Superconducting radiofrequency cavities – An introduction

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Goals of this lecture

• SRF is a humongous topic! – offered as a separate 3-credit USPAS course
• Here, we will look at basics of SRF cavities including the topics of:
  • Working principle
  • Figures of merit
  • Cavity types
  • Processing techniques for performance enhancement
• Look at some new frontiers in SRF
Introduction

Superconducting radiofrequency (SRF) cavities
• A technology for production of energetic particle beams,
• Invented half-a-century ago, matured via solid R&D
• One of the two largest applications of low temperature superconductivity

Today, SRF cavities is a core technology used in the construction of large linear particle accelerators for discovery science
• Electron-positron collider
• X-ray/light sources
• Neutron, neutrino production
• Acceleration of rare isotopes, heavy ions
RF cavity working principle

- Metallic cells maintain a standing-wave RF field
- Particle bunches in phase with the RF field gain energy
- RF fields penetrate a penetration depth, $\delta$, the metallic cell walls and dissipate heat in the surface resistance, $R_s$
- A coolant on the outside extracts the heat and prevents the cavity from heating above its operating temperature
RF surface resistance

Why is RF surface resistance a key parameter?

• Dissipated power in the cavity is proportional to its surface resistance
• The cost of cooling the cavity (coolant fluid, temperature, fluid pumping power, etc.) scales with dissipated power
• With hundreds of cavities in a particle accelerator, the cavity cooling cost forms a significant fraction of accelerator operating cost

Keeping low RF surface resistance is therefore necessary to reduce the accelerator operating cost.
Normal vs. superconducting cavities

How does the surface resistance compare?

Water cooled copper cavities near room temperature

\[ R_s = \frac{1}{\sigma \delta} = \sqrt{\frac{\mu_0 \omega}{2\sigma}} \]

\( \omega = \) angular frequency
\( \sigma = \) electrical conductivity

With \( \sigma \sim 5.8 \times 10^7 \text{ S/m} \) at 1.5 GHz and 300 K, we get \( R_s = 10 \text{ m}\Omega \)

Liquid helium cooled niobium cavity \( \leq \sim 5 \text{ K} \)

\[ R_s = R_{BCS}(T) + R_{res} \]

\[ A \frac{\omega^2}{T} \exp\left( -1.85 \frac{T_c}{T} \right) + R_{res} \]

At 1.5 GHz and 2 K, and neglecting the residual \( R_{res} \), we get \( R_s = 20 \text{ n}\Omega \)
Normal vs. superconducting cavities

Ratio of surface resistance at 1.5 GHz:
\[
\frac{R_s(\text{niobium, } 2K)}{R_s(\text{copper, } 300K)} = \frac{20 \, n\Omega}{10 \, m\Omega} \sim 10^{-6}
\]

Penalty for 2 K cryogenics:
\[
\eta_{\text{Carnot}} = 0.67\% \quad \eta_{\text{plant}} \leq 20\%
\]

Even after accounting the premium for 2 K cryogenics, SRF drives down the cooling driven operating cost by a factor $\sim 1000$ !!!

The significantly lower surface resistance in SRF also offers other benefits:

- Cavities can be operating with 100% RF duty cycle that facilitate production of high average power particle beams
- Cavities can be made with larger aperture (by relaxing shunt impedance) that reduce loss of high-power beams during transport through the cavity
Helium cooling of SRF cavities

Liquid helium 1.8 – 4.2 K

Optimal operating temperature with helium?

\[ R_s = A \left( \frac{1}{T} \right) f^2 e^{\frac{(T)}{kT}} + R_0 \]

- The surface resistance goes up with frequency and down with temperature: lower temperature equals less resistance, particularly at higher frequencies
- What is the optimal temperature?
  - Above about 500 – 700 MHz you win by operating below 4.2 K (typically 1.8 – 2 K)
  - At lower frequencies (eg. 80 MHz) you are better at 4.2 K thermodynamically but there may be other considerations (FRIB)
  - Between these limits it’s a fairly broad minimum. Most systems operate ~ 2 K – He II

Content courtesy: J. G. Weisend II (ESS)
# SRF accelerators under operation/construction

