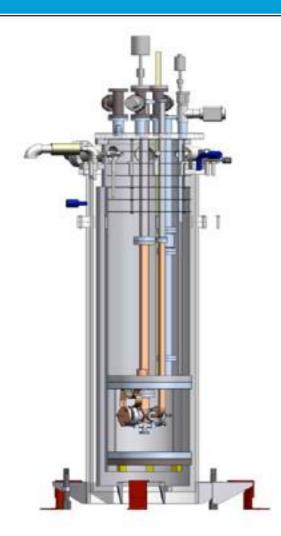
$$Q = hA(T_{surface} - T_{fluid})$$

- where h is the heat transfer coefficient and is a function of Re, Pr, geometry etc depending on the situation
- In cryogenics we eliminate convection heat leak in cryogenic systems by "simply" eliminating the fluid – vacuum insulation
- Using vacuum insulation to create vessels capable of storing cryogenic liquids was first done by James Dewar – who liquefied hydrogen
  - Such vessels are frequently called dewars though not always, more later
  - Thermos bottles are a simple example of this approach



# Design Example Vacuum Insulated Test Cryostat





- Contains 3 Vacuum Spaces
  - 1 between 300 K wall and LN<sub>2</sub> bath
  - 1 between LN<sub>2</sub> bath and LHe bath
  - 1 between LHe bath and experiment



### **Vacuum Insulation**



- How much vacuum is enough?
  - This of course depends on the heat leak requirements but generally we want to be below 10<sup>-5</sup> torr If we maintain this level or better we can generally neglect the convection heat leak for most applications.
    - » Cryogenic Engineering, Flynn (1997) has a good discussion of calculating heat leak due to residual gas pressure

#### Cryopumping

- At cryogenic temperatures almost all common gases condense and freeze onto the cold surface. Typically, we'll see that once surface are cooled to ~ 77 K the isolation vacuum will drop to the 10-8 torr or better range if the system is leak tight and doesn't have significant outgassing
- But don't just start cooling with everything at room pressure
  - » Heat leak will likely be too high
  - » Safety hazards due to enrichment of LOX on cold surfaces
  - » Large amounts of condensed gases in vacuum space can lead to other problems including rapid pressure rise upon warming and possible solid conduction
  - » Best practice is to be at least 10<sup>-3</sup> torr before cooling, lower pressures are better but there may be operational tradeoffs

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### **Outgassing and Getters**



- All material outgas into a vacuum. This can raise the pressure in a sealed vacuum space
- Reduce outgassing by:
  - Minimize amount of polymers, wire insulation, FRP etc difficult
  - Keep vacuum surfaces as clean as possible. Remove any oil or cutting fluid, wear gloves etc.
- Getters: materials inserted into vacuum spaces to remove residual gas at low pressures
- In cryogenic systems, getters may be useful in removing residual gas and passively managing small leaks



### **Outgassing and Getters**



- 3 types of getters
  - Adsorbers –gas bonds to surface
    - » Activated charcoal, silica gel
    - » Effectiveness increases with decreasing temperature good for cryogenic systems
  - Chemical getters chemical reaction between material and gas
    - » Ba & other Alkali metals not very common in cryogenics
  - Solution or absorber getters gas is absorbed in interstitial space of metals
    - » Ti, Zr, Th works well with H<sub>2</sub>, O<sub>2</sub> and N<sub>2</sub>
    - » Much better at room temperature
    - » Occasional use in room temperature applications in cryogenic systems



# Getters, Cryogenics and Gilligan's island



- It turns out that one of the most common and effective materials used for getters of low pressure He gas is activated charcoal made from coconut husks.
- There is a significant amount of this material in the LHC magnet cryostats



The Professor says: "Lets look for the Higgs!"



# Foam & Other Insulation Methods

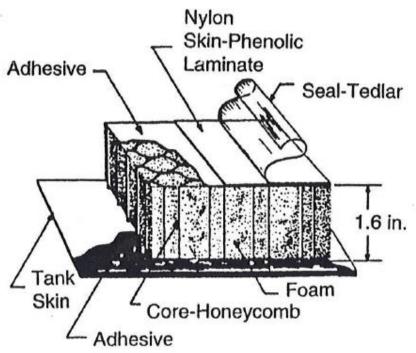


- Not all cryogenic systems use vacuum insulation
- This is particularly true of storage vessels for fluids other than helium
- Reasons for using alternatives to vacuum insulation
  - Cost
  - Weight Space shuttle main tank
  - Required hold time related to size
  - Complex vessel shapes
- Some solutions
  - Expanded closed or open cell foams
  - Rock wool, fiberglass or other porous material
- These all require vapor barriers to prevent air from being pulled into the insulation and condensed (can cause both a safety hazard via O<sub>2</sub> enrichment & reduce effectiveness)



