## **Practical Lattice Design**

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#### Marion Vanwelde



#### USPAS - July, 15-19, 2024

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## Purpose of the Course



- Gain a deeper understanding of the basic concepts of linear optics
- Develop intuition concerning optics functions and their manipulation
- Acquire familiarity with a modern optics design tool - Xsuite in Python Jupyther notebooks.
- Experiment with a variety of case studies

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## **Content and Structure**

|     | 9:00-12:00   | 13:30-16:30                               |                          | 19:00-21:00              |
|-----|--|---|--------------------------|--------------------------|
| Mon | L1 'Introduction to Transverse<br>Optics' (A)          | 'Introduction to Xs<br>'FODO Lattice' (M) | uite' (C)                | Homework<br>and Tuoring  |
| Tue | L2 'Dispersion Suppressor' (A)                         | 'Arc-to-Straight Des                      | ign' (C)                 | Homework<br>and Tutoring |
| Wed | L3 'Low β Optics' (C) 'IR design'                      | (C) L4 'Coupled La                        | ttices' <mark>(M)</mark> | Homework<br>and Tutoring |
| Thu | L5 'Radiation Damping - Low<br>Emittance Lattices' (A) | 'DBA, TME and FM<br>Optics' (A)           | С                        | Homework<br>and Tutoring |
| Fri | Final Exam (9:00-13:00)                                |   |                          |                          |
|     |  | A - Alex Bogacz                           |                          |                          |
|     |  |   | C - Cedric Hernalsteens  |                          |
|     |  |   | M - Marion               | Vanwelde                 |
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## Some references

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- 2. Andrzej Wolski, *Beam Dynamics in High Energy Particle Accelerators*, Imperial College Press, 2014
- The CERN Accelerator School (CAS) Proceedings, e.g. 1992, Jyväskylä, Finland; or 2013, Trondheim, Norway
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## Introduction to Transverse Optics

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USPAS - July, 15-19, 2024

#### Part 1

## Basics, single-particle dynamics

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### Relativistic beams - 'Big picture'

In a typical **storage ring** particles are accelerated and stored for  $\sim 12-15$  hours. The distance traveled by particles moving at nearly the speed of light,  $v \approx c$ , for 12 hours is:

#### $\approx 3\times 10^{10}\,\text{km}$

 $\rightarrow$  This is about the distance from Sun to Pluto and back!

Challenge: How to maintain them in a few millimiter wide beam-pipe?



### Forces and fields

Four fundamental interactions in Nature, the electromagnetic one is the most promising→the Lorentz force

$$\vec{F} = q \cdot \left(\vec{E} + \vec{v} \times \vec{B}\right)$$

where, in high energy machines,  $|\vec{v}| \approx c \approx 3 \cdot 10^8$  m/s. Usually there is no electric field, and the transverse deflection is given by a magnetic field only.





Stable circular motion: centrifugal force + centripetal force = 0

 $\left. \begin{array}{lll} \text{Lorentz force} & F_L & = qvB \\ \text{Centripetal force} & F_{\text{centr}} & = \frac{mv^2}{\rho} \\ & \frac{mv_{\rho}^4}{\rho} & = q \not \! / B \end{array} \right\}$ 

$$P = mv = m_0 \gamma v$$
 "momentum"  
 $B\rho =$  "beam ridigity"

$$\frac{P}{q} = \mathsf{B}\rho$$

#### The gutter analogy

$$\vec{F} = q \cdot \left(\vec{E} + \vec{v} \times \vec{B}\right)$$



Remember the 1d harmonic oscillator: F = -kx

## Dipole magnets: the magnetic guide

Rule of thumb, in practical units:

$$\frac{1}{\rho \ [m]} \approx 0.3 \frac{B \ [T]}{P \ [GeV/c]}$$

Example: In the LHC,  $\rho = 2.53$  km. The circumference  $2\pi\rho = 15.9$  km  $\approx 60\%$  of the entire LHC. (R = 4.3 km, and the total circumference is  $C = 2\pi R \approx 27$  km)

The field *B* is  $\approx 1 \dots 8$  T

The quantity  $\frac{1}{\rho}$  can be seen as a "normalized bending strength", i.e. the bending field normalized to the beam rigidity.

#### Quadrupole magnets: the focusing force

Quadrupole magnets are required to keep the trajectories in vicinity of the ideal orbit They exert a linearly-increasing Lorentz force, thru a linearly-increasing magnetic field:

$$B_{x} = gy \qquad \Rightarrow F_{x} = -qv_{z}B_{y} = -qv_{z}gx$$
$$\Rightarrow F_{y} = qv_{z}B_{x} = qv_{z}gy$$

Gradient of a quadrupole magnet:

$$g = \frac{2\mu_0 n I}{r_{\text{aperture}}^2} \left[\frac{T}{m}\right] = \frac{B_{\text{poles}}}{r_{\text{aperture}}} \left[\frac{T}{m}\right]$$

► LHC main quadrupole magnets:  $g \approx 25...235$ T/m



the arrows show the force exerted on a particle

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Dividing by p/q one finds k, the "normalized focusing strength"

$$k = \frac{g}{P/q} [m^{-2}] \quad \Rightarrow \quad g = \left[\frac{T}{m}\right]; \quad q = [e]; \quad \frac{P}{q} = \left[\frac{\text{GeV}}{\text{c} \cdot e}\right] = \left[\frac{GV}{c}\right] = [T m]$$

