



# U.S. Particle Accelerator School

## July 15 – July 19, 2024

# VUV and X-ray Free-Electron Lasers

## Transverse Focusing

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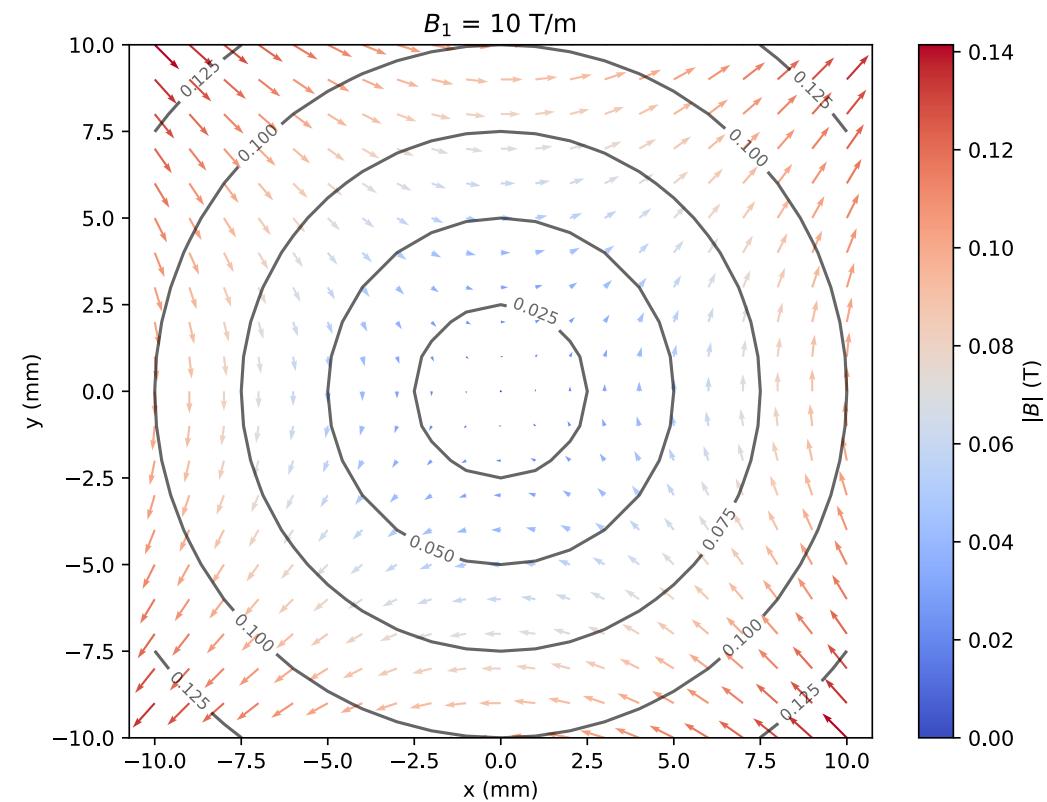
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<sup>2</sup> SLAC National Accelerator Laboratory

<sup>3</sup> Xelera



# Quadrupole Fields & Forces



An ideal upright quadrupole field is defined by

$$B_x(x, y) = B_1 y$$

$$B_y(x, y) = B_1 x$$

$$B_1 = \frac{dB_x}{dy} \Big|_{x,y=0}$$

The transverse force on charged particle moving along the  $z$  axis is then

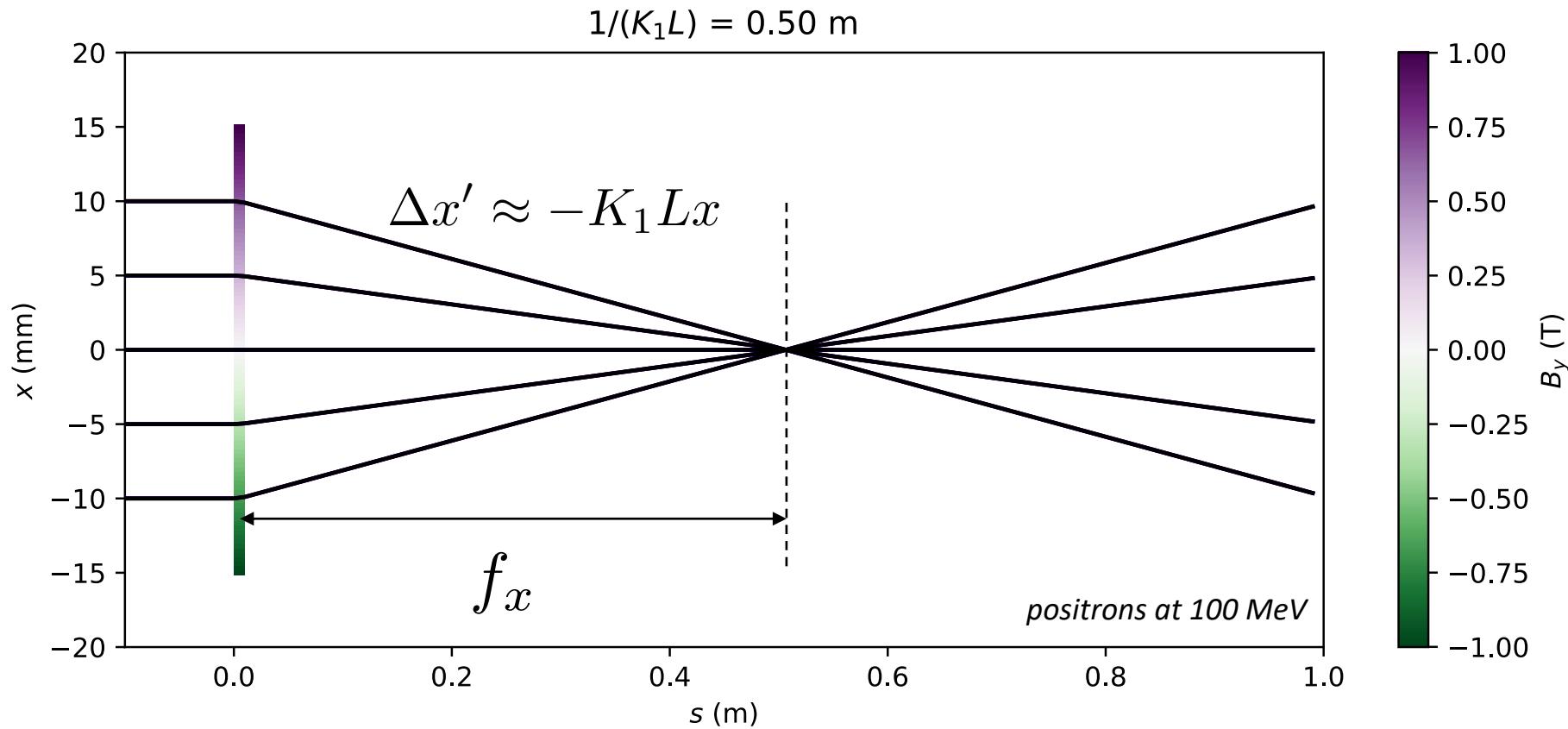
$$\frac{dx'}{ds} = -K_1 x$$

$$\frac{dy'}{ds} = +K_1 y$$

$$K_1 \equiv \frac{qB_1}{p_0}$$

# Thin Quadrupole lens

For a thin quadrupole with effective length  $L$ , we can identify the focal lengths in the  $x$  and  $y$  planes



$$\frac{dx'}{ds} = -K_1 x$$

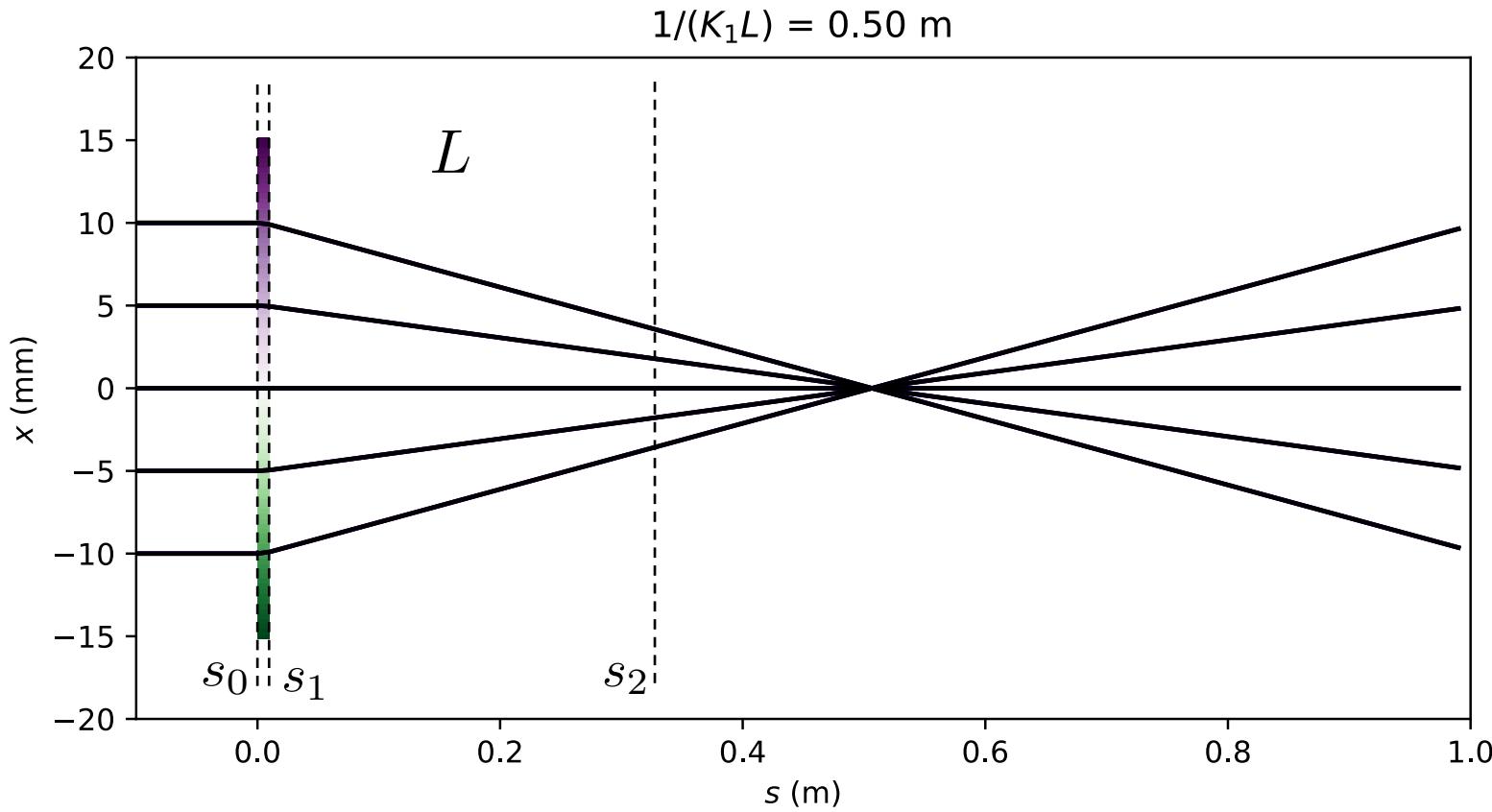
$$\frac{dy'}{ds} = +K_1 y$$

$$f_x = \frac{1}{K_1 L}$$

$$f_y = -f_x$$

# Thin Quad, Drift transfer matrices

Thin linear maps for quadrupole and drifts illustrate the building blocks of map analysis:



positrons at 100 MeV

Thin quad map from 0 to 1:

$$\begin{pmatrix} x_1 \\ x'_1 \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ -1/f_x & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$