# Design Example: Complex Foam Insulation System: LH<sub>2</sub> Tank for 2<sup>nd</sup> Stage Saturn V





From Cryogenic Engineering, Flynn

- Allows helium purging of the insulation
- Weight ~ 4.15 kg/m<sup>2</sup>
- Performance: measured effective thermal conductivity (0.86 1.1 mW/cm K) at T<sub>av</sub> = 144 K Note this includes conduction, convection and radiation heat transfer





- Frequently the largest source of heat leak to cryogenic systems
- Fundamental Equation: Stefan-Boltzmann Law energy emitted from an ideal black body:  $E_b = \sigma T^4$  where  $\sigma = 5.67x10^{-8}$  W/m<sup>2</sup>K<sup>4</sup>
  - Real world Assumptions:
    - » Emissivity ( $\varepsilon$ ) << 1 and independent of wavelength (grey body)
    - » Two parallel infinite plates: Radiative heat flux (W/m²)

Eq. A 
$$q_r = \left(\frac{\varepsilon_1 \varepsilon_2}{\varepsilon_1 + \varepsilon_2 - \varepsilon_1 \varepsilon_2}\right) \sigma \left(T_1^4 - T_2^4\right)$$

» Frequently in cryogenic systems  $\varepsilon_1 \sim \varepsilon_2 << 1$  then Eq. A becomes:

Eq. B 
$$q_r = \left(\frac{\varepsilon}{2}\right) \sigma \left(T_1^4 - T_2^4\right)$$





» Two long concentric cylinders or concentric spheres (1 represents the inner cylinder): the radiative heat flux (W/m²) on the inner cylinder is

Eq. C 
$$q_1 = \left(\frac{\sigma\left(T_1^4 - T_2^4\right)}{\frac{1}{\varepsilon_1} + \left(\frac{A_1}{A2}\right)\left(\frac{1}{\varepsilon_2} - 1\right)}\right)$$

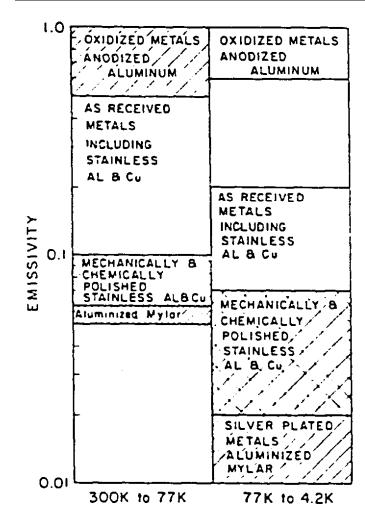
» Note as is frequently the case in cryogenics, if the spacing between the cylinders is small compared to the inner radius (i.e.  $A_1 \sim A_2$ ) Eq. C becomes Eq. A





- Looking at Eq. A, How do we reduce the radiation heat transfer?
- We could reduce the emissivity (ε)
  - This is done in some cases; using either reflective tape or silver plating
  - Better below 77 K
  - It's also part of MLI systems (see below)
  - We have to consider tarnishing
  - May be labor intensive

From Helium Cryogenics - S. W. Van Sciver







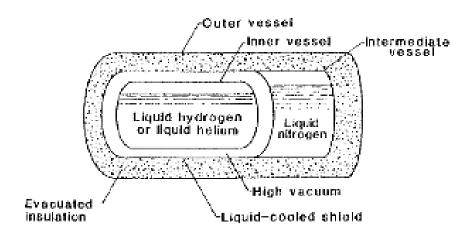
- Another way to reduce radiation heat transfer is to install intermediate actively cooled radiation shields that operate at a temperature between 300 K and the lowest cryogenic temperature. This has several advantages.
  - It greatly reduces the heat load to the lowest temperature level
    - » Assume parallel plates with  $\varepsilon = 0.2$
    - » then from Eq. B q (300 K 4.2 K) = 46 W/m<sup>2</sup> while q (77 4.2) = 0.2 W/m<sup>2</sup>
  - It allows heat interception at higher temperatures & thus better Carnot efficiency
  - Such an actively cooled shield provides a convenient heat intercept for supports, wires etc to reduce conduction heat leak.
- Shields may be cooled by
  - Liquid baths (LN<sub>2</sub>)
  - Vapor boil off from stored liquid common in LHe storage dewars
  - Cooling flows from refrigeration plants
  - Conductive cooling via small cryocoolers



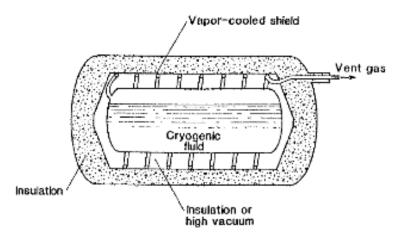
# **Examples of Cooled Radiation Shields**