Another useful rule of thumb:  $k [m^{-2}] \approx 0.3 \frac{g [T/m]}{P/q [GeV/c/c]}$ 

## Focal length of a quadrupole

The focal length of a quadrupole is  $f = \frac{1}{k \cdot L}$  [m], where *L* is the quadrupole length:



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## Reminder: the 1d Harmonic oscillator

Restoring force

$$F = -kx$$

Equation of motion:

$$x'' = -\frac{k}{m}x$$

 $x(t) = A\cos(\omega t + \phi) = a_1\cos(\omega t) + a_2\sin(\omega t)$ 

which has solution:



- F , restoring force, N or MeV/m
- k, spring constant or focusing strength, N/m or MeV/m<sup>2</sup>
- $\omega = \sqrt{\frac{k}{m}} = 2\pi f$ , angular velocity, rad/s •  $\phi$ , initial phase, rad A.

- f, rotation frequency, Hz
- A, oscillation amplitude, m
- ▶ m<sub>0</sub>, particle's rest mass, MeV/c<sup>2</sup>
- $m = m_0 \gamma$ , particle's mass, MeV/c<sup>2</sup>

#### Phase-space coordinates



- the ideal particle coincides with the reference orbit (perfect machine) or closed orbit (real machine)
- any other particle  $\Rightarrow$  has coordinates

$$x, y, P_x, P_y \neq 0; P \neq P_0$$
 with

• 
$$x, y \ll \rho$$

 $(x, x', y, y', z, \delta)$ 

y

► 
$$P_x$$
,  $P_y \ll P_0$ 

The state of a particle is represented with a 6-dimensional phase-space vector:



 $P_0$  is the reference momentum and  $P = P_0 (1 + \delta)$ 

$$x' = \frac{\mathrm{d}x}{\mathrm{d}s} = \frac{\mathrm{d}x}{\mathrm{d}t}\frac{\mathrm{d}t}{\mathrm{d}s} = \frac{V_x}{V_z} = \frac{P_x}{P_z} \approx \frac{P_x}{P_0} \qquad [\mathrm{rad}]$$

$$y' = \frac{dy}{ds} = \frac{dy}{dt}\frac{dt}{ds} = \frac{V_y}{V_z} = \frac{P_y}{P_z} \approx \frac{P_y}{P_0}$$
 [rad]

$$\delta = \frac{\Delta P}{P_0} = \frac{P - P_0}{P_0} \tag{#}$$

#### The equation of motion

$$x''(s) + \underbrace{\left(\frac{1}{\rho^2} + k\right)}_{\text{focusing effect}} x(s) = 0$$

there is a focusing force,  $\frac{1}{a^2}$ , even without a quadrupole gradient,

$$k = 0 \quad \Rightarrow \quad x'' = -\frac{1}{\rho^2}x$$

even without quadrupoles there is retrieving force (focusing) in the bending plane of the dipole magnets

In large machines, this effect is very weak.



#### Solution of the trajectory equations

Definition:

horizontal plane  $K = 1/\rho^2 + k$ vertical plane K = -k x'' + Kx = 0

This is the differential equation of a 1d harmonic oscillator with spring constant K. We know that, for K > 0, the solution is in the form:

$$x\left(s
ight)=a_{1}\cos\left(\omega s
ight)+a_{2}\sin\left(\omega s
ight)$$

In fact,

$$\begin{aligned} x'(s) &= -a_1\omega\sin(\omega s) + a_2\omega\cos(\omega s) \\ x''(s) &= -a_1\omega^2\cos(\omega s) + a_2\omega^2\sin(\omega s) = -\omega^2x(s) \quad \to \quad \omega = \sqrt{\kappa} \end{aligned}$$

Thus, the general solution is

$$x(s) = a_1 \cos\left(\sqrt{\kappa}s\right) + a_2 \sin\left(\sqrt{\kappa}s\right)$$

for K > 0.

We determine  $a_1$ ,  $a_2$  by imposing the initial conditions:

$$s = 0 \quad \rightarrow \quad \begin{cases} x(0) = x_0, & a_1 = x_0 \\ x'(0) = x'_0, & a_2 = \frac{x'_0}{\sqrt{K}} \end{cases}$$

Horizontal focusing quadrupole, K > 0:

$$x(s) = x_0 \cos\left(\sqrt{K}s\right) + x'_0 \frac{1}{\sqrt{K}} \sin\left(\sqrt{K}s\right)$$
$$x'(s) = -x_0 \sqrt{K} \sin\left(\sqrt{K}s\right) + x'_0 \cos\left(\sqrt{K}s\right)$$

We can use the matrix formalism:



For a quadrupole of length L:

$$M_{\rm foc} = \begin{pmatrix} \cos\left(\sqrt{K}L\right) & \frac{1}{\sqrt{K}}\sin\left(\sqrt{K}L\right) \\ -\sqrt{K}\sin\left(\sqrt{K}L\right) & \cos\left(\sqrt{K}L\right) \end{pmatrix}$$

 $\left(\begin{array}{cc}1 & L\\ 0 & 1\end{array}\right).$ 

Notice that for a drift space, i.e. when  $K = 0 \rightarrow M_{drift} =$ A. Bogacz - Introduction to Transverse Optics