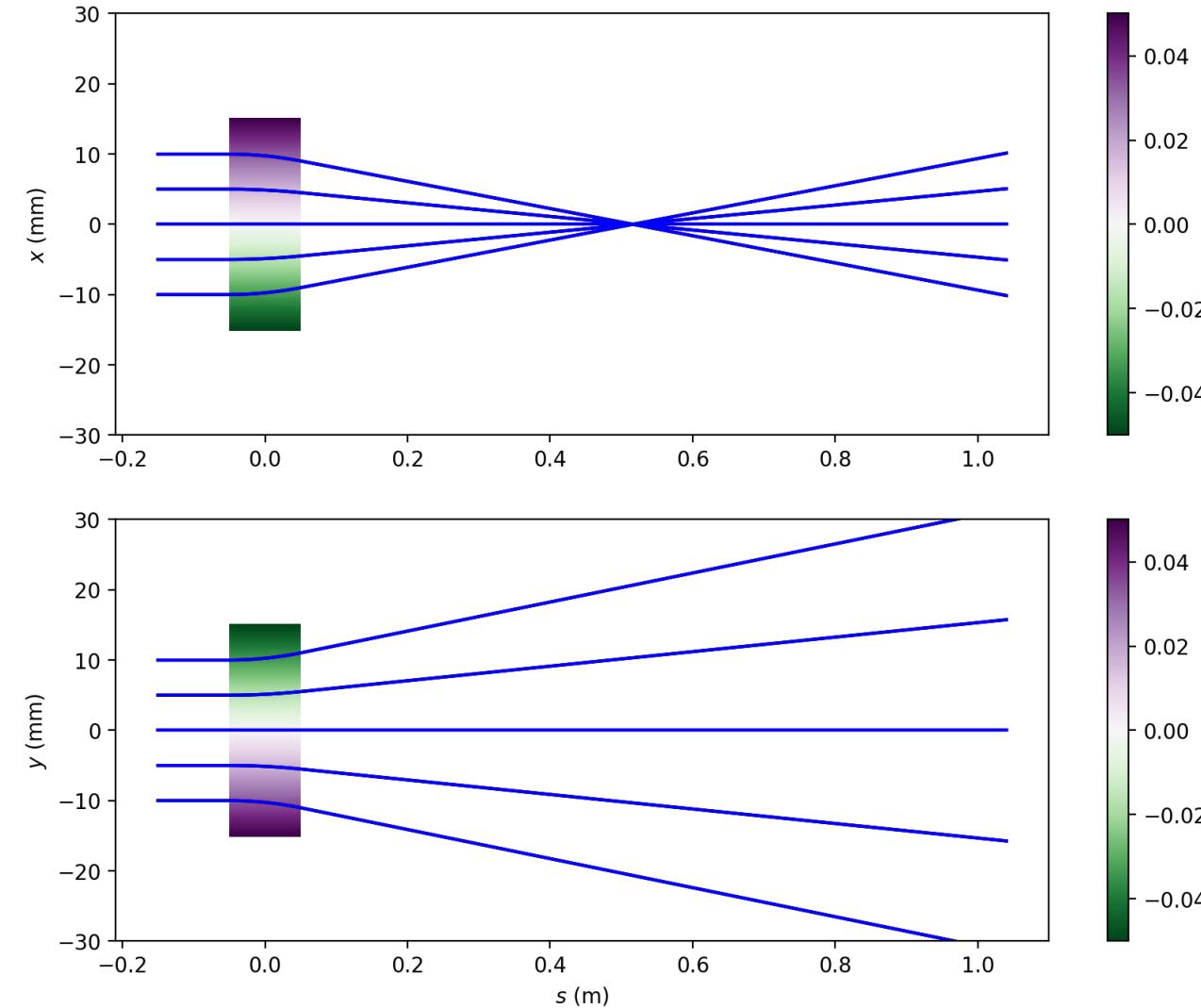
Drift map from 1 to 2:

$$\begin{pmatrix} x_2 \\ x'_2 \end{pmatrix} = \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix} \begin{pmatrix} x_1 \\ x'_1 \end{pmatrix}$$

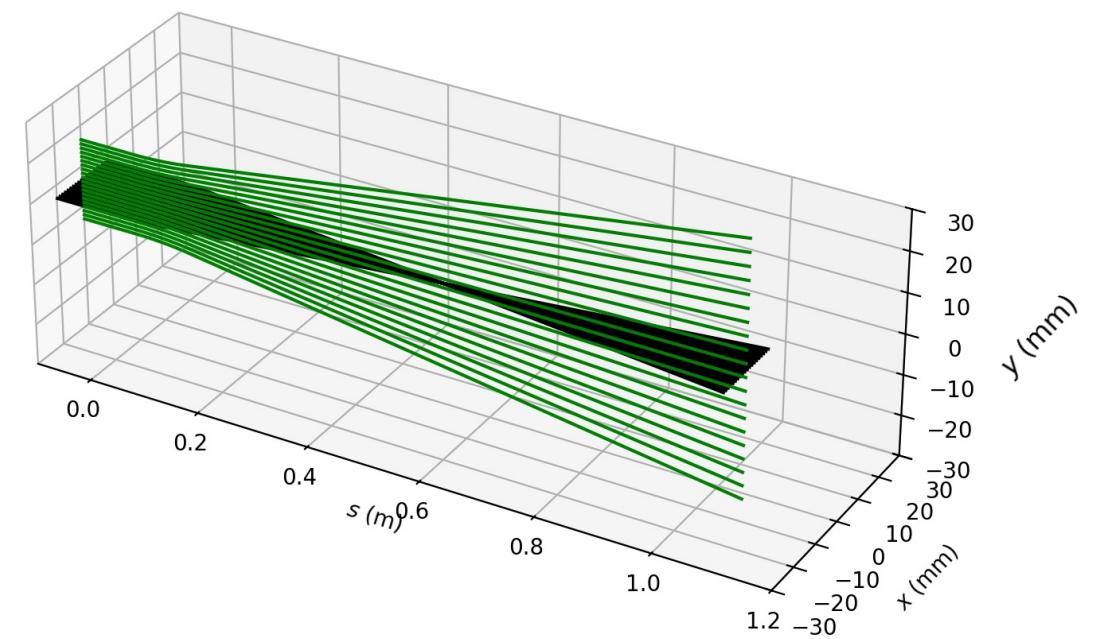
Linear map from 0 to 2:

$$\begin{pmatrix} x_2 \\ x'_2 \end{pmatrix} = \begin{pmatrix} 1 - L/f_x & L \\ -1/f_x & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ x'_0 \end{pmatrix}$$

# Thick Quadrupole Focusing

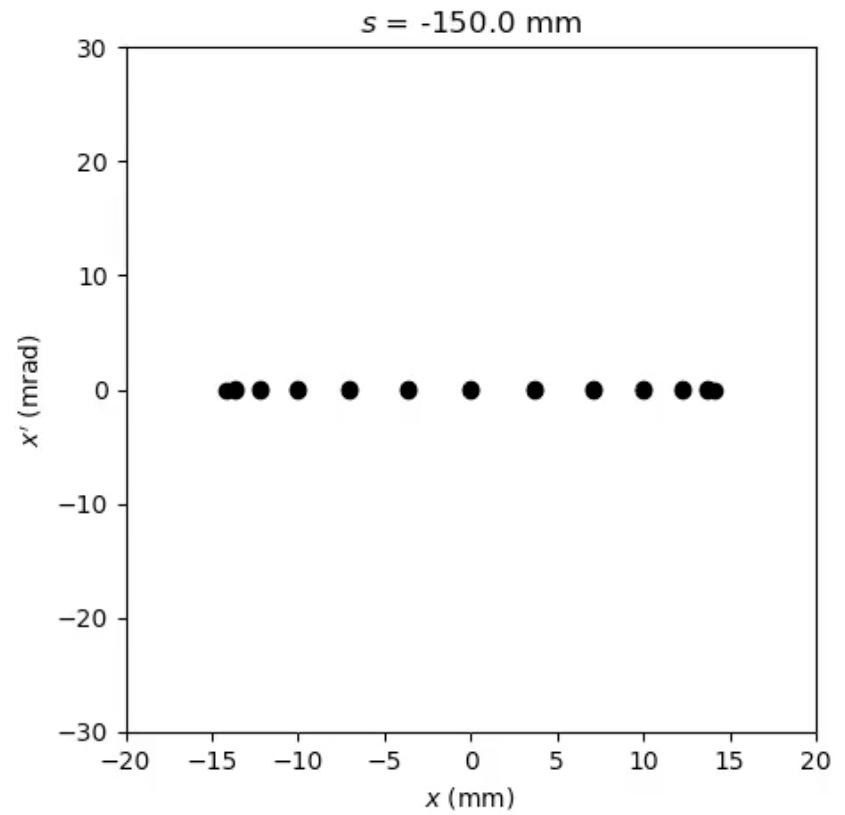
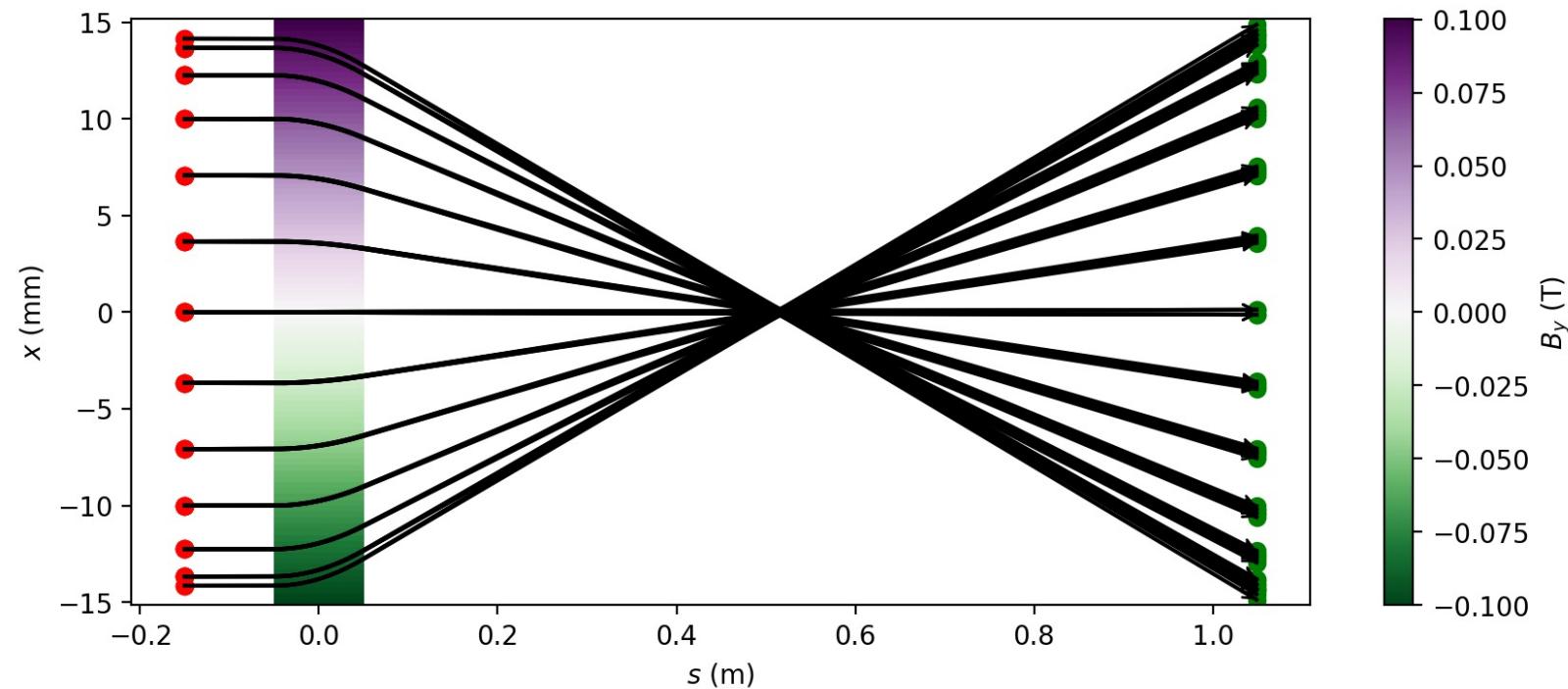


A quadrupole that focuses in one plane will always defocus in the other plane.