<table>
<thead>
<tr>
<th>Name</th>
<th>Accelerator Type</th>
<th>Lab</th>
<th>T (K)</th>
<th>Refrigeration Capacity</th>
<th>Status</th>
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<tr>
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<td>Electron Linac</td>
<td>JLab</td>
<td>2.1</td>
<td>4.2 kW @ 2.1 K</td>
<td>Operating</td>
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<td>Proton Linac</td>
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<td>Proton Linac</td>
<td>Fermilab</td>
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<td>288 L/Hr</td>
<td>Operating</td>
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<td>S-DALINAC</td>
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<td>TU Darmstadt</td>
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<td>120 W @ 2.0 K</td>
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<td>Electron Linac</td>
<td>DESY</td>
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<td>2.5 kW @ 2 K</td>
<td>Under construction</td>
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<td></td>
<td></td>
<td></td>
<td>5-8</td>
<td>4 kW @ 5-8 K</td>
<td></td>
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<td>40-80</td>
<td>26 kW @ 40-80 K</td>
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<td>Heavy Ion Linac</td>
<td>ANL</td>
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<td>1.2 kW @ 4.7</td>
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<td>Accelerator</td>
<td>SLAC</td>
<td>2.0 K</td>
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<td></td>
<td>2.6 kW @ 4.5-6 K</td>
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<tr>
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<td>MSU</td>
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<td></td>
<td>4.5</td>
<td>4.5 kW @ 4.5 K</td>
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</tbody>
</table>

Content courtesy: J. G. Weisend II (ESS)
SRF cavity – figures of merit

Accelerating gradient, $E_{acc}$
- defined as the ratio of the accelerating voltage, $V_c$, divided by the cavity length, $L$. $V_c$ is obtained by integrating the electric field at the particle’s position as it traverses the cavity:

$$E_{acc} = \frac{V_c}{L} = \frac{1}{L} \left| \int_0^L E_z (r = 0, z) e^{i\omega_0 z/c} \, dz \right|$$

- $\omega_0$ = RF frequency
- $c$ = speed of light in vacuum
- $z$ = beam travel direction

Intrinsic quality factor, $Q_0$
- defined as the ratio of the energy stored, $U_{\text{stored}}$ divided by the energy dissipated in in one RF period, $P_{\text{diss}}$

$$Q_0 = \frac{\omega_0 U_{\text{stored}}}{P_{\text{diss}}} = \frac{\omega_0 \mu_0 \int_V |H|^2 \, dv}{\int_S R_s |H|^2 \, ds} = \frac{G}{R_s}$$

- $G$ = shape factor (a constant)
- $R_s$ = surface resistance
- $H$ = magnetic field (A/m)
Higher $E_{acc}$ = Larger energy gain per length

Higher $Q_0$ = Lower cryogenic heat load

Real ‘high-field’ Losses (HFQS)

BCS + residual resistance

Only BCS resistance

Q slope

Good

Ideal
SRF cavity – figures of merit

**Peak field ratios** (geometry dependent only, smaller are better)

\[
\frac{B_{\text{peak}}}{E_{\text{acc}}} \quad \text{Determines max. } E_{\text{acc}} \text{ that can be generated before reaching quench magnetic field at the cavity surface}
\]

\[
\frac{E_{\text{peak}}}{E_{\text{acc}}} \quad \text{Determines max. } E_{\text{acc}} \text{ that can be generated before } E_{\text{peak}} \text{ induced field emission sets in}
\]

**Shunt impedance, } R_{sh} \text{ (geometry dependent only, larger is better)**

\[
R_{sh} = \frac{V_{c}^{2}}{P_{\text{diss}}} = \frac{(E_{\text{acc}}L)^{2}}{P_{\text{diss}}}
\]

A measure of voltage that can be generated for a given dissipated power (analogous to Ohm’s law)
**Dissipated power**

\[
P_{\text{diss}} = \frac{(E_{\text{acc}} L)^2}{(R_{sh}/Q) * Q_0} \quad \text{DF} = \frac{(E_{\text{acc}} L)^2 (R_{\text{res}} + R_{\text{BCS}})}{(R_{sh}/Q) * G}
\]

- \(E_{\text{acc}} L\) = **Voltage gain** – dictated by end-application
- \(\text{DF} = \text{RF duty factor}\) – fraction of unit time when the RF power supply is ON; usually dictated by end-application
- \(P_{\text{diss}} = \text{Cryogenic load}\) – need to minimize this to lower the cost of refrigeration
- \(R_{sh}/Q*G = \text{Geometry factor}\) – should be made as high as practical; this is optimized using FEA codes during cavity design stage
- \(R_s = R_{\text{res}} + R_{\text{BCS}}(T)\) = **RF surface resistance** – must be kept small; several recipes for surface treatment have been developed to reduce \(R_{\text{res}}\)
Electrons are ‘light’ and attain $\beta \approx 1$ over ‘short’ acceleration distance
  • Can use elliptical cavities immediately after injector

Protons and ions are ‘heavy’ and need gradual acceleration over long length
  • Start with low-\(\beta\) cavity after injector followed by cavities with gradually increasing $\beta$
SRF cavities for Fermilab PIP-II

PIP-II is a proton accelerator being built at Fermilab that will provide 800 MeV proton beam for neutrino experiments.