## Defocusing quadrupole

The equation of motion is

with

$$x'' + Kx = 0$$
$$K < 0$$



The solution is in the form:

$$x(s) = a_1 \cosh(\omega s) + a_2 \sinh(\omega s)$$

with  $\omega = \sqrt{|K|}$ . For a quadrupole of length L the transfer matrix reads:

$$M_{\rm defoc} = \begin{pmatrix} \cosh\left(\sqrt{|K|}L\right) & \frac{1}{\sqrt{|K|}}\sinh\left(\sqrt{|K|}L\right) \\ \sqrt{|K|}\sinh\left(\sqrt{|K|}L\right) & \cosh\left(\sqrt{|K|}L\right) \end{pmatrix}$$
  
Again when  $K = 0 \rightarrow M_{\rm drift} = \begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix}$ 

#### Thin-lens approximation of a quadrupole magnet

When the focal length f of the quadrupolar lens is much bigger than the length of the magnet itself,  $L_Q$ 

$$f = \frac{1}{k \cdot L_Q} \qquad \gg L_Q$$

we can derive the limit for  $L \rightarrow 0$  while keeping constant f, i.e.  $k \cdot L_Q = \text{const.}$ 

The transfer matrices are

$$M_{x} = \begin{pmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{pmatrix} \qquad M_{y} = \begin{pmatrix} 1 & 0 \\ \frac{1}{f} & 1 \end{pmatrix}$$

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focusing, and defocusing respectively.

This approximation is useful for fast calculations.

#### Transformation through a system of lattice elements

One can compute the solution of a system of elements, by multiplying the matrices of each single element:

$$M_{\text{total}} = M_{\text{QF}} \cdot M_{\text{D}} \cdot M_{\text{Bend}} \cdot M_{\text{D}} \cdot M_{\text{QD}} \cdot \cdots$$

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_2} = M_{s_1 \to s_2} \cdot M_{s_0 \to s_1} \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$

$$(M_{\text{total}} = M_{s_1 \to s_2} \cdot M_{s_0 \to s_1} \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$

$$(M_{\text{total}} = M_{s_1 \to s_2} \cdot M_{s_0 \to s_1} \cdot \begin{pmatrix} x \\ x' \end{pmatrix}_{s_0}$$

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In each accelerator element the particle trajectory corresponds to the movement of a harmonic oscillator.



### Properties of the transfer matrix M

The transfer matrix M has two important properties:

Its determinant is 1 (Liouville's theorem)

 $\det(M) = 1$ 

(symplecticity condition for the 2D case)

▶ Provides a stable motion over N turns, with  $N \rightarrow \infty$ , if and only if:

trace (M)  $\leq 2$ 

(Stability condition)

#### Orbit and tune

Tune: the number of oscillations per turn.



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The non-integer part is crucial!

## Summary

$$\begin{aligned} & \text{beam rigidity:} \quad B\rho = \frac{p}{q} \\ & \text{bending strength of a dipole:} \quad \frac{1}{\rho} \left[ m^{-1} \right] = \frac{0.2998 \cdot B_0 \left[ T \right]}{P \left[ \text{GeV/c} \right]} \\ & \text{focusing strength of a quadruple:} \quad k \left[ m^{-2} \right] = \frac{0.2998 \cdot g}{P \left[ \text{GeV/c} \right]} \\ & \text{focal length of a quadrupole:} \quad f = \frac{1}{k \cdot L_Q} \\ & \text{equation of motion:} \quad x'' + \left( \frac{1}{\rho^2} + k \right) x = 0 \\ & \text{solution of the eq. of motion:} \quad x_{s_2} = M \cdot x_{s_1} \qquad \dots \text{ with } M \equiv \left( \begin{array}{c} C & S \\ C' & S' \end{array} \right) \\ & \text{e.g.:} \quad M_{\text{QF}} = \left( \begin{array}{c} \cos\left(\sqrt{K}L\right) & \frac{1}{\sqrt{K}}\sin\left(\sqrt{K}L\right) \\ -\sqrt{K}\sin\left(\sqrt{K}L\right) & \cos\left(\sqrt{K}L\right) \end{array} \right) \text{ Thin Lense} \rightarrow \left( \begin{array}{c} 1 & 0 \\ -\frac{1}{f} & 1 \end{array} \right), \\ & M_{\text{QD}} = \left( \begin{array}{c} \cosh\left(\sqrt{|K|}L\right) & \frac{1}{\sqrt{|K|}}\sinh\left(\sqrt{|K|}L\right) \\ \sqrt{|K|}\sinh\left(\sqrt{|K|}L\right) & \cosh\left(\sqrt{|K|}L\right) \end{array} \right), \quad M_{\text{D}} = \left( \begin{array}{c} 1 & L \\ 0 & 1 \end{array} \right) \end{aligned}$$

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#### Part 2

# Optics functions and Twiss parameters

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## Envelope

So far we have studied the motion of a particle.

Question: what will happen, if the particle performs a second turn ?

 $\blacktriangleright$  ... or a third one or ...  $10^{10}$  turns ...



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## The Hill's equation

In 19th century George William Hill, one of the greatest masters of celestial mechanics of his time, studied the differential equation for "motions with periodic focusing properties": the "Hill's equation"

$$x''(s) + K(s)x(s) = 0$$

with:

- ▶ a restoring force  $\neq$  const
- K(s) depends on the position s
- K(s + L) = K(s) periodic function, where L is the "lattice period"

We expect a solution in the form of a quasi harmonic oscillation: amplitude and phase will depend on the position *s* in the ring.