- LN<sub>2</sub> bath surrounds inner LHe or LH<sub>2</sub> bath
- Baths are separated by a vacuum insulation space



- Shield is cooled by boil off gas from stored cryogen
  - Spacing of cooling tubes on shield may be calculated by:  $\Delta T = qL^2/2kt$ 
    - »  $\Delta T$  = max allowable temperature difference between any point on shield and tube
    - » q = heat flux on shield
    - » k = shield thermal conductivity
    - »  $L = \frac{1}{2}$  max tube spacing
    - » t = shield thickness



From Cryogenic Engineering, Flynn

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### **Thermal Radiation Shields**



- Uncooled thermal radiation shields placed in a vacuum space between the warm & cold surfaces also help reduce the thermal radiation heat leak
- It can be shown (with the grey approximation and equal emissivities) that with N shields thermal radiation heat transfer is given by:

$$q = \frac{\varepsilon}{(N+1)2} \sigma \left( T_H^4 - T_L^4 \right)$$

This is the motivation behind Multilayer Insulation



### MultiLayer Insulation

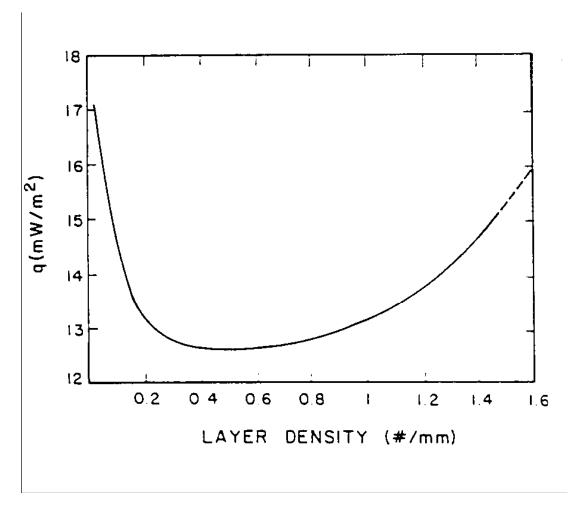


- Also referred to as superinsulation
- Used in the vacuum space of many cryostats (10<sup>-5</sup> torr or better for best performance)
- Consists of highly reflective thin sheets with poor thermal contact between sheets.
  - Made of aluminized Mylar ( or less frequently Kapton)
  - May include separate non conducting mesh
  - May use Mylar aluminized on only one side and crinkled to allow only point contacts between sheets
  - Frequently perforated to allow for better pumping
- Can be made up into blankets for ease of installation
- Don't pack MLI too tightly. Optimal value is ~ 20 layers / inch
- Great care must be taken with seams, penetrations and ends.
  - Problems with these can dominate the heat leak



### MLI

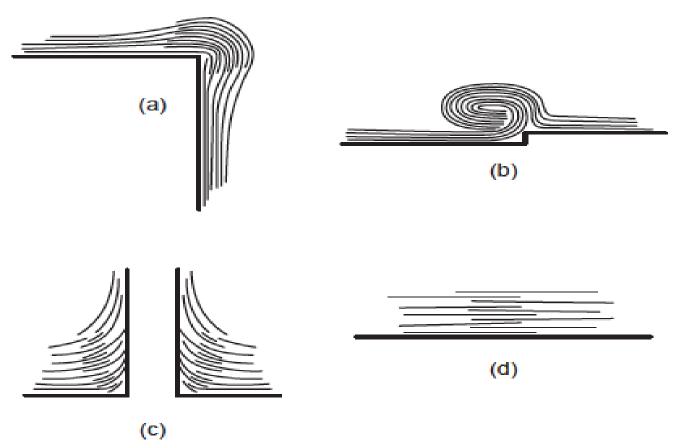






# **Examples of Proper MLI Installation**





From "Cryogenic Engineering" in Wiley Mechanical Engineer's Handbook



### **MLI Example from LHC cryostats**





"SERIES-PRODUCED HELIUM II CRYOSTATS FOR THE LHC MAGNETS: TECHNICAL CHOICES, INDUSTRIALISATION, COSTS" A. Poncet and V. Parma Adv. Cryo. Engr. Vol 53



#### **Porous Insulation**



- Radiation heat transfer may also be reduced by filling the vacuum space between 300 K and cryogenic temperatures with other materials that are low conductivity and block line of sight
- Such materials include:
  - Glass beads or microspheres
  - Perlite powder (made from a volcanic rock)
  - Opaciated powders copper or other metallic flakes mixed in with other powders to further reduce radiant heat transfer
  - Aerogel
- Advantages:
  - Cheaper
  - Easier to install in complex shapes
  - Better performance than MLI in poor or no vacuum
- Frequently used in large storage and transport dewars