- **Half Wave Resonator**
  - $\beta = 0.11$, $Q_0 = 0.85 \times 10^{10}$
  - $162.5$ MHz, $v/c = 0.11$

- **Single Spoke SSR1**
  - $\beta = 0.22$, $Q_0 = 0.82 \times 10^{10}$
  - $325$ MHz, $v/c = 0.22$

- **Single Spoke SSR2**
  - $\beta = 0.47$, $Q_0 = 0.82 \times 10^{10}$
  - $325$ MHz, $v/c = 0.47$

- **Elliptical LB650**
  - $\beta = 0.61$, $Q_0 = 2.4 \times 10^{10}$
  - $650$ MHz, $v/c = 0.61$

- **Elliptical HB650**
  - $\beta = 0.92$, $Q_0 = 3.3 \times 10^{10}$
  - $650$ MHz, $v/c = 0.92$

Increasing proton energy
PIP-II linac layout

PIP-II Superconducting RF CW Linac, 800 MeV
Consists of Five Types of Cryomodules

- **Cryoplant**
- **Single Spoke**
  - SSR1 X 2
  - 16 Cavities
  - 325 MHz
- **Single Spoke**
  - SSR2 X 7
  - 35 Cavities
  - 325 MHz
- **Elliptical**
  - HB650 X 4
  - 24 Cavities
  - 650 MHz
- **Elliptical**
  - LB650 X 9
  - 36 Cavities
  - 650 MHz

**H- Ion source**

**CDS**
- 8 Cavities
- 162.5 MHz

**RFQ**
- 2.1 MeV

**Room Temperature**
- 10 MeV
- 32 MeV
- 177 MeV
- 516 MeV
- 833 MeV

**Superconducting**

**PIP-II Linac is technically complex, state of the art superconducting RF accelerator**

**PIP-II is the world’s highest energy and power CW proton linac, and the U.S. first accelerator project to be built with major international contributions**
SRF cavity material

- **Niobium** has been the material of choice for SRF cavities for the last ~50 years
- Some of the best superconducting properties of all elements including highest critical temperature $T_c \sim 9.2$ K and high $H_{c1} \sim 190$ mT
- Easy metallurgy – purify, make sheets, form, weld, heat treat. No need to achieve precise stoichiometry as niobium is not a compound or alloy
- Good structural and thermal properties in bulk form, doesn’t react with water
- SRF grade niobium is $\text{RRR} > 300$ that provides good bulk thermal conductivity for heat conduction from RF surface to helium coolant
- Some accelerators (eg. LEP at CERN) used bulk copper cavities sputtered with a few microns of niobium on the inner RF surface
Surface processing techniques

- Niobium cavities are produced from bulk sheets deep drawn into the desired shape (e.g., elliptical half-cells) and then e-beam welded together.
- The cavities undergo several heat/surface treatments before assembly in an accelerator. The goals are to:
  - Repair the RF surface as well as reduce bulk stresses arising from the fabrication processes.
  - Enhance the surface RF properties for maximizing $Q_0$.
- Common steps (both done to all cavities):
  1. Bulk electropolishing – 100-200 um of ‘damaged’ RF surface is removed.
  2. $800^\circ$C bake in vacuum for ~3 hours (aka high T bake) – reduce residual stress, improve microstructure, remove absorbed hydrogen during fabrication process.
Surface processing techniques

• **Special treatments** – these are selected according to the desired performance ($Q_0$ and $E_{acc}$):

  1. **Buffer Chemical Polishing (BCP):**
     - 10-20 um of RF surface is etched using 1:1:2 solution of hydrofluoric, nitric and phosphoric acids
     - Cavities shows good performance up to ~20 MV/m followed from Q-slope
  2. **Electropolishing:**
     - 10-20 um of RF surface is etched using hydrofluoric and sulfuric acids usually with ratio 1:10
     - Cavities shows good performance up to ~25 MV/m followed from Q-slope
  3. **Low T bake:**
     - Vacuum baking at 120 °C for ~48 hours
     - Cavities do not see the Q-slope and gradient up to ~40 MV/m can be attained
Surface processing techniques