#### The beta function

General solution of Hill's equation:

$$x(s) = \sqrt{\beta_x(s) J_x} \cos(\mu_x(s) + \mu_{x,0})$$
(1)

 $J_x$ ,  $\mu_0$  =integration constants determined by initial conditions

 $\beta_x$  (s) is a periodic function given by the focusing properties of the lattice  $\leftrightarrow$  quadrupoles  $\beta_x$  (s + L) =  $\beta_x$  (s)

Inserting Eq. (1) in the equation of motion, we get (Floquet's theorem) the following result

$$\mu_{x}(s) = \int_{0}^{s} \frac{\mathrm{d}s}{\beta_{x}(s)}$$

where  $\mu_{\chi}(s)$  is the "phase advance" between the points 0 and s, in the phase space.

For one complete revolution,  $\mu_x(s)$  is the number of oscillations per turn, or "tune" when normalized to  $2\pi$ 

$$Q_{x}=\frac{1}{2\pi}\oint\frac{\mathrm{d}s}{\beta_{x}\left(s\right)}$$

 $J_x$  is a constant of motion, called the Courant-Snyder invariant or "action".

#### The orbit in the phase space is an ellipse

General solution of the Hill's equation

$$x(s) = \sqrt{\beta_x(s)} J_x \cos(\mu_x(s) + \mu_{x,0})$$
(1)

$$x'(s) = -\frac{\sqrt{J_x}}{\sqrt{\beta_x(s)}} \{ \alpha_x(s) \cos(\mu_x(s) + \mu_{x,0}) + \sin(\mu_x(s) + \mu_{x,0}) \}$$
(2)

From Eq. (1) we get

$$\cos(\mu(s) + \mu_0) = \frac{x(s)}{\sqrt{J_x}\sqrt{\beta_x(s)}} \qquad \qquad \alpha_x(s) = -\frac{1}{2}\beta'_x(s)$$
$$\gamma_x(s) = \frac{1 + \alpha_x(s)^2}{\beta_x(s)}$$

Insert into Eq. (2) and solve for J

$$J_{x} = \gamma_{x}(s) x (s)^{2} + 2\alpha_{x}(s) x (s) x' (s) + \beta_{x}(s) x' (s)^{2}$$

- $\blacktriangleright$   $J_x$  is a constant of the motion, i.e. the Courant-Snyder invariant or Action
- ▶ it is a parametric representation of an ellipse in the xx' space
- ▶ the shape and the orientation of the ellipse are given by  $\alpha_x$ ,  $\beta_x$ , and  $\gamma_x \Rightarrow$  these are the Twiss parameters
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#### The phase-space ellipse



The area of ellipse,  $\pi \cdot J_x$ , is an intrinsic beam parameter and cannot be changed by the focal properties.

Important remarks:

- A large  $\beta$ -function corresponds to a large beam size and a small beam divergence
- wherever  $\beta$  reaches a maximum or a minimum,  $\alpha = 0$ .

#### Particles distribution and beam ellipse

For each turn x, x' at a given position  $s_1$  and plot in the phase-space diagram



Plane: x - x'

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### Particles distribution and beam matrix

In the phase space a realistic particles distribution matches the shape of an ellipse, and can be described using a "beam matrix"  $\Sigma$ 

Where  $\Sigma$  is defined as

$$\Sigma = \begin{pmatrix} \sigma_{11} & \sigma_{12} \\ \sigma_{21} & \sigma_{22} \end{pmatrix} = \begin{pmatrix} \langle x^2 \rangle & \langle xx' \rangle \\ \langle x'x \rangle & \langle x'^2 \rangle \end{pmatrix}$$

the covariance matrix of the particles distribution



The determinant of the covariance matrix of a distribution, can be used to define the geometric emittance, corresponding to the area of the distribution

$$\epsilon = \sqrt{\det \Sigma} = \sqrt{\det \left( \operatorname{cov}(\mathbf{x}, \mathbf{x}') \right)} = \sqrt{\sigma_{11}\sigma_{22} - \sigma_{12}\sigma_{21}} = \text{area of the beam ellipse}$$

Remember: when accelerating the beam the preserved quantity is the normalised emittance:

$$\epsilon_{\textit{normalized}} \stackrel{\text{def}}{=} \beta_{\text{rel}} \cdot \gamma_{\text{rel}} \cdot \epsilon_{\text{geometric}}$$

#### The transfer matrix in terms of Twiss parameters

As we have already seen, a general solution of the Hill's equation is:

$$\begin{aligned} x(s) &= \sqrt{\beta_{x}(s) J_{x}} \cos(\mu_{x}(s) + \mu_{x,0}) \\ x'(s) &= -\sqrt{\frac{J_{x}}{\beta_{x}(s)}} \left[ \alpha_{x}(s) \cos(\mu_{x}(s) + \mu_{x,0}) + \sin(\mu_{x}(s) + \mu_{x,0}) \right] \end{aligned}$$

Let's remember some trigonometric formulæ:

 $sin (a \pm b) = sin a cos b \pm cos a sin b,$  $cos (a \pm b) = cos a cos b \mp sin a sin b, ...$ 

then,

$$\begin{aligned} x(s) &= \sqrt{\beta_x(s) J_x} \left( \cos \mu_x(s) \cos \mu_{x,0} - \sin \mu_x(s) \sin \mu_{x,0} \right) \\ x'(s) &= -\sqrt{\frac{J_x}{\beta_x(s)}} \left[ \alpha_x(s) \left( \cos \mu_x(s) \cos \mu_{x,0} - \sin \mu_x(s) \sin \mu_{x,0} \right) + \\ &+ \sin \mu_x(s) \cos \mu_{x,0} + \cos \mu_x(s) \sin \mu_{x,0} \right] \end{aligned}$$