### **Porous Insulation**



The total heat transfer through porous insulation between 2 spheres may be estimated by:

$$W = \frac{\overline{k}(T_2 - T_1)}{t} \sqrt{A_1 A_2}$$

- Where
  - t = thickness of Insulation
  - $\overline{k}$  = the mean thermal conductivity
  - 1 = inner vessel and 2 = outer vessel
- Mean thermal conductivities may be found in references such as <u>Cryogenic Engineering</u> by Flynn



# Comparison of Thermal Insulation Approaches (6 inch thick insulation in all cases)



	Total Heat Flux ( W/m²)	
Type of Insulation	300 K to 77 K	77 K to 20 K
Polystyrene Foam (2 lb/ft <sup>3</sup> )	48.3	5.6
Gas Filled Perlite powder (5 – 6 lb/ft <sup>3</sup> filled with He)	184.3	21.8
Perlite powder in vacuum (5 – 6 lb/ft³)	1.6	0.07
High Vacuum (10 <sup>-6</sup> torr $\epsilon = 0.02$ )	9	0.04
Opacified powder (Cu flakes in Santocel)	0.3	-
MLI	0.03	0.007

Increasing Cost & Complexity

Note better performance of evacuated Perlite over high vacuum between 300 K & 77 K



### Cryostat Design

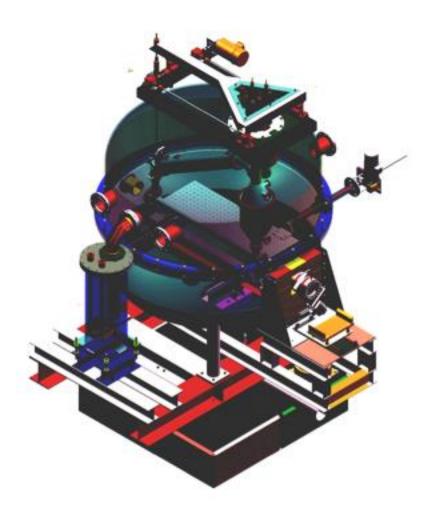


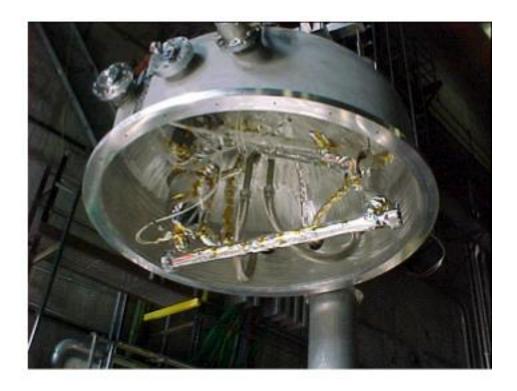
- What is a cryostat?
  - A device or system for maintaining objects at cryogenic temperatures.
- Cryostats which contain superconducting RF systems are traditionally called cryomodules (term originally coined by Jlab)
- Cryostats whose principal function is to store cryogenic fluids are frequently called Dewars. Named after the inventor of the vacuum flask and the first person to liquefy hydrogen



# E158 LH<sub>2</sub> Target Cryostat









# Cryostat Design



- Cryostats are one of the technical building blocks of cryogenics
- Cryostat design involves many subtopics:
  - Development of requirements covered here
  - Materials selection already covered
  - Thermal insulation already covered
  - Support systems covered here
  - Safety covered in a future lecture
  - Instrumentation covered in a future lecture
- One of the best ways to learn about cryostat design is through examples (see next 2 talks) Also:
  - Cryostat Design J.G. Weisend II (Ed) Springer (2016)
- There are many different types of cryostats with differing requirements
  - The basic principles of cryostat design remain the same
  - Before we can do anything else we have to define our requirements



## **Cryostat Requirements**



- Maximum allowable heat leak at various temperature levels
  - This may be driven by the number of cryostats to be built as well as by the impact of large dynamic heat loads (SCRF or target cryostats)
- Alignment and vibration requirements
  - Impact of thermal cycles
  - Need to adjust alignment when cold or under vacuum?
  - Alignment tolerances can be quite tight (TESLA :
  - +/- 0.5 mm for cavities and +/- 0.3 mm for SC magnets)
- Number of feed throughs for power, instrumentation, cryogenic fluid flows, external manipulators



## **Cryostat Requirements**



- Safety requirements (relief valves/burst discs)
  - Design safety in from the start. Not as an add on
- Size and weight
  - Particularly important in space systems
- Instrumentation required
  - Difference between prototype and mass production
- Ease of access to cryostat components
- Existing code requirements (e.g. TUV or ASME)
- Need, if any, for optical windows
- Presence of ionizing radiation



### **Cryostat Requirements**



- Expected cryostat life time
- Will this be a one of a kind device or something to be mass produced?
- Schedule and Cost
  - This should be considered from the beginning

### All Design is Compromise