- **Special treatments** – these are selected according to the desired performance ($Q_0$ and $E_{acc}$):

  4. **Nitrogen doping**:
     - After high T bake, nitrogen is let in the furnace at a constant pressure of 25 mTorr;
     - cavity is let to anneal for several minutes and then heating is stopped
     - The cavity is cooled and then 5-10μm of material is removed by electropolishing
     - $E_{acc}$ can be pushed beyond 50 MV/m

  5. **Nitrogen infusion**:
     - After high T bake, the furnace temperature is lowered to 120-160 °C
     - Nitrogen is let in at 25 mTorr
     - Temperature is held steady for ~48 hours
     - No chemical treatment done after cooling the cavity to room temperature
     - The technique produces very high $Q_0$ and highest $E_{acc}$
Effect of surface treatments on performance

![Graph showing the effect of surface treatments on performance. The graph plots $Q_0$ against $E_{acc}$ (MV/m). The treatments include N-doped, N-infused, 120 °C baked, EP, and BCP. The graph highlights HFQS ~20 MV/m and HFQS ~25 MV/m.]
Practically important aspects of SRF cavities

- Local magnetic fields (including the Earth’s) degrade cavity performance ($Q_0$)
  - Result is that cavities are designed with passive and sometimes active magnetic shields. Use of magnetic materials near cavities must be carefully examined
- Cavities are resonant structures that require tuning frequently at cryogenic temperatures
- Vibrations (microphonics) can detune cavities depending on cavity stiffness and design
  - This may put strict limits on vibrations near cavities
  - Use of He II (see lecture on superfluid helium) prevents bulk boiling in the helium bath that may affect the cavity tune

Content courtesy: J. G. Weisend II (ESS)
SRF cavities – cost perspective

Processed One-Cell
$40k Cadillac CTS

New Nine-Cell
$85k BMW M5

Dressed Nine-Cell
$250k Aston Martin DBS

Content courtesy: A. Rowe (Fermilab)
New frontiers in SRF

**Nb$_3$Sn as an alternative to traditional niobium**

- Superconductor with $T_c \approx 18$ K, almost twice that of niobium’s 9.2 K
- Has significantly lower $R_{BCS}$ than niobium at liquid helium temperatures $< 4.2$ K
- If $R_{res}$ is kept small (by ensuring proper stoichiometry, surface treatments, and magnetic shielding), Nb$_3$Sn cavities exhibit very high $Q_0$ even at $\sim 4$ K
  - An accelerator can be operated with 4.2 K LHe systems, which are much cost effective compared to 2 K helium systems needed for niobium cavities
- Active research areas – growing thin layer of Nb$_3$Sn on inner walls of niobium cavities; cooling and mag-shielding techniques to minimize trapped flux

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New frontiers in SRF

Cryogen-free, cryocooler conduction cooled SRF cavities

- Use closed-cycle 4 K cryocoolers and conduction links to extract $P_{diss}$ from Nb3Sn SRF cavities
  - Liquid helium around the SRF cavity not needed
    - $\rightarrow$ no cryoplant, no distribution or recovery system
    - $\rightarrow$ no complex pressure vessel design of the cryomodule
- Cryocoolers are plug-n-play machines that turn on/off with the push of a button
  - Unlike helium cryo-plants that are operationally complex
- Potential use of conduction cooled SRF in e-beam irradiation machines for industrial applications:
  - Industrial and municipal waste-water treatment
  - Medical device sterilization, medical waste treatment
- Active research areas
  - Design of cavities and thermal links for SRF conduction cooling
  - Design of low heat leak, magnetically shielded, compact cryomodules
New frontiers in SRF

Fermilab efforts for conduction cooled SRF cavity development
Fermilab efforts for conduction cooled SRF cavity development

World’s first demonstration of practical $E_{acc}$ on a conduction cooled SRF cavity
R. C. Dhuley et al., https://doi.org/10.1088/1361-6668/ab82f0

Conduction cooled SRF test setup at Fermilab
New frontiers in SRF

Other ongoing efforts for conduction cooled SRF cavity development

Jefferson Lab
- 1.5 GHz
- Cold sprayed + electrodeposited copper

Cornell University
- 2.6 GHz
- Copper clamps

https://doi.org/10.1088/1757-899X/755/1/012136

New frontiers in SRF

Compact e-beam accelerator development at Fermilab using conduction cooled SRF cavities
Further reading