At the starting point,  $s(0) = s_0$ , we put  $\mu(0) = 0$ . Therefore we have

$$\begin{aligned} \cos \mu_0 &= \frac{x_0}{\sqrt{\beta_0 J}}\\ \sin \mu_0 &= -\frac{1}{\sqrt{J}} \left( x_0' \sqrt{\beta_0} + \frac{\alpha_0 x_0}{\sqrt{\beta_0}} \right) \end{aligned}$$

If we replace this in the formulæ, we obtain:

$$\underline{x(s)} = \sqrt{\frac{\beta_s}{\beta_0}} \left\{ \cos \mu_s + \alpha_0 \sin \mu_s \right\} \underline{x_0} + \left\{ \sqrt{\beta_s \beta_0} \sin \mu_s \right\} \underline{x_0'}$$
$$\underline{x'(s)} = \frac{1}{\sqrt{\beta_s \beta_0}} \left\{ (\alpha_0 - \alpha_s) \cos \mu_s - (1 + \alpha_0 \alpha_s) \sin \mu_s \right\} \underline{x_0} + \sqrt{\frac{\beta_0}{\beta_s}} \left\{ \cos \mu_s - \alpha_s \sin \mu_s \right\} \underline{x_0'}$$

The linear map follows easily,

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s} = M \begin{pmatrix} x \\ x' \end{pmatrix}_{0} \rightarrow M = \begin{pmatrix} \sqrt{\frac{\beta_{s}}{\beta_{0}}} (\cos \mu_{s} + \alpha_{0} \sin \mu_{s}) & \sqrt{\beta_{s}\beta_{0}} \sin \mu_{s} \\ \frac{(\alpha_{0} - \alpha_{s}) \cos \mu_{s} - (1 + \alpha_{0}\alpha_{s}) \sin \mu_{s}}{\sqrt{\beta_{s}\beta_{0}}} & \sqrt{\frac{\beta_{0}}{\beta_{s}}} (\cos \mu_{s} - \alpha_{s} \sin \mu_{s}) \end{pmatrix}$$

We can compute the single particle trajectories between two locations in the ring, if we know the α, β, and γ at these positions!

Exercise: prove that det(M) = 1

### Periodic lattices, 1-turn map

The transfer matrix for a particle trajectory

$$M_{0\to s} = \begin{pmatrix} \sqrt{\frac{\beta_s}{\beta_0}} \left( \cos \mu_s + \alpha_0 \sin \mu_s \right) & \sqrt{\beta_s \beta_0} \sin \mu_s \\ \frac{(\alpha_0 - \alpha_s) \cos \mu_s - (1 + \alpha_0 \alpha_s) \sin \mu_s}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta_s}} \left( \cos \mu_s - \alpha_s \sin \mu_s \right) \end{pmatrix}$$

simplifies considerably if we consider one complete turn:



$$M = \begin{pmatrix} \cos \mu_L + \alpha_s \sin \mu_L & \beta_s \sin \mu_L \\ -\gamma_s \sin \mu_L & \cos \mu_L - \alpha_s \sin \mu_L \end{pmatrix}$$

where  $\mu_L$  is the phase advance per period

$$u_{L} = \int_{s}^{s+L} \frac{\mathrm{d}s}{\beta(s)}$$

Remember: the tune is the phase advance in units of  $2\pi$ :

$$Q = \frac{1}{2\pi} \oint \frac{\mathrm{d}s}{\beta(s)} = \frac{\mu_L}{2\pi}$$

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#### Evolution of $\alpha$ , $\beta$ , and $\gamma$ Consider

two positions in the storage ring:  $s_0$ , s

$$M = M_{\rm QF} \cdot M_{\rm D} \cdot M_{\rm Bend} \cdot M_{\rm D} \cdot M_{\rm QD} \cdot \cdots$$

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s} = M \begin{pmatrix} x \\ x' \end{pmatrix}_{s_{0}} \text{ with}$$
$$M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix} \qquad M^{-1} = \begin{pmatrix} S' & -S \\ -C' & C \end{pmatrix}$$

Since the Liouville theorem holds, J = const:

$$J = \beta x'^{2} + 2\alpha x x' + \gamma x^{2}$$
$$J = \beta_{0} x_{0}'^{2} + 2\alpha_{0} x_{0} x_{0}' + \gamma_{0} x_{0}^{2}$$

We express  $x_0$  and  $x'_0$  as a function of x and x':

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{s_0} = M^{-1} \begin{pmatrix} x \\ x' \end{pmatrix}_s \quad \Rightarrow \quad \begin{array}{c} x_0 = S'x - Sx' \\ x'_0 = -C'x + Cx' \end{array}$$

Substituting  $x_0$  and  $x'_0$  into the expression of *J*, we obtain:

$$J = \beta x'^{2} + 2\alpha xx' + \gamma x^{2}$$
  
$$J = \beta_{0} \left( -C'x + Cx' \right)^{2} + 2\alpha_{0} \left( S'x - Sx' \right) \left( -C'x + Cx' \right) + \gamma_{0} \left( S'x - Sx' \right)^{2}$$