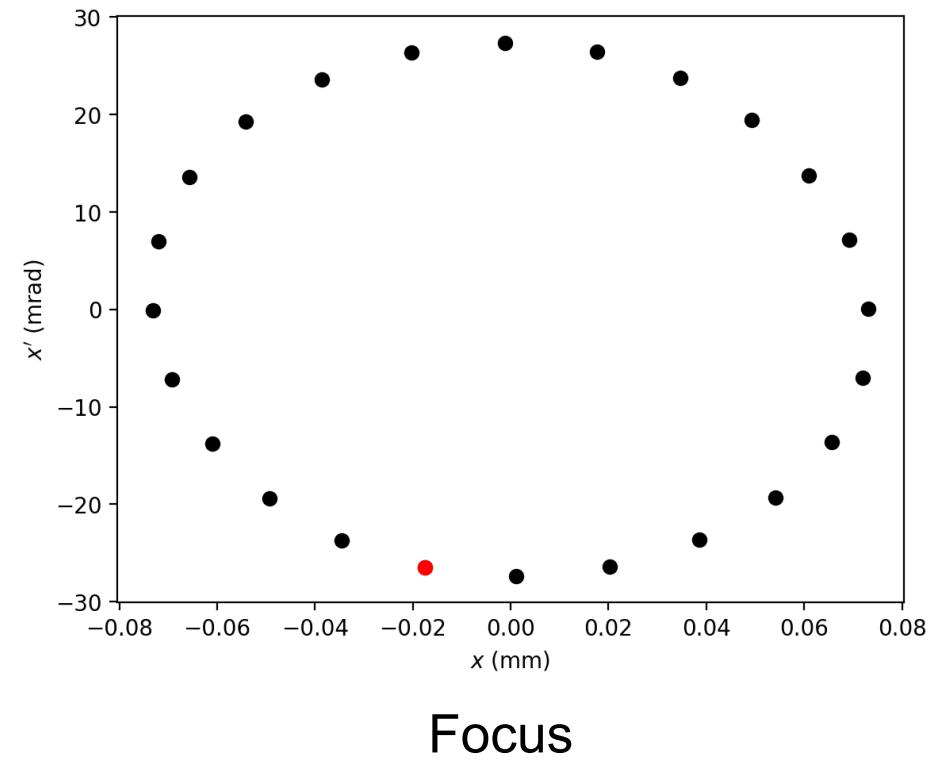
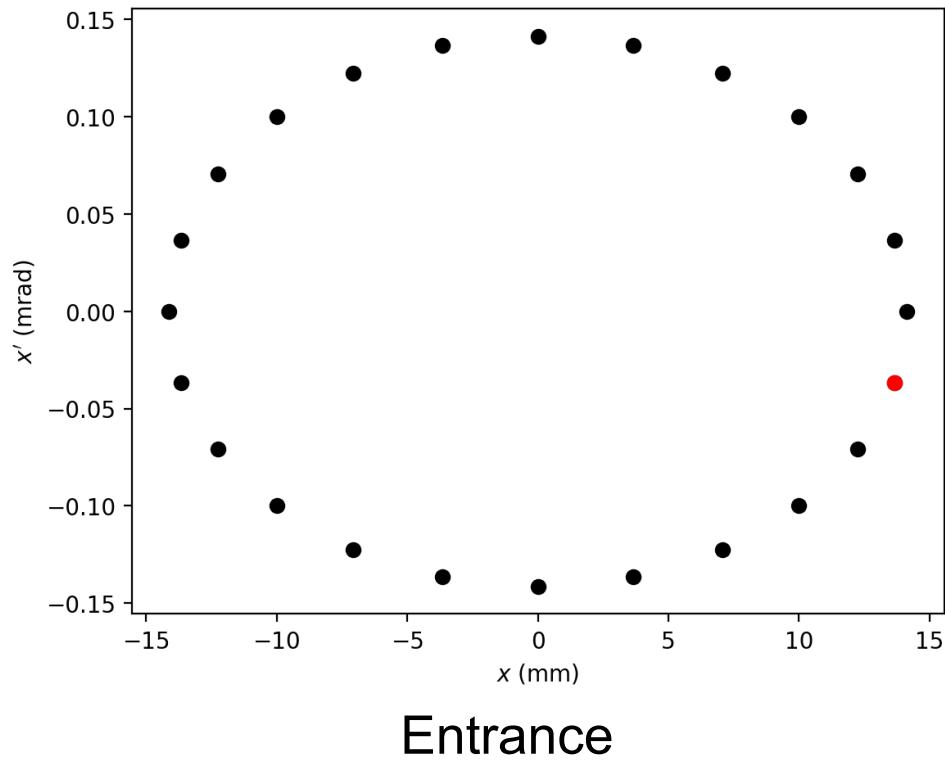
# 2D phase space

Here is the motion in 2D ( $x$ ,  $x'$ ) phase space.



# 2D phase space

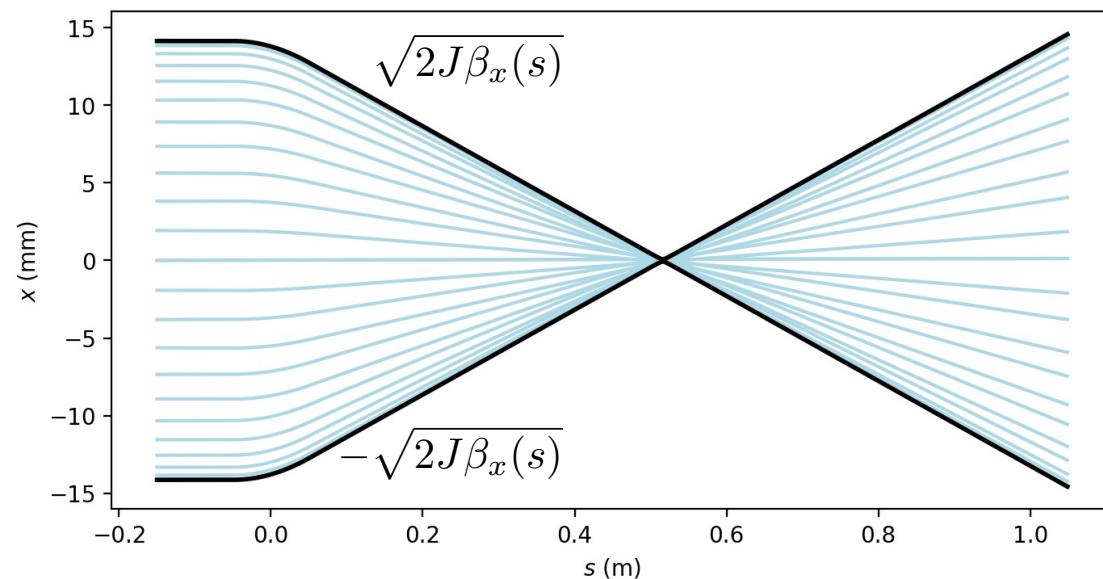
A closer look shows that the particles are initially started on an ellipse in phase space, and that the phase space area enclosed by this ellipse is conserved. This is because a transfer matrix derived from a Hamiltonian is **symplectic**, which has determinant 1 (“area preserving”)



# Action-Angle coordinates

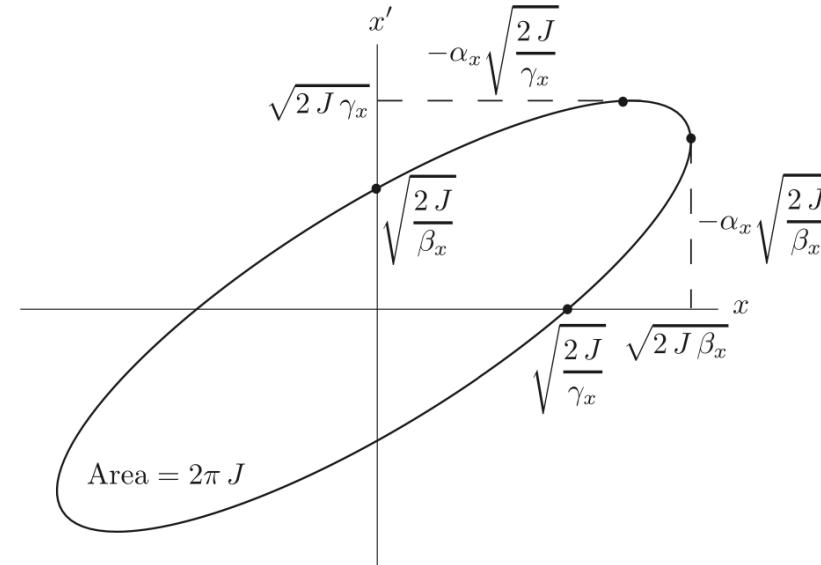
An alternative way to view particle motion in the transverse phase space is to use action-angle coordinates:

$$\begin{pmatrix} x \\ x' \end{pmatrix} = \sqrt{2J} \begin{pmatrix} \sqrt{\beta_x} & 0 \\ -\frac{\alpha_x}{\sqrt{\beta_x}} & \frac{1}{\sqrt{\beta_x}} \end{pmatrix} \begin{pmatrix} \sin(\psi_x + \phi) \\ \cos(\psi_x + \phi) \end{pmatrix}$$



Amplitude:	$J$
Phase:	$\psi_x(s) + \phi$
Beta function:	$\beta_x(s)$
Alpha function:	$\alpha_x(s)$

Particles with the same amplitude will lie on an ellipse in transverse phase space:



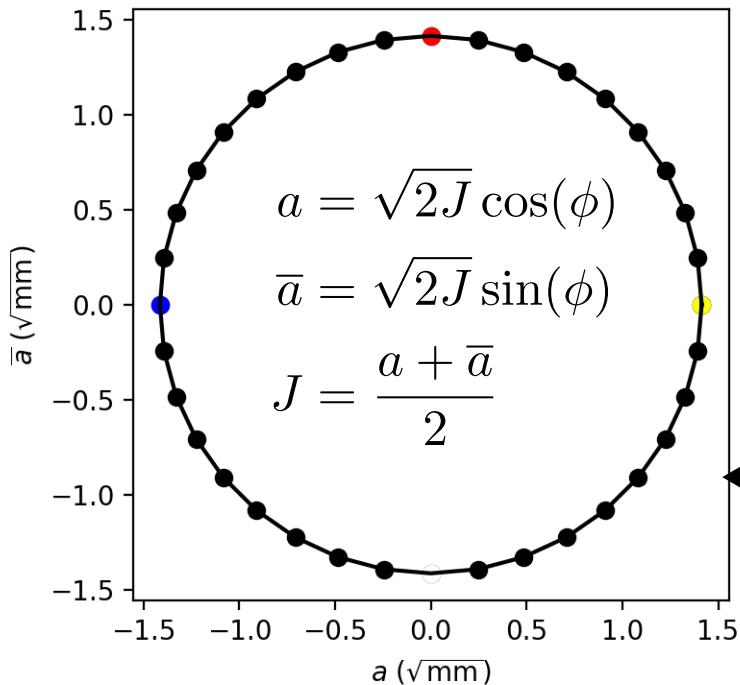
$$\psi_x(s) \equiv \int_0^s \frac{1}{\beta_x(s)} ds$$

$$\alpha_x \equiv -\frac{1}{2}\beta'_x$$

$$\gamma_x = \frac{1 + \alpha_x^2}{\beta_x}$$

# Normalized Coordinates

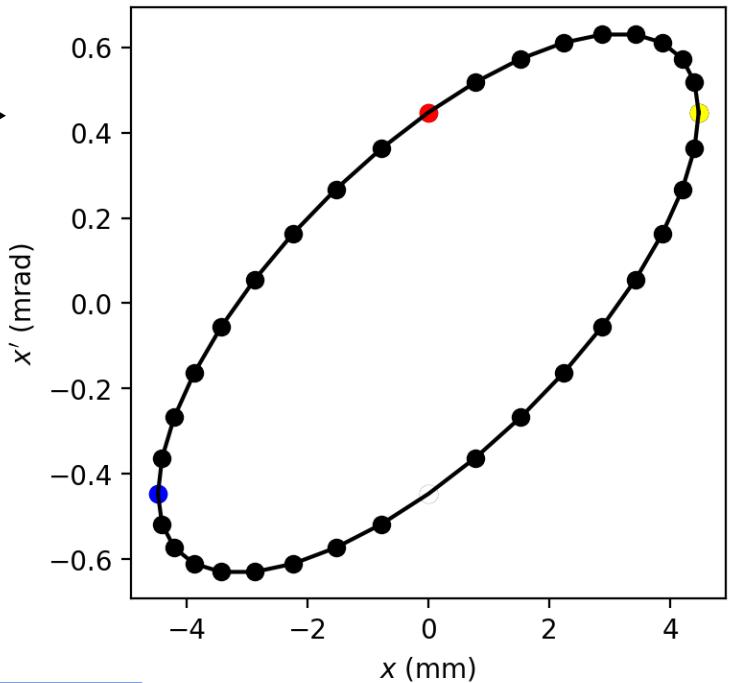
$$\begin{pmatrix} a \\ \bar{a} \end{pmatrix} = \begin{pmatrix} \frac{1}{\sqrt{\beta}} & 0 \\ \frac{\alpha}{\sqrt{\beta}} & \sqrt{\beta} \end{pmatrix} \begin{pmatrix} x \\ x' \end{pmatrix}$$



$$A = \begin{pmatrix} \sqrt{\beta} & 0 \\ -\frac{\alpha}{\sqrt{\beta}} & \frac{1}{\sqrt{\beta}} \end{pmatrix}$$

$$A^{-1} = \begin{pmatrix} \frac{1}{\sqrt{\beta}} & 0 \\ \frac{\alpha}{\sqrt{\beta}} & \sqrt{\beta} \end{pmatrix}$$

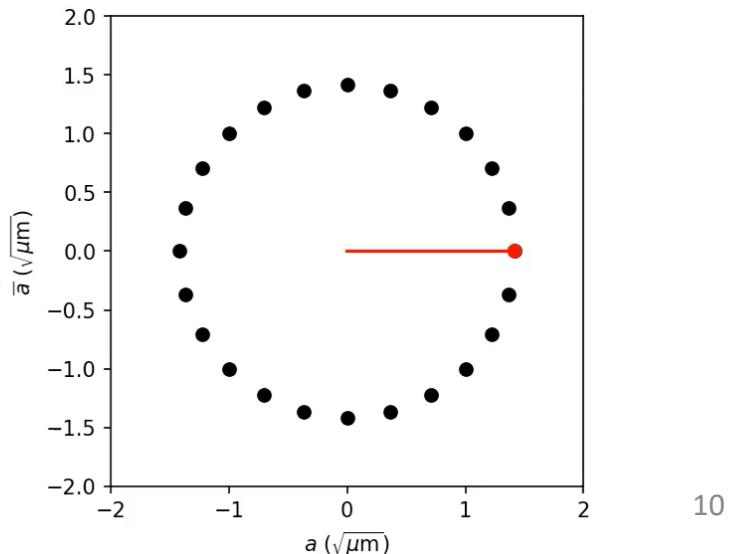
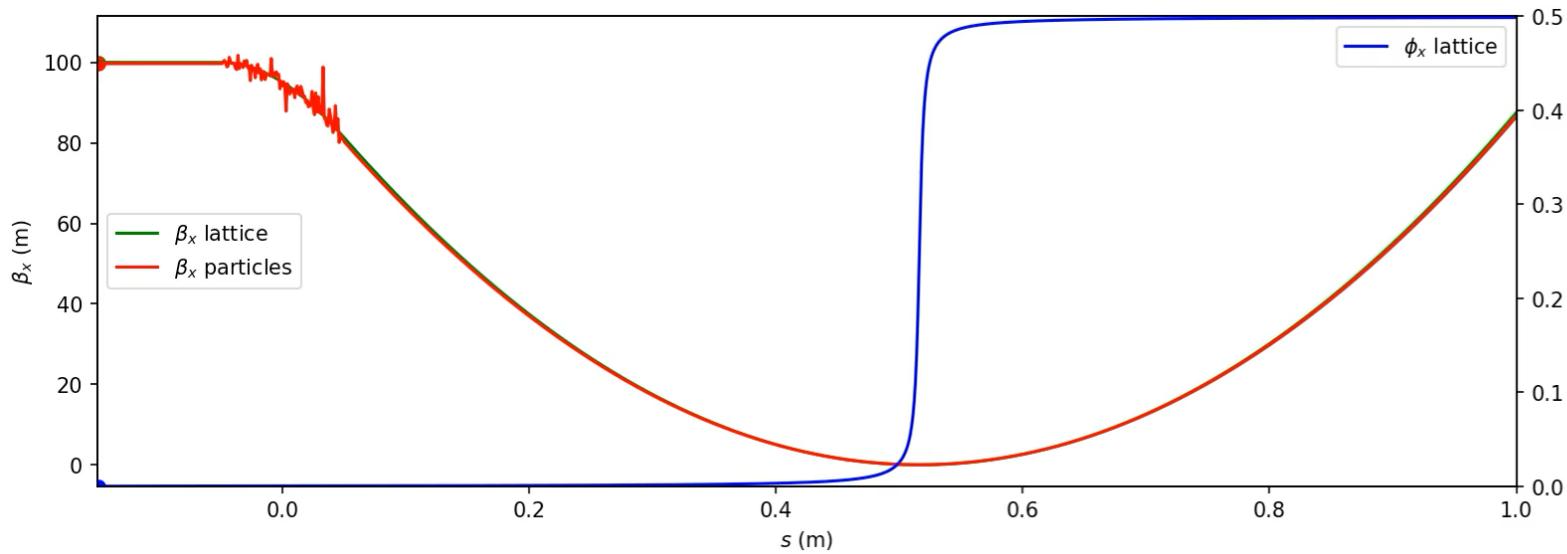
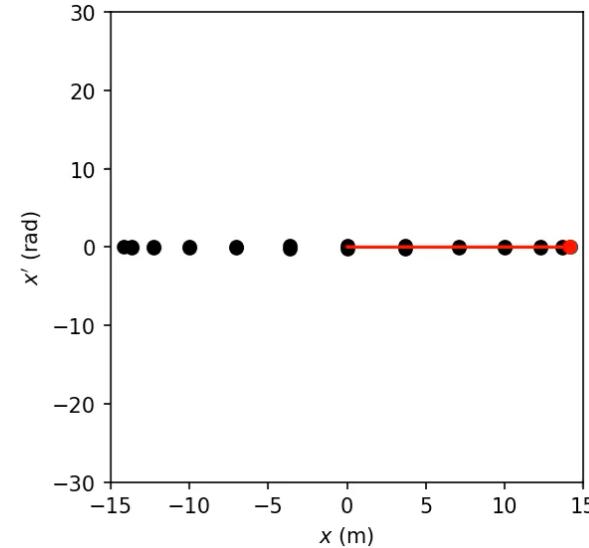
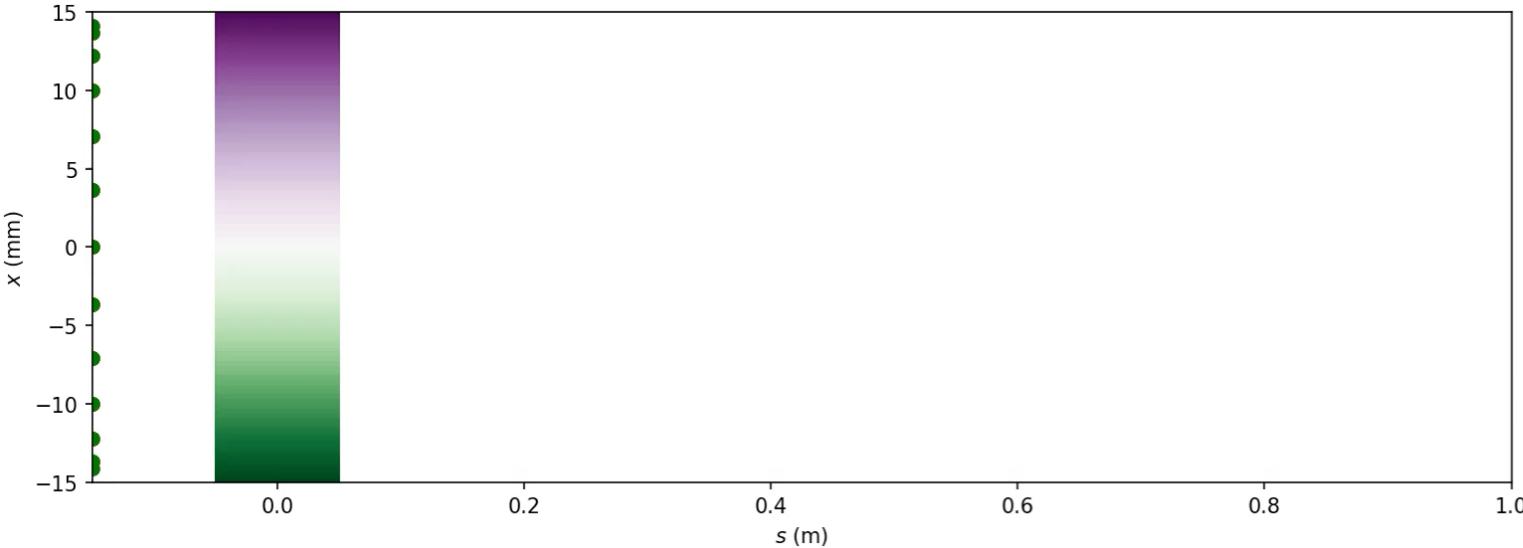
$$\begin{pmatrix} x \\ x' \end{pmatrix} = \begin{pmatrix} \sqrt{\beta} & 0 \\ -\frac{\alpha}{\sqrt{\beta}} & \frac{1}{\sqrt{\beta}} \end{pmatrix} \begin{pmatrix} a \\ \bar{a} \end{pmatrix}$$