We need to sort by x and x':

$$\beta (s) = C^2 \beta_0 - 2SC \alpha_0 + S^2 \gamma_0$$
  

$$\alpha (s) = -CC' \beta_0 + (SC' + S'C) \alpha_0 - SS' \gamma_0$$
  

$$\gamma (s) = C'^2 \beta_0 - 2S'C' \alpha_0 + S'^2 \gamma_0$$

## Evolution of $\alpha$ , $\beta$ , and $\gamma$ in matrix form

The beam ellipse transformation in matrix notation:

$$T_{0\to s} = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC' + S'C & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix}$$
$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = T_{0\to s} \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0$$

This expression is important, and useful:

- 1. given the twiss parameters  $\alpha$ ,  $\beta$ ,  $\gamma$  at any point in the lattice we can transform them and compute their values at any other point in the ring
- 2. the transfer matrix is given by the focusing properties of the lattice elements, the elements of M are just those that we used to compute single particle trajectories

#### Exercise: Twiss transport matrix, T

Compute the Twiss transport matrix, T,

$$T = \begin{pmatrix} C^2 & -2SC & S^2 \\ -CC' & SC' + S'C & -SS' \\ C'^2 & -2S'C' & S'^2 \end{pmatrix}$$
$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_s = T \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_0$$

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for:

- 1. the identity matrix:  $M = \pm \mathbf{I}$
- 2. a drift of length L
- 3. a thin quadrupole with focal length  $\pm f$

#### Beam ellipse evolution (another approach)

Let's write the ellipse equation:  $J = \gamma x^2 + 2\alpha x x' (s) + \beta x'^2$ in matrix form, for  $X = \begin{pmatrix} x \\ x' \end{pmatrix}$ :  $X^T \Omega^{-1} X = J$  with:  $\Omega = \begin{pmatrix} \beta & -\alpha \\ -\alpha & \gamma \end{pmatrix} = \frac{\Sigma}{\varepsilon^2}$ 

At a later point if the lattice the coordinates of an individual particle are given using the transfer matrix M from  $s_0$  to  $s_1$ :

$$X_1 = M \cdot X_0$$

Solving for  $X_0$ , i.e.  $X_0 = M^{-1} \cdot X_1$ , and inserting in  $X_0^T \Omega_0^{-1} X_0 = J$ , one obtains:

$$(M^{-1} \cdot X_1)^T \Omega_0^{-1} (M^{-1} \cdot X_1) = J$$
$$\left(X_1^T \cdot \left(M^T\right)^{-1}\right) \Omega_0^{-1} (M^{-1} \cdot X_1) = J$$
$$X_1^T \cdot \underbrace{\left(M^T\right)^{-1} \Omega_0^{-1} M^{-1}}_{\Omega_0^{-1}} \cdot X_1 = J$$

Which gives

$$\Omega_1 = M \cdot \Omega_0 \cdot M^T$$

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## Summary

Hill's equation: 
$$x''(s) + K(s)x(s) = 0$$
,  $K(s) = K(s + L)$ 

general solution of the  
Hill's equation: 
$$x(s) = \sqrt{J\beta(s)} \cos(\mu(s) + \mu_0)$$
  
phase advance & tune:  $\mu_{12} = \int_{s_1}^{s_2} \frac{ds}{\beta(s)}, \quad Q = \frac{1}{2\pi} \oint \frac{ds}{\beta(s)}$   
beam ellipse:  $J = \gamma(s) x(s)^2 + 2\alpha(s) x(s) x'(s) + \beta(s) x'(s)^2$   
beam emittance:  $\epsilon = \text{Area of the beam ellipse} = \sqrt{\det(\text{cov}(\mathbf{x}, \mathbf{x}'))}$   
transfer matrix  $s_1 \rightarrow s_2$ :  $M = \begin{pmatrix} \sqrt{\frac{\beta s}{\beta 0}} (\cos \mu_s + \alpha_0 \sin \mu_s) & \sqrt{\beta_s \beta_0} \sin \mu_s \\ \frac{(\alpha_0 - \alpha_s) \cos \mu_s - (1 + \alpha_0 \alpha_s) \sin \mu_s}{\sqrt{\beta_s \beta_0}} & \sqrt{\frac{\beta_0}{\beta_s}} (\cos \mu_s - \alpha_s \sin \mu_s) \end{pmatrix}$ 

stability criterion:  $|\text{trace}(M)| \leq 2$ 

# Summary: beam matrix, emittance, and Twiss parameters

The beam matrix is the covariance matrix of the particle distribution

$$\Sigma = \begin{pmatrix} \sigma_{11} & \sigma_{12} \\ \sigma_{21} & \sigma_{22} \end{pmatrix} = \begin{pmatrix} \langle x^2 \rangle & \langle xx' \rangle \\ \langle x'x \rangle & \langle x'^2 \rangle \end{pmatrix}$$

this matrix can be also expressed in terms of Twiss parameters  $\alpha$ ,  $\beta$ ,  $\gamma$  and of the emittance  $\epsilon$ :

$$\Sigma = \begin{pmatrix} \langle x^2 \rangle & \langle xx' \rangle \\ \langle x'x \rangle & \langle x'^2 \rangle \end{pmatrix} = \epsilon^2 \begin{pmatrix} \beta & -\alpha \\ -\alpha & \gamma \end{pmatrix}$$

• Given  $M = \begin{pmatrix} C & S \\ C' & S' \end{pmatrix}_{0 \to s}$ , we can transport the beam matrix, or the twiss parameters, from 0 to *s* in two equivalent ways:

1. Twiss  $3 \times 3$  transport matrix:

$$\left( \begin{array}{c} \beta \\ \alpha \\ \gamma \end{array} \right)_{s} = \left( \begin{array}{cc} C^{2} & -2SC & S^{2} \\ -CC' & SC' + S'C & -SS' \\ C'^{2} & -2S'C' & S'^{2} \end{array} \right) \left( \begin{array}{c} \beta \\ \alpha \\ \gamma \end{array} \right)_{0}$$

2. Recalling that  $\Sigma_s = M \Sigma_0 M^T$ :

$$\begin{pmatrix} \beta & -\alpha \\ -\alpha & \gamma \end{pmatrix}_{s} = M \cdot \begin{pmatrix} \beta & -\alpha \\ -\alpha & \gamma \end{pmatrix}_{0} \cdot M^{T}$$

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## **APPENDIX I**

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## A derivation of the equation of motion

Linear approximation:

- the ideal particle coincides with the reference orbit
- ► any other particle ⇒ has coordinates
  - $x, y, P_x, P_y \neq 0; P \neq P_0$  with
    - $x, y \ll \rho$
    - $P_x$ ,  $P_y \ll P_0$
- only linear terms in x and y of B are taken into account

![](_page_43_Picture_8.jpeg)

Let's recall some useful relativistic formulæ and definitions:

| $P_0$ | $= m_0  \gamma_0  v_0 = m_0  \gamma_0  \beta_0  c$                          | reference momentum          |
|-------|---|-----------------------------|
| Ρ     | $= P_0 \left( 1 + \delta \right)$   | total momentum              |
| δ     | $= (P - P_0) / P_0$   | relative momentum offset    |
| E     | $= \sqrt{P^2 c^2 + m_0^2 c^4} = m_0 \gamma c^2 = m_0 c^2 + K$               | total energy                |
| K     | $=\dot{E}-m_0c^2$   | kinetic energy              |
| β     | $=rac{v}{c}=rac{Pc}{E};$ $\gamma=rac{1}{\sqrt{1-eta^2}}=rac{E}{m_0c^2}$ | relativistic beta and gamma |

#### Towards the equation of motion

Taylor expansion of the  $B_y$  field:

$$B_{y}(x) = B_{y0} + \frac{\partial B_{y}}{\partial x}x + \frac{1}{2}\frac{\partial^{2}B_{y}}{\partial x^{2}}x^{2} + \frac{1}{3!}\frac{\partial^{3}B_{y}}{\partial x^{3}}x^{3} + \dots$$

Now we drop the suffix 'y' and normalize to the magnetic rigidity  $P/q=B\rho$ 

$$\frac{B(x)}{P/q} = \frac{B_0}{B_0\rho} + \frac{g}{P/q}x + \frac{1}{2}\frac{g'}{P/q}x^2 + \frac{1}{3!}\frac{g''}{P/q}x^3 + \dots$$
$$= \frac{1}{\rho} + kx + \frac{1}{2}mx^2 + \frac{1}{3!}nx^3 + \dots$$

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In the linear approximation, only the terms linear in x and y are taken into account:

- ▶ dipole fields, 1/ρ
- quadrupole fields, k

It is more practical to use "separate function" magnets, rather than combined ones:

- split the magnets and optimize them regarding their function
  - bending
  - focusing, etc.

### The equation of motion in radial coordinates

Let's consider a local segment of one particle's trajectory:

![](_page_45_Figure_2.jpeg)

and recall the radial centrifugal acceleration:  $a_r = \frac{d^2 \rho}{dt^2} - \rho \left(\frac{d\theta}{dt}\right)^2 = \frac{d^2 \rho}{dt^2} - \rho \omega^2$ .

• For an ideal orbit: 
$$\rho = \text{const} \Rightarrow \frac{d\rho}{dt} = 0$$

$$\Rightarrow \text{the force is} \qquad \begin{array}{l} F_{\text{centrifugal}} = -m\rho\omega^2 = -mv^2/\rho \\ F_{\text{Lorentz}} = qB_yv = -F_{\text{centrifugal}} \end{array} \Rightarrow \qquad \begin{array}{l} \frac{P}{q} = B_y\rho \end{array}$$

For a general trajectory: 
$$\rho \to \rho + x$$
:  
 $F_{\text{centrifugal}} = m a_r = -F_{\text{Lorentz}} \Rightarrow m \left[ \frac{d^2}{dt^2} \left( \rho + x \right) - \frac{v^2}{\rho + x} \right] = -qB_y v$ 

$$F = \underbrace{m\frac{d^2}{dt^2}(\rho + x)}_{\text{term 1}} - \underbrace{\frac{mv^2}{\rho + x}}_{\text{term 2}} = -qB_y v$$

• Term 1: As  $\rho = \text{const...}$ 

$$m\frac{\mathrm{d}^2}{\mathrm{d}t^2}\left(\rho+x\right) = m\frac{\mathrm{d}^2}{\mathrm{d}t^2}x$$