“Courant-Synder Invariant”

$$2J = \frac{(\alpha^2 + 1)}{\beta} x^2 + 2\alpha x x' + \beta x'^2$$

# Normalized Coordinates



# Twiss Propagation

It can be shown that the Twiss parameters at one location along  $s$  can be related to another by the transfer matrix  $M$  between these locations:

$$T_x(s_1) = M \cdot T_x(s_0) \cdot M^T$$

where the Twiss matrix is defined as:

$$T_x \equiv \begin{pmatrix} \beta_x & -\alpha_x \\ -\alpha_x & \gamma_x \end{pmatrix}$$

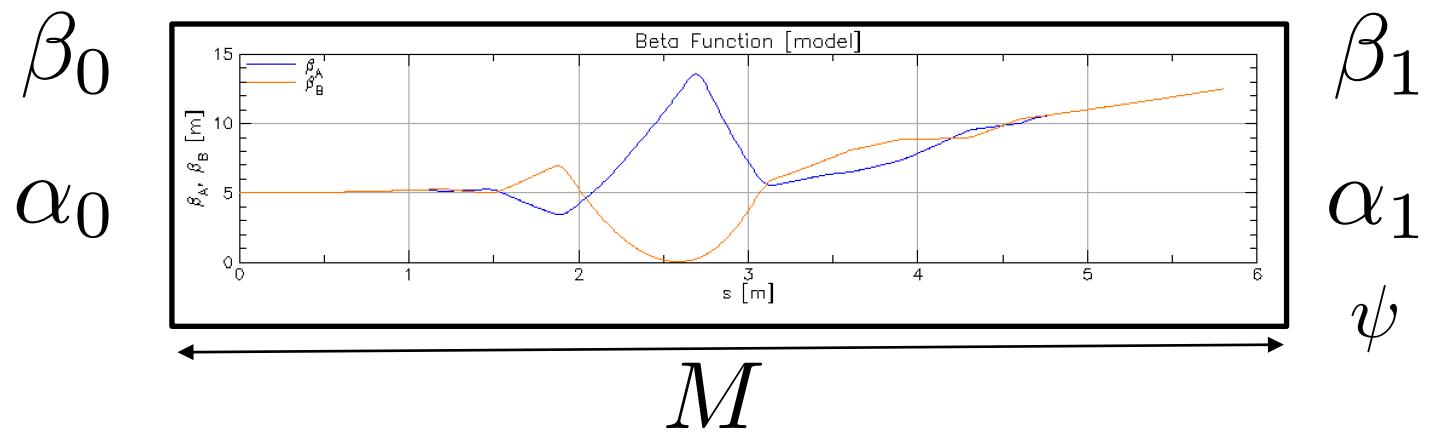
# Matrix from Twiss

A transfer matrix can also be written in terms of beginning and ending Twiss parameters, denoted by 0 and 1 respectively:

$$M = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} = \begin{pmatrix} \sqrt{\frac{\beta_1}{\beta_0}} (\cos \psi + \alpha_0 \sin \psi) & \sqrt{\beta_0 \beta_1} \sin \psi \\ \frac{(\alpha_0 - \alpha_1) \cos \psi - (1 + \alpha_0 \alpha_1) \sin \psi}{\sqrt{\beta_0 \beta_1}} & \sqrt{\frac{\beta_0}{\beta_1}} (\cos \psi - \alpha_1 \sin \psi) \end{pmatrix}$$

Note that this decomposition is not unique, because it depends on the initial Twiss to be defined.

However, with a periodic system, the decomposition is unique.



# Periodic Twiss from Matrix

The transfer matrix can also be used to define a periodic system. Setting beginning and ending Twiss to be the same in the previous slide gives:

$$\begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} = \begin{pmatrix} \cos \psi + \alpha \sin \psi & \beta \sin \psi \\ -\frac{(1+\alpha^2)}{\beta} \sin \psi & \cos \psi - \alpha \sin \psi \end{pmatrix}$$

This is easily solved:

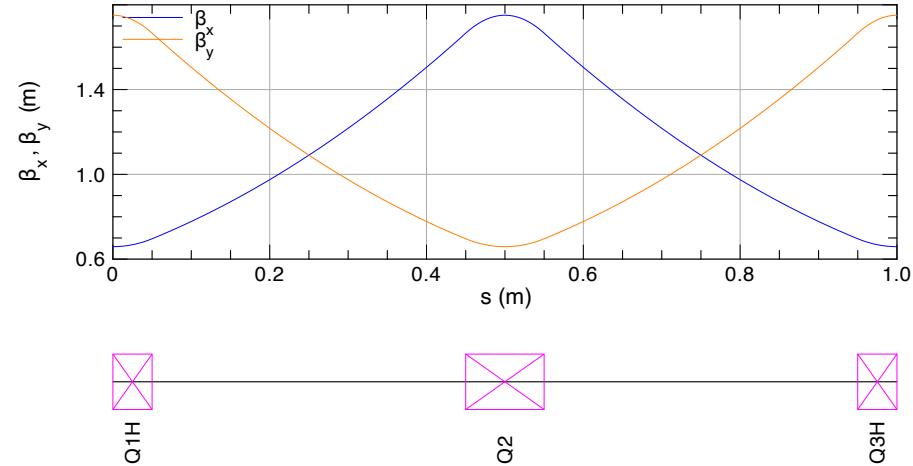
$$\cos \psi = \frac{1}{2}(M_{11} + M_{22})$$

$$\beta = \frac{M_{12}}{\sqrt{1 - (M_{11} + M_{22})^2/4}}$$

$$\alpha = \frac{1}{2} \frac{M_{11} - M_{12}}{\sqrt{1 - (M_{11} + M_{22})^2/4}}$$

There is a real periodic solution only if:  $\frac{1}{2} |M_{11} + M_{22}| \leq 1$

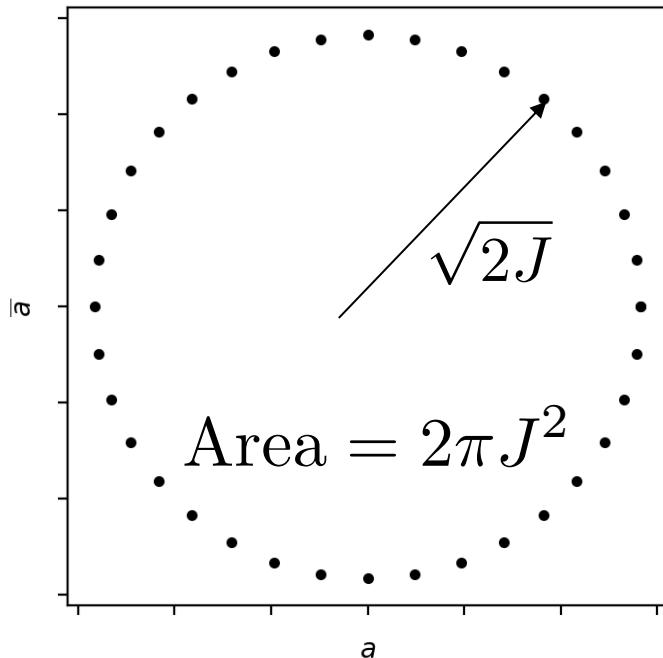
Example: FODO Cell



0.56682984	0.54276144 m
-1.25046455	0.56682984 m

# Twiss from Particles

Twiss parameters can also be determined from particle distributions. To understand this, consider a distribution of particles with amplitude  $J = \epsilon_x$  and uniform distribution in phases:



Transforming to physical coordinates:

$$\begin{pmatrix} x \\ x' \end{pmatrix} = \begin{pmatrix} \sqrt{\beta} & 0 \\ -\frac{\alpha}{\sqrt{\beta}} & \frac{1}{\sqrt{\beta}} \end{pmatrix} \begin{pmatrix} a \\ \bar{a} \end{pmatrix}$$

and averaging over phases reveals:

$$\langle x^2 \rangle = \epsilon_x \beta_x$$

$$\langle x'^2 \rangle = \epsilon_x \gamma_x$$

$$\langle x, x' \rangle = -\epsilon_x \alpha_x$$

*geometric emittance:*  $\epsilon_x = \sqrt{\langle x^2 \rangle \langle x'^2 \rangle - \langle x x' \rangle^2}$

$$\langle J \rangle = \epsilon_x$$

# Mismatch

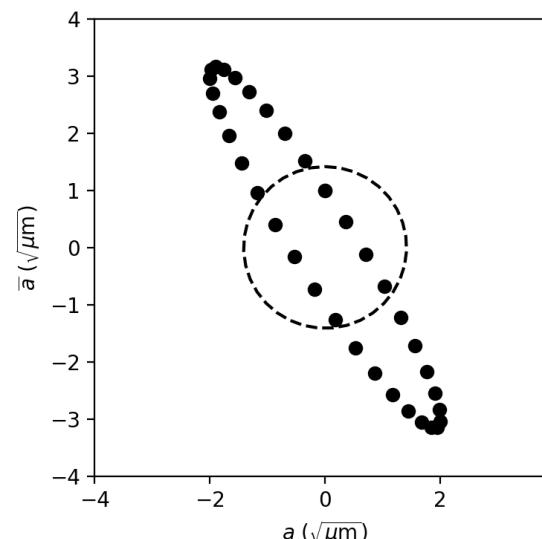
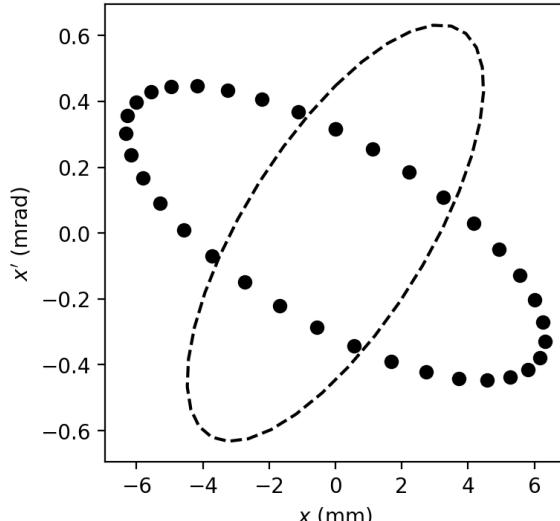
A beam is **mismatched** when its statistical Twiss parameters are not the same as the designed Twiss parameters. To quantify this, recall that the design Twiss parameters define the amplitude according to:

$$2J = \frac{(\alpha^2 + 1)}{\beta} x^2 + 2\alpha x x' + \beta x'^2$$

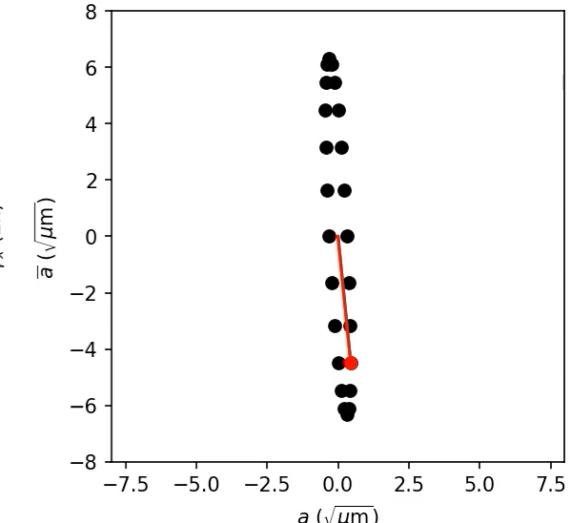
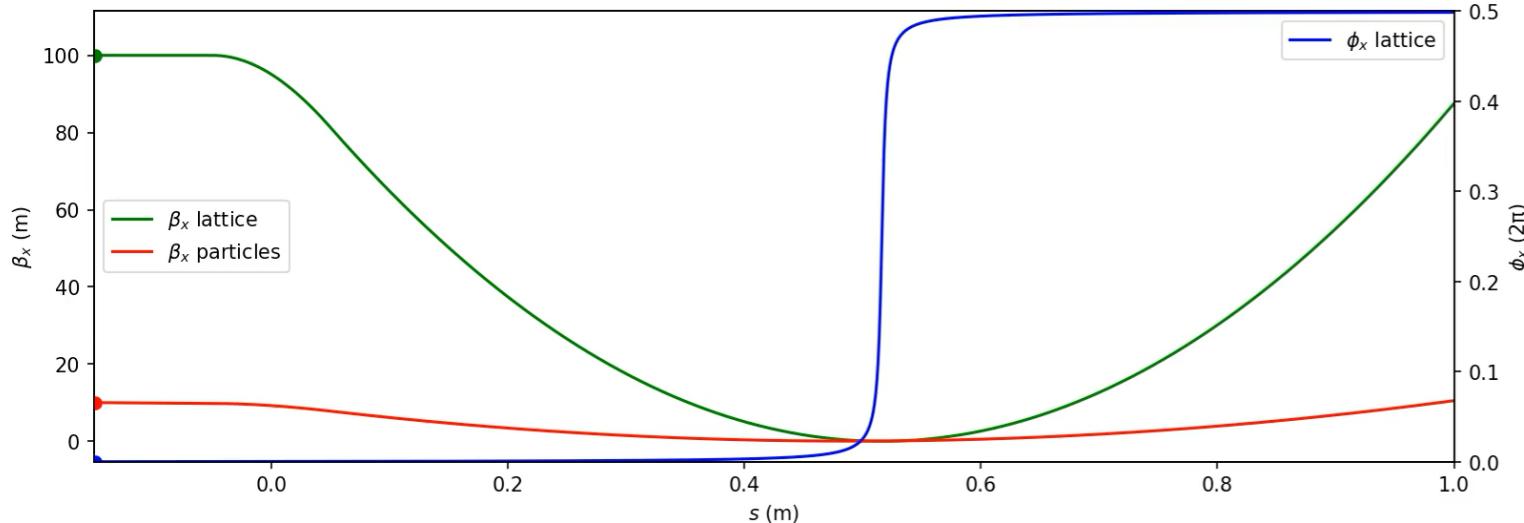
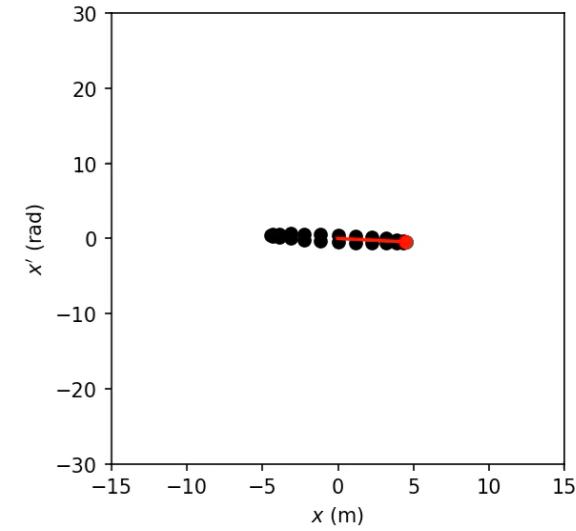
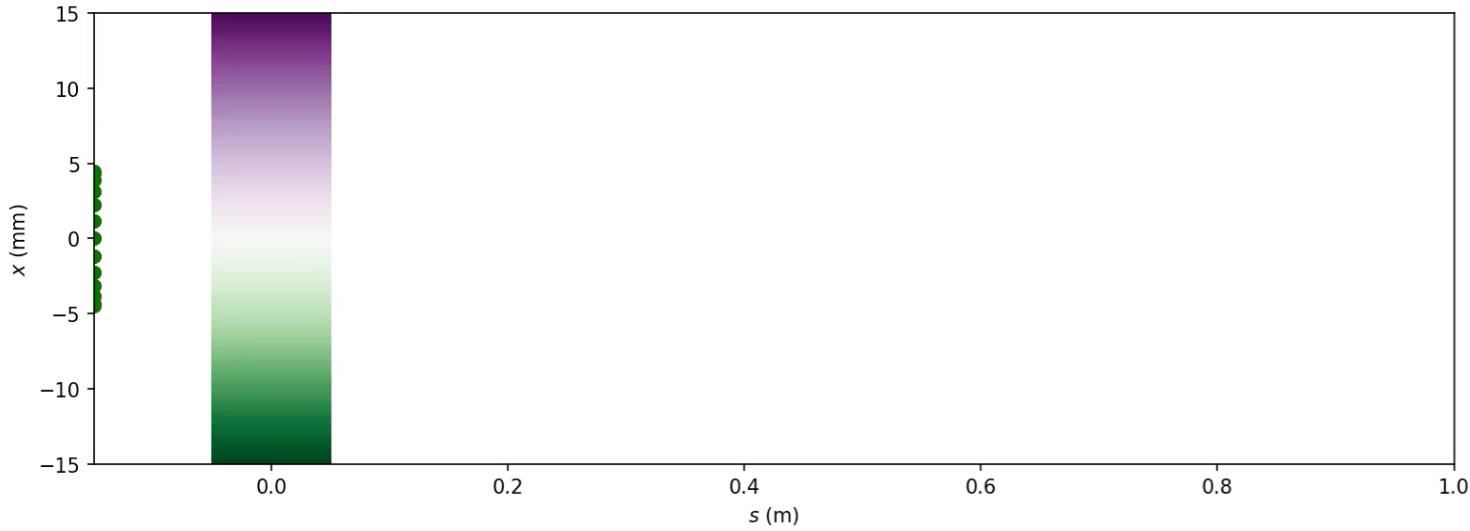
Labeling 0 for the design and 1 for the particles and averaging:

$$\langle 2J_1 \rangle = \frac{(1 + \alpha_0^2)}{\beta_0} \underbrace{\langle x_1^2 \rangle}_{\beta_1 \epsilon_1} + 2\alpha_0 \underbrace{\langle x_1 x'_1 \rangle}_{-\alpha_1 \epsilon_1} + \beta_0 \underbrace{\langle x'_1^2 \rangle}_{\frac{(1+\alpha_1^2)}{\beta_1} \epsilon_1}$$

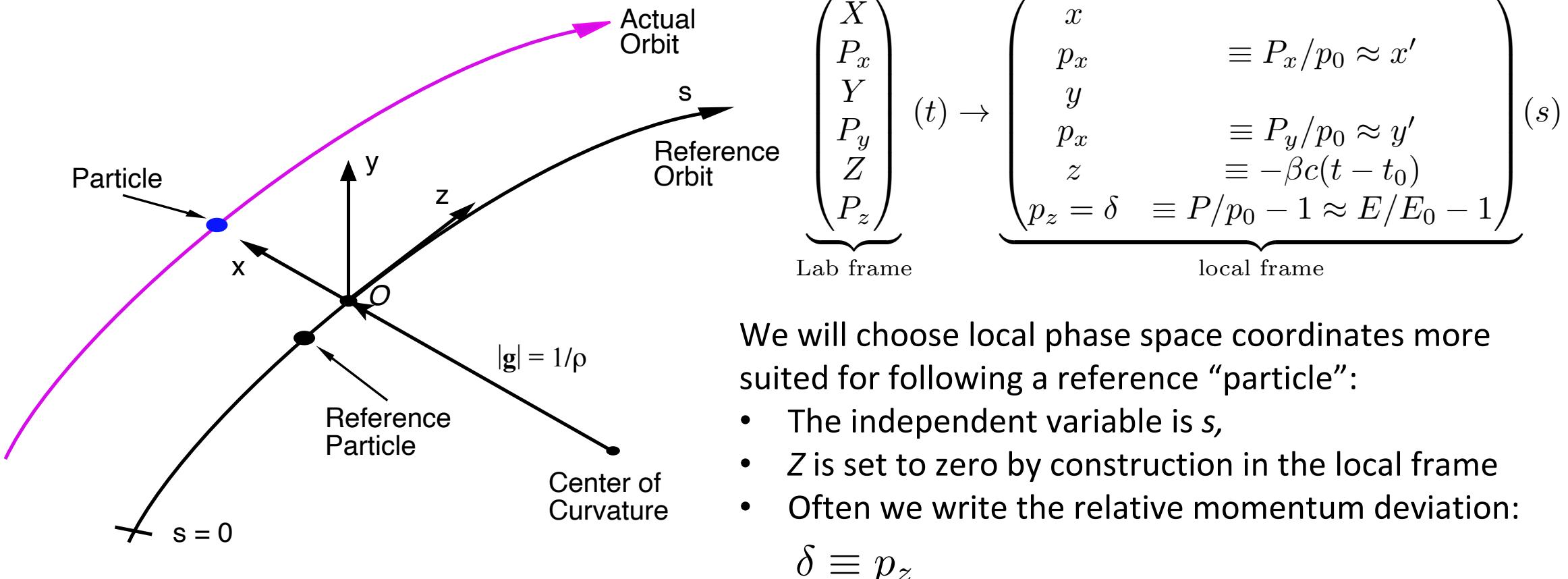
$$\implies B_{\text{mag}} = \frac{\langle J_1 \rangle}{\epsilon_1} = \frac{1}{2} \left( \frac{\beta_1}{\beta_0} + \frac{\beta_0}{\beta_1} + \beta_0 \beta_1 \left( \frac{\alpha_1}{\beta_1} - \frac{\alpha_0}{\beta_0} \right)^2 \right)$$



# Normalized Coordinates, Mismatched



# 6D Phase Space Coordinates



We will choose local phase space coordinates more suited for following a reference “particle”:

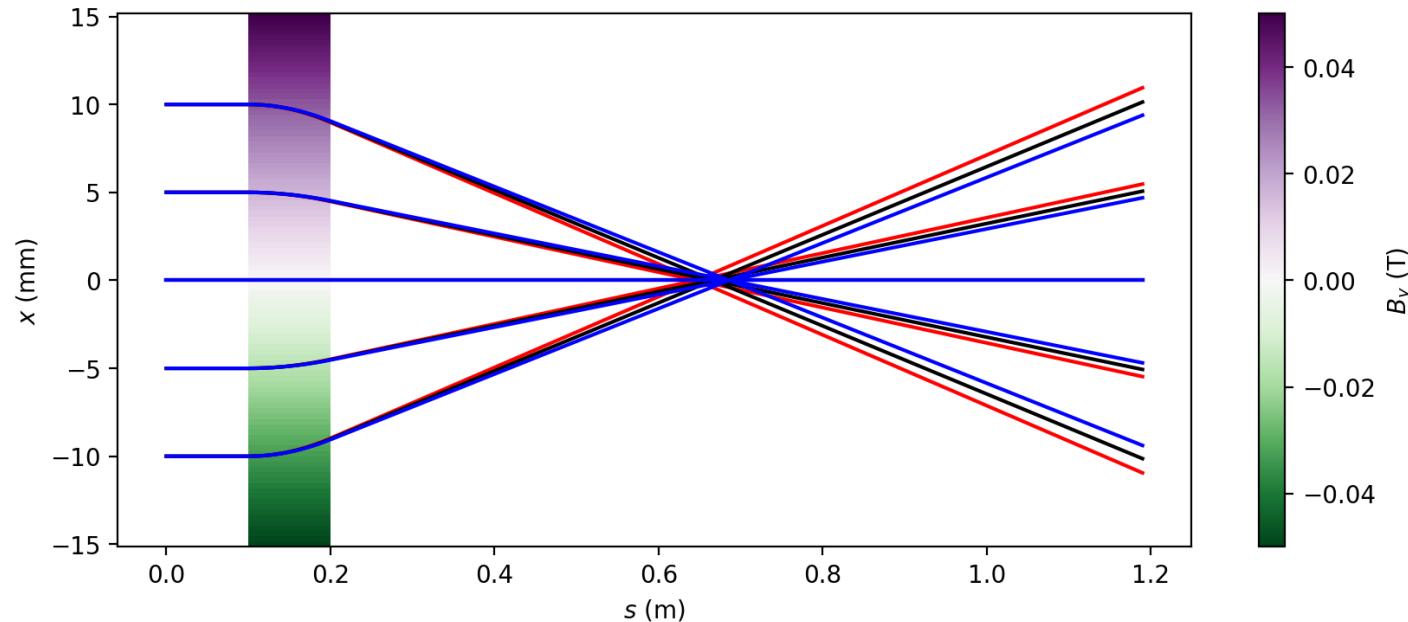
- The independent variable is  $s$ ,
- $Z$  is set to zero by construction in the local frame
- Often we write the relative momentum deviation:  
 $\delta \equiv p_z$

Note that there are many conventions used. This is the convention used by *Bmad*.