▶ Term 2: Remember:  $x \approx mm$  whereas  $\rho \approx m \rightarrow we$  develop for small x

remember  

$$\frac{1}{\rho+x} \approx \frac{1}{\rho} \left( 1 - \frac{x}{\rho} \right)$$

$$\left| \begin{array}{c} \text{Taylor expansion:} \\ f(x) = f(x_0) + \\ + (x - x_0) f'(x_0) + \frac{(x - x_0)^2}{2!} f''(x_0) + \cdots \right. \\ m \frac{d^2x}{dt^2} - \frac{mv^2}{\rho} \left( 1 - \frac{x}{\rho} \right) = -qB_y v$$

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The guide field in linear approximation  $B_y = B_0 + x \frac{\partial B_y}{\partial x}$ 

$$m\frac{d^2x}{dt^2} - \frac{mv^2}{\rho}\left(1 - \frac{x}{\rho}\right) = -qv\left\{B_0 + x\frac{\partial B_y}{\partial x}\right\} \qquad \text{let's divide by } m$$
$$\frac{d^2x}{dt^2} - \frac{v^2}{\rho}\left(1 - \frac{x}{\rho}\right) = -\frac{qvB_0}{m} - x\frac{qvg}{m}$$

Let's change the independent variable:  $t \rightarrow s$ 

$$\frac{dx}{dt} = \frac{dx}{ds}\frac{ds}{dt} = x'v$$

$$\frac{d^2x}{dt^2} = \frac{d}{dt}\frac{dx}{dt} = \frac{d}{dt}\left(\underbrace{\frac{dx}{ds}}_{x'}\frac{ds}{dt}_{v}\right) = \frac{d}{dt}(x'v) =$$

$$= \frac{d}{ds}\underbrace{\frac{ds}{dt}}_{v}(x'v) = \frac{d}{ds}(x'v^2) = x''v^2 + x'2v\frac{dv}{ds}$$

$$x''v^2 - \frac{v^2}{\rho}\left(1 - \frac{x}{\rho}\right) = -\frac{qvB_0}{m} - x\frac{vg}{m} \quad \text{let's divide by } v^2$$

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$$x'' - \frac{1}{\rho} \left( 1 - \frac{x}{\rho} \right) = -\frac{qB_0}{mv} - x\frac{qg}{mv}$$
$$x'' - \frac{1}{\rho} + \frac{x}{\rho^2} = -\frac{B_0}{P/q} - \frac{xg}{P/q}$$
$$x'' - \frac{Y}{\rho} + \frac{x}{\rho^2} = -\frac{Y}{\rho} - kx$$

Remember:

$$mv = p$$

Normalize to the momentum of the particle:

$$\frac{1}{\rho} = \frac{B_0}{P/q} \, [\mathrm{m}^{-1}]; \quad k = \frac{g}{P/q} \, [\mathrm{m}^{-2}]$$

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$$x'' + x\left(\frac{1}{\rho^2} + k\right) = 0$$

Equation for the vertical motion

• 
$$\frac{1}{a^2} = 0$$
 usually there are not vertical bends

$$k \leftrightarrow -k$$
 quadrupole field changes sign

$$y'' - ky = 0$$

## **APPENDIX II**

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#### Stability condition

Question: Given a periodic lattice with generic transport map M,

$$M = \left(\begin{array}{cc} a & b \\ c & d \end{array}\right)$$

under which condition the matrix M provides stable motion after N turns (with  $N \to \infty$ )?

$$x_N = \underbrace{M \cdot \ldots \cdot M \cdot M \cdot M}_{N \text{ turns with } N \to \infty} x_0 = M^N x_0$$

The <u>answer</u> is simple: the motion is stable when all elements of  $M^N$  are finite, with  $N \to \infty$ . The difficult question is... <u>how do we compute  $M^N$  with  $N \to \infty$ ?</u> Remember:

Remember:

▶ det (M) = ad - bc = 1

trace 
$$(M) = a + d$$

If we diagonalize M, we can rewrite it as:

$$M = U \cdot \left(\begin{array}{cc} \lambda_1 & 0 \\ 0 & \lambda_2 \end{array}\right) \cdot U^{\mathsf{T}}$$

where U is some unitary matrix,  $\lambda_1$  and  $\lambda_2$  are the eigenvalues.

#### Extra: Stability condition (cont.)

What happens if we consider N turns?

$$M^{N} = U \cdot \begin{pmatrix} \lambda_{1}^{N} & 0 \\ 0 & \lambda_{2}^{N} \end{pmatrix} \cdot U^{T}$$

Notice that  $\lambda_1$  and  $\lambda_2$  can be complex numbers. Given that det (M) = 1, then

$$\lambda_1 \cdot \lambda_2 = 1 \quad \rightarrow \lambda_1 = \frac{1}{\lambda_2} \quad \rightarrow \lambda_{1,2} = e^{\pm i x}$$

 $\Rightarrow$  to have a stable motion, x must be real:  $x \in R$ .

Now we can find the eigenvalues through the characteristic equation:

$$\det (M - \lambda I) = \det \begin{pmatrix} a - \lambda & b \\ c & d - \lambda \end{pmatrix} = 0$$
$$\lambda^{2} - (a + d)\lambda + (ad - bc) = 0$$
$$\lambda^{2} - \operatorname{trace} (M)\lambda + 1 = 0$$
$$\operatorname{trace} (M) = \lambda + 1/\lambda =$$
$$= e^{ix} + e^{-ix} = 2\cos x$$

From which derives the stability condition:

since 
$$x \in \mathbb{R} \rightarrow |\text{trace}(M)| \leq 2$$