# 6D Thick Quadrupole Map

In these coordinates, the body field of a quadrupole (neglecting the fringe fields) has a well-known analytic solution.

Here we see that the map varies with the momentum deviation (“chromatic”), red = -4%, blue = +4%:



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CHAPTER 24. TRACKING OF CHARGED PARTICLES

The Hamiltonian for an upright quadrupole is

$$H = \frac{p_x^2 + p_y^2}{2(1 + p_z)} + \frac{k_1}{2}(x^2 - y^2) \quad (24.102)$$

This is simply solved

$$\begin{aligned} x_2 &= c_x x_1 + s_x \frac{p_{z1}}{1 + p_{z1}} \\ p_{x2} &= \tau_x \omega^2 (1 + p_{z1}) s_x x_1 + c_x p_{x1} \\ y_2 &= c_y y_1 + s_y \frac{p_{y1}}{1 + p_{z1}} \\ p_{y2} &= \tau_y \omega^2 (1 + p_{z1}) s_y y_1 + c_y p_{y1} \\ z_2 &= z_1 + m_{511} x_1^2 + m_{512} x_1 p_{x1} + m_{522} p_{x1}^2 + m_{533} y_1^2 + m_{534} y_1 p_{y1} + m_{544} p_{y1}^2 \\ p_{z2} &= p_{z1} \end{aligned} \quad (24.103)$$

where

$$\omega \equiv \sqrt{\frac{|k_1|}{1 + p_{z1}}} \quad (24.104)$$

and

$$\begin{array}{ll} k_1 > 0 & k_1 < 0 \\ c_x = \cos(\omega L) & \cosh(\omega L) \\ s_x = \frac{\sin(\omega L)}{\omega} & \frac{\sinh(\omega L)}{\omega} \\ \tau_x = -1 & +1 \\ & \end{array} \quad \begin{array}{ll} k_1 > 0 & k_1 < 0 \\ c_y = \cosh(\omega L) & \cos(\omega L) \\ s_y = \frac{\sinh(\omega L)}{\omega} & \frac{\sin(\omega L)}{\omega} \\ \tau_y = +1 & -1 \end{array} \quad (24.105)$$

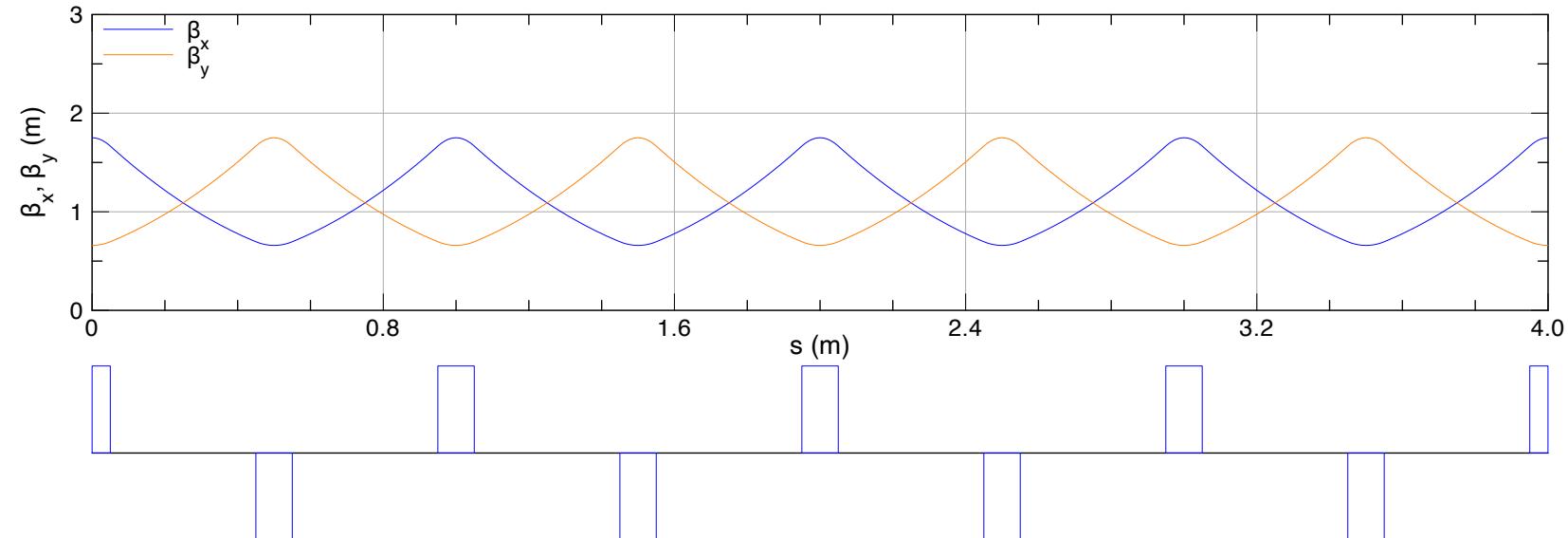
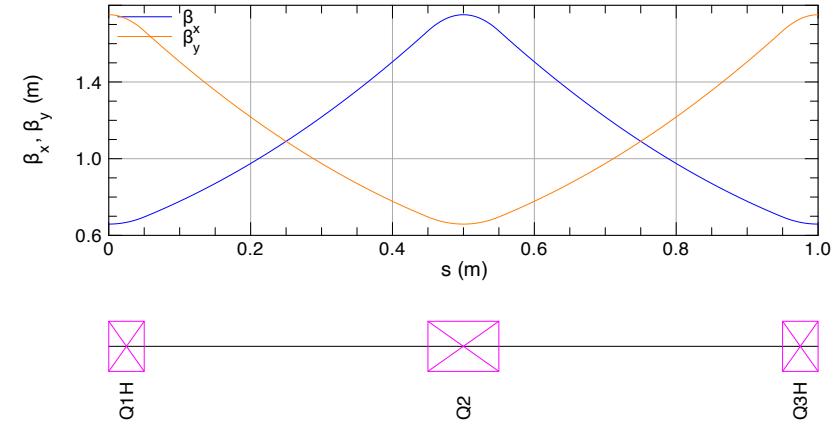
with this

$$\begin{array}{ll} m_{511} = \frac{\tau_x \omega^2}{4} (L - c_x s_x) & m_{533} = \frac{\tau_y \omega^2}{4} (L - c_y s_y) \\ m_{512} = \frac{-\tau_x \omega^2}{2(1 + p_{z1})} s_x^2 & m_{534} = \frac{-\tau_y \omega^2}{2(1 + p_{z1})} s_y^2 \\ m_{522} = \frac{-1}{4(1 + p_{z1})^2} (L + c_x s_x) & m_{544} = \frac{-1}{4(1 + p_{z1})^2} (L + c_y s_y) \end{array} \quad (24.106)$$

# FODO Cell and Lattice

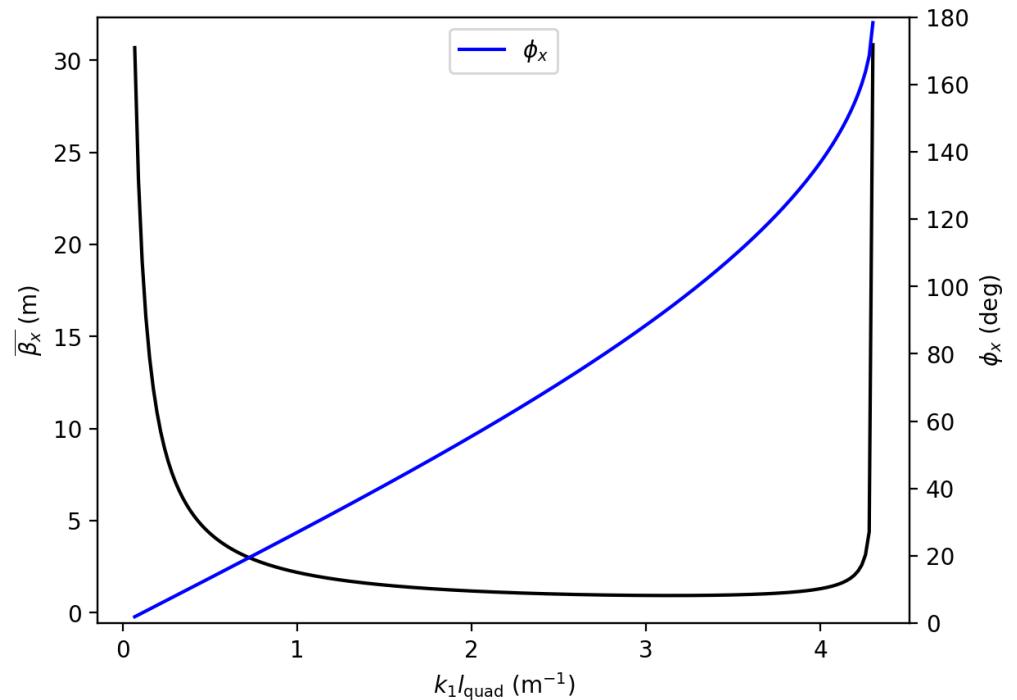
A system consisting of equally spaced quadrupole magnets with alternating field strengths is called a **FODO lattice** (“focusing, defocusing”).

A system with a single period is called a **FODO cell**. Because of the periodicity, the cell could be defined to start anywhere, and repeated cells will yield periodic beta functions.



# FODO Stability

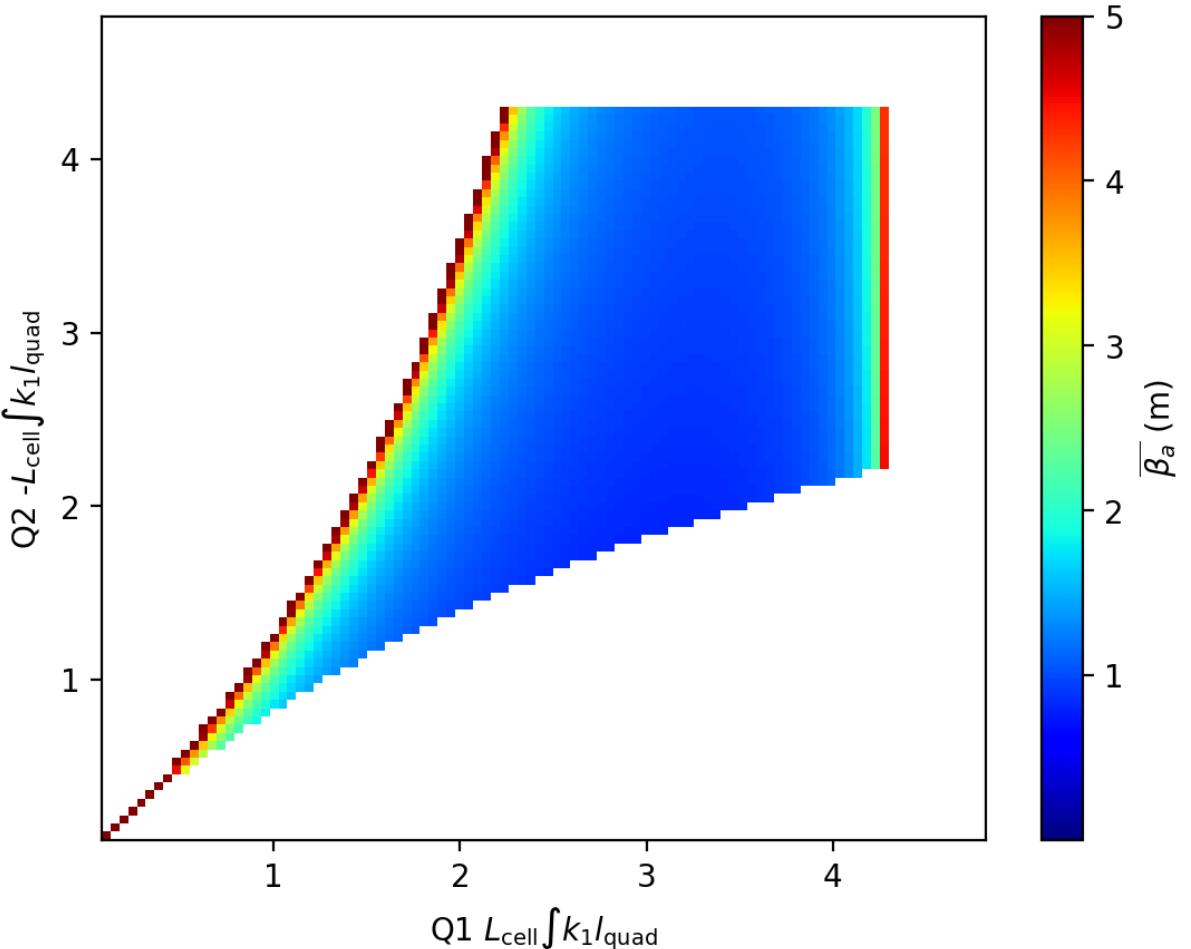
Scanning the focusing strength reveals average beta functions and stability for this **thick quad** system:



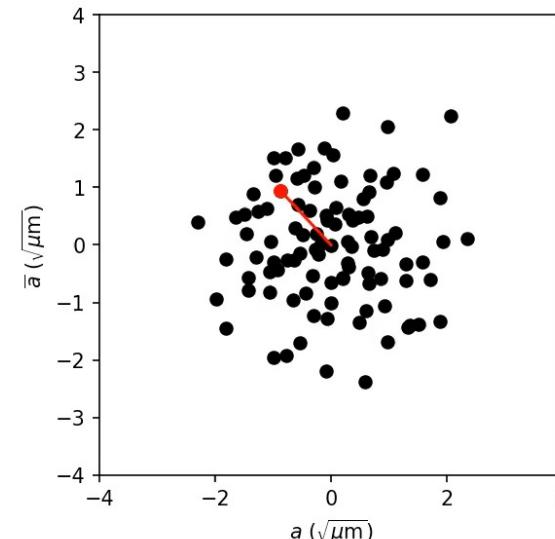
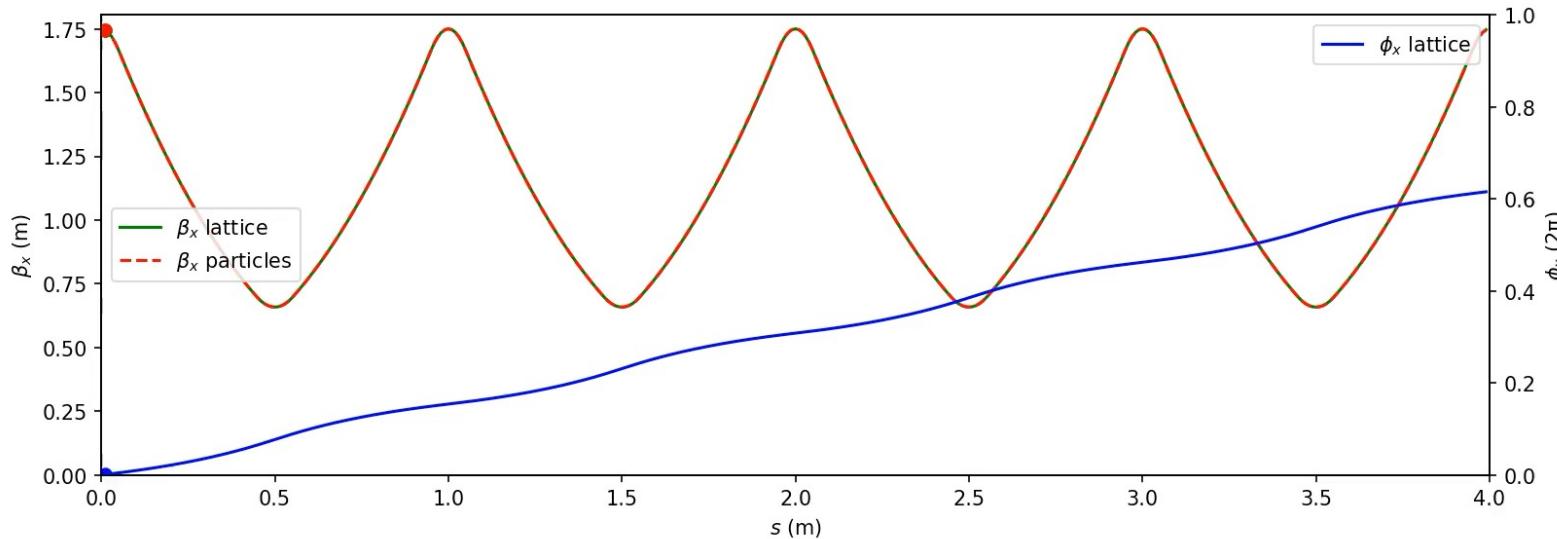
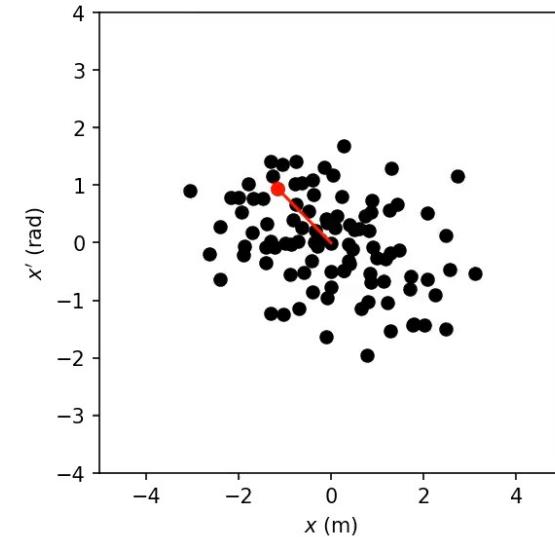
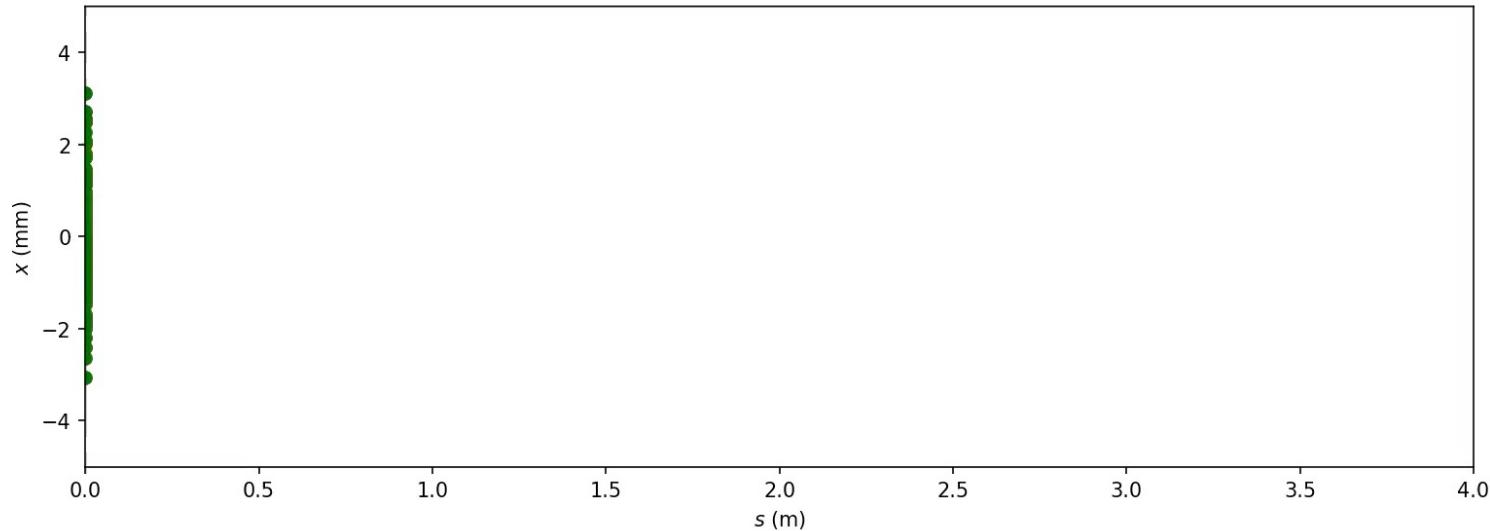
Generally, there are stable solutions when:

$$\int k_1(s) ds \lesssim 4/L_{\text{cell}}$$

2D stability “necktie” plot



# FODO tracking



# References

This formalism was originally developed in

E. Courant & H. Snyder, Theory of the alternating-gradient synchrotron, Annals of Physics Volume 3, Issue 1 (1958)

It is now a sophisticated subject, and things become much more complicated when considering 4D and 6D coupled transport. See, for example:

- D. Sagan and D. Rubin, Linear analysis of coupled Lattices, PRAB 074001 (1999)
- A. Wolski, Alternative approach to general coupled linear optics, PRAB 024001 (2006)
- P. Nishikawa, De Moivre's formula: are Sands'H-functions the same as Chao's, JINST 7 P07012 (2012)

Practically we need to use numerical methods and computer simulations, many of which are described in

- D. Sagan, *Bmad Manual* ([online](#)) (continuously updated)

Also see these standard reference books:

- Forest, Etienne. *Beam Dynamics: A New Attitude and Framework*. Harwood Academic Publishers, 1998.
- Wiedemann, Helmut. *Particle Accelerator Physics*. 3rd ed., Springer, 2007.
- Wille, Klaus. *The Physics of Particle Accelerators: An Introduction*. Oxford: Oxford University Press, 